B.1. Text of the regulation, general requirements

1. Purpose

1.1. This regulation provides a worldwide-harmonized measurement method for the determination of the levels of gaseous pollutant emissions at the tailpipe, the emissions of carbon dioxide and the energy efficiency in terms of fuel consumption of two-wheeled motor vehicles that are representative for real world vehicle operation

2. Scope

2.1 Two-wheeled motor vehicles equipped with a propulsion unit in accordance with table B.1-1:

	Vehicle with PI engines (Petrol)	Vehicle with CI engines (Diesel)
Type I Test	Yes	Yes
Type I Test particulate mass	Yes (only for DI)	Yes
Type II Test	Yes	Yes
Type VII Test	Yes	Yes

Table B.1-1

Note: For vehicles with Bi fuels, if the petrol fuel tank (provided for limp home or for starting) capacity is not exceeding two litres, Type I test need not be done in petrol mode.

3. Vehicle sub-classification

3.1 Figure B.1-1 provides a graphical overview of the vehicle subclassification in terms of engine capacity and maximum vehicle speed if subject to the environmental test types indicated by the (sub-)class numbers in the graph areas. The numerical values of the engine capacity and maximum vehicle speed shall not be rounded up or down.

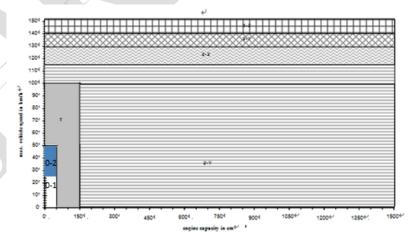


Figure B.1.-1: Vehicle sub-classification for environmental testing, test types I and VII

3.2. Class 0

Vehicles that fulfil the following specifications belong to class 0 and shall be sub-classified in:

Engine Capacity $\leq 50 \text{cm}^3$ and $v_{\text{max}} \leq 25 \text{km/h}$	Sub-class 0-1
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Engine Capacity $\leq 50 \text{cm}^3$ and $25 \text{km/h} < v_{\text{max}} \leq 50 \text{km/h}$ Sub	class 0-2
---	-----------

Table B.1.-2: sub-classification criteria for class 0 Two wheeled vehicles

3.3 Class 1

Vehicles that fulfil the following specifications belong to class 1:

50cm ³ < Engine Capacity < 150cm ³ and v _{max} ≤ 50km/h	Class 1
Or	
Engine Capacity < 150cm ³ and 50km/h < v _{max} < 100km/h	

Table B.1.-3: Classification criteria for class 1 Two wheeled vehicles

3.4. Class 2

Vehicles that fulfil the following specifications belong to class 2 and shall be sub-classified in:

Engine Capacity <150cm³ and 100km/h ≤v _{max}	Sub-class 2-1
<115km/h	
Or	
Engine Capacity $\geq 150 \text{cm}^3$ and $v_{\text{max}} < 115 \text{km/h}$	
$115 \text{km/h} \le v_{\text{max}} < 130 \text{km/h}$	Sub-class 2-2

Table B.1.-4: sub-classification criteria for class 2 Two wheeled vehicles

3.5. Class 3

Vehicles that fulfil the following specifications belong to class 3 and shall be sub-classified in:

$130 \text{km/h} \le v_{\text{max}} < 140 \text{km/h}$	Sub-class 3-1
$v_{\text{max}} \ge 140 \text{km/h}$	Sub-class 3-2

Table B.1.-5: sub-classification criteria for class 3 Two wheeled vehicles

3.6 A Contracting Party may choose Class 0 vehicles to be excluded from the contracting party's regulation

4. **Definitions**

The following definitions shall apply in this GTR:

- 4.1 "Equivalent inertia" determined in relation to the reference mass as defined in paragraph 4.41, to this regulation
- 4.2 "Engine and vehicle characteristics": Subject to the provisions of paragraph 6.2.1, the engine and vehicle characteristics as defined in Annex 4 to this regulation.
- 4.3 "Unladen mass" (mk) means the nominal mass of a complete vehicle as determined by the following criteria:

Mass of the vehicle with bodywork and all factory fitted equipment, electrical and auxiliary equipment for normal operation of vehicle, including liquids, tools, fire extinguisher, standard spare parts, chocks and spare wheel, if fitted.

The fuel tank shall be filled to at least 90 per cent of rated capacity and the other liquid containing systems to 100 per cent of the capacity specified by the manufacturer

- 4.4 "Driver mass" means the nominal mass of a driver that shall be 75 kg (subdivided into 68 kg occupant mass at the seat and 7 kg luggage mass in accordance with ISO standard 2416-1992)
- 4.5 "Gaseous pollutants" means carbon monoxide (CO), oxides of nitrogen (NOx) expressed in terms of nitrogen dioxide (NO2) equivalence, and hydrocarbons (HC), assuming a ratio of:

 $C_1H_{1.85}$ for petrol,

C₁H_{1.86} for diesel fuel.

- 4.6 "CO2 emissions" means carbon dioxide.
- 4.7 "Fuel consumption" means the amount of fuel consumed, calculated by the carbon balance method.
- 4.8 "Maximum vehicle speed" (vmax) is the maximum speed of the vehicle as declared by the manufacturer, measured in accordance with Appendix 1 and Appendix 1.1 of Annex-X of European Union Regulation (EU) no. 134/2014(on the maximum design speed, maximum torque and maximum net engine power of two wheeled motor vehicles).
- 4.9 "Maximum net engine power" is the maximum net engine power of the vehicle as declared by the manufacturer, measured in accordance with Appendix 2, Appendix 2.2, Appendix 2.2.1 and Appendix 2.3 of Annex X of European Union Regulation (EU) no. 134/2014.
- 4.10 'Actuator' means a converter of an output signal from a control unit into motion, heat or other physical state in order to control the powertrain, engine(s) or drive train;
- 4.11 'Air intake system' means a system composed of components allowing the fresh-air charge or air-fuel mixture to enter the engine and includes, if fitted, the air filter, intake pipes, resonator(s), the throttle body and the intake manifold of an engine;
- 4.12 'Boost control' means a device to control the boost level produced in the induction system of a turbocharged or super-charged engine;
- 4.13 'Carburettor' means a device that blends fuel and air into a mixture that can be combusted in a combustion engine;
- 4.14 'Catalytic converter' means an emission pollution-control device which converts toxic by-products of combustion in the exhaust of an engine to less toxic substances by means of catalysed chemical reactions;
- 4.15 'Cold-start device' means a device that temporarily enriches the air/fuel mixture of the engine, or any device or means which can assist to start the engine.
- 4.16 'Common rail' means a fuel supply system to the engine in which a common high pressure is maintained;
- 4.17 'Compression ignition engine' or 'CI engine' means a combustion engine working according to the principles of the 'Diesel' cycle;
- 4.18 'Defeat device' means any element of design which senses temperature, vehicle speed, engine rotational speed, drive gear, manifold vacuum or any other parameter for the purpose of activating, modulating, delaying or deactivating the operation of any part of the emission control and exhaust after-treatment system that reduces the effectiveness of the emission control system under conditions which may reasonably be expected to be

- encountered in normal vehicle operation and use. Such an element of design may not be considered a defeat device if:
- (a) The need for the device is justified in terms of protecting the engine against damage or accident and for safe operation of the vehicle; or
- (b) The device does not function beyond the requirements of engine starting; or
- (c) Conditions are substantially included in the Type 1 test procedures.
- 4.19 'Drive train control unit' means the on-board computer that partly or entirely controls the drive train of the vehicle;
- 4.20 'Drive train' means the part of the powertrain downstream of the output of the propulsion unit(s) that consists if applicable of the torque converter clutches, the transmission and its control, either a drive shaft or belt drive or chain drive, the differentials, the final drive, and the driven wheel tyre (radius);
- 4.21 'Electronic throttle control' (ETC) means the control system consisting of sensing of driver input via the accelerator pedal or handle, data processing by the control unit(s), resulting actuation of the throttle and throttle position feedback to the control unit in order to control the air charge to the combustion engine;
- 4.22 'Engine capacity' means:
 - (a) for reciprocating piston engines, the nominal engine swept volume;
 - (b) for rotary-piston (Wankel) engines, double the nominal engine swept volume;
- 4.23 'Engine control unit' means an on-board computer that partly or entirely controls the engine(s) and all emission related devices / systems of the vehicle:
- 4.24 'Exhaust emissions' means emissions of gaseous pollutants and particulate matter from the tailpipe;
- 4.25 'Exhaust gas recirculation (EGR) system' means a part of the exhaust gas flow led back to the combustion chamber of an engine in order to lower the combustion temperature;
- 4.26 'Intercooler' means a heat exchanger that removes waste heat from the compressed air by a charger before entering into the engine, thereby improving volumetric efficiency by increasing intake air charge density;
- 4.27 'Distance accumulation' means a representative test vehicle or a fleet of representative test vehicles driving a predefined distance as set out in [point 5 of section B.4.] in accordance with the test requirements of Annex B.4.1. or B.4.2.];
- 4.28 'Mono-fuel vehicle' means a vehicle that is designed to run on one type of fuel;
- 4.29 'Opacity' means an optical measurement of the density of particulate matter in the exhaust flow of an engine, expressed in m⁻¹;
- 4.30 'Parent vehicle' means a vehicle that is representative of a propulsion unit family set out in Annex B.5.10 :
- 4.31 'Particulate filter' means a filtering device fitted in the exhaust system of a vehicle to reduce particulate matter from the exhaust flow;
- 4.32 'Particulate matter (PM)' means the mass of any particulate material from the vehicle exhaust quantified according to the dilution, sampling and measurement methods as specified in this UN GTR

Particle number emissions" (PN) means the total number of solid particles emitted from the vehicle exhaust quantified according to the dilution, sampling and measurement methods as specified in this UN GTR.

- 4.33 'Pollution-control device' means those components (hardware or software) of a vehicle that control or reduce emissions;
- 4.34 'Positive ignition engine' or 'PI engine' means a combustion engine working according to the principles of the 'Otto' cycle;
- 4.35 'Powertrain' means the components and systems of a vehicle that generate power and deliver it to the road surface, including the engine(s), the engine management systems or any other control module, the pollution environmental protection control devices including pollutant emissions and noise abatement systems, the transmission and its control, either a drive shaft or belt drive or chain drive, the differentials, the final drive, and the driven wheel tyre (radius);
- 4.36 'Powertrain calibration' means the application of a specific set of data maps and parameters used by the control unit's software to tune the vehicle's powertrain, propulsion or drive train unit(s)'s control;
- 4.37 'Powertrain control unit' means a combined control unit of combustion engine(s), electric traction motors or drive train unit systems including the transmission or the clutch:
- 4.38 'Powertrain software' means a set of algorithms concerned with the operation of data processing in powertrain control units, propulsion control units or drive-train control units, containing an ordered sequence of instructions that change the state of the control units;
- 4.39 'Properly maintained and used' means that when selecting a test vehicle it satisfies the criteria with regard to a good level of maintenance and normal use according to the recommendations of the vehicle manufacturer for acceptance of such a test vehicle;
- 4.40 'Propulsion unit' means a combustion engine, an electric motor, any hybrid application or a combination of those engine types or any other engine type;
- 4.41 'Reference mass (m_{ref})' means the unladen mass of the vehicle increased with the mass of the driver (75 kg);
- 4.42 'Scavenging port' means a connector between crankcase and combustion chamber of a two-stroke engine through which the fresh charge of air, fuel and lubrication oil mixture enters the combustion chamber;
- 4.43 'Sensor' means a converter that measures a physical quantity or state and converts it into an electric signal that is used as input to a control unit;
- 4.44 'Stop-start system' means automatic stop and start of the propulsion unit;
- 4.45 'Forced Induction System' is the process of delivering compressed air / air-fuel mixture to the intake of an internal combustion engine.
- 4.45.1 'Super-charger' means an intake air/air fuel mixture compressor run by any means other than engine exhaust and used for forced induction of a combustion engine, thereby increasing propulsion unit performance;
- 4.45.2 'Turbocharger' means an exhaust gas turbine-powered centrifugal compressor boosting the amount of air charge into the combustion engine, thereby increasing the propulsion unit performance;
- 4.46 'Tailpipe emissions' means the emission of gaseous pollutants and particulate matter at the tailpipe of the vehicle;

4.47 "Useful life" means the relevant period of distance and/or time over which compliance with the relevant gaseous and particulate emission limits has to be assured.

5. General Requirements

- 5.1 The manufacturer shall equip two-wheeled vehicles in the scope of this GTR with systems, components and separate technical units affecting the environmental performance of a vehicle that are designed, constructed and assembled so as to enable the vehicle in normal use and maintained according to the prescriptions of the manufacturer to comply with the detailed technical requirements and testing procedures of this GTR during its useful life, as defined by the Contracting Party, including when installed in the vehicle.
- Any hidden strategy that 'optimises' the powertrain of the vehicle running the relevant test cycles in an advantageous way, reducing tailpipe emissions and running significantly differently under real-world conditions differently than under emission test laboratory conditions, is considered a defeat strategy and is prohibited, unless the manufacturer has documented and declared it to the satisfaction of the responsible authority.
- 5.2.1 An element of design shall not be considered a defeat device if any of the following conditions is met:
- 5.2.1.1 the need for the device is justified in terms of protecting the engine against damage or accident and ensuring safe operation of the vehicle;
- 5.2.1.2 the device does not function beyond the requirements of engine starting;
- 5.2.1.3 the operating conditions are included to a substantial extent in the test procedures for verifying if the vehicle complies with this GTR
- 5.3 The environmental performance type-approval regarding test types I, II and VII shall extend to different vehicle variants, versions and propulsion unit types and families, provided that the vehicle version, propulsion unit or pollution-control system parameters specified in [Annex B.5.10] are identical or remain within the prescribed and declared tolerances in that Annex.

6. Nomenclature

6.1 Wherever required, values shall be rounded-off as follows:

When the digit next beyond that last place to be retained, is

- (a) less than 5, retain the last digit unchanged. (E.g. 1.243 becomes 1.24)
- (b) greater than 5, increase the last digit by one. (E.g. 1.246 becomes 1.25)
- (c) equals 5, and there are no digits beyond this, or only zeros, increase the last digit by one, if the last digit is odd (E.g. 1.235 becomes 1.24) and retain the last digit unchanged if it is even (E.g. 1.245 becomes 1.24)
- d) equals 5, and there are digits beyond this, increase the last digit by one. (E.g. 1.2451 becomes 1.25)
- 6.2 Throughout this document the decimal sign is a full stop (period) "." and if used, the thousands separator is a comma ",".
- 6.3 Temperature shall be measured in $^{\circ}$ C. Wherever temperature conversion is required in K for calculation purpose, the following equivalence shall be used, $^{\circ}$ C = 273.15K.

7. Performance requirements for the type I test of a two-wheeled vehicle

- 7.1 The principal requirements of performance are set out in point 7.2 for two-wheeled vehicles. Contracting Parties may also accept compliance with one or more of the alternative performance requirements set out in point 7.3 for two-wheeled vehicles.
- 7.2 The gaseous pollutant emissions for each class of two-wheeled vehicle set out in point 3. of section B.1., obtained when tested in accordance with the applicable test cycle specified in Annex B.5.14., shall not exceed the pollutant tailpipe emission limit values specified in Table B.1.-6

Class		Limi	ts (mg/k	Reference Fuel		
	CO	THC	NMHC	NOx	PM	
PI	1,000	100	68	60	4.5 (only for DI)	As per Annex ###(corresponding to E5
CI	500	100	68	90	4.5	As per Annex ###(corresponding to B5)

Table B.1.-6: Principal performance requirements.

Note:

The test values multiplied by DF must be below the limits in the above table. DF for PI engine vehicles for CO is 1.3, THC is 1.3, NMHC is 1.3, NOx is 1.3 and PM is 1.0. DF for CI engine vehicles for CO is 1.3, THC is 1.1, NMHC is 1.1, NOx is 1.1 and PM is 1.0.

7.3 Alternative performance requirements

The gaseous emissions for each class of vehicle set out in point 3. of section B.1., obtained when tested in accordance with the applicable test cycle specified in Annex B.5.14., shall not exceed the pollutant emission limit values specified in table B.1.-7, as per the Alternate chosen by the Contracting Party.

Cub		Limits (mg/km) for PI Engines										
Sub- Class		СО			НС			NOx			HC+NOx	
	Alt A (3)	Alt B ⁽⁴⁾	Alt C ⁽⁵⁾	Alt A (3)	Alt B ⁽⁴⁾	Alt C ⁽⁵⁾	Alt A (3)	Alt B ⁽⁴⁾	Alt C ⁽⁵⁾	Alt A ^{(1) (3)}	Alt B ⁽⁴⁾	Alt C ⁽⁵⁾
1	1,403	1,140	2,620	NA	380	750	390	70	170	790	NA	NA
2-1(2)	1,403	1,140	2,620	NA	380	750	390	70	170	790	NA	NA
2-2	1,970	1,140	2,620	NA	380	750	340	70	170	670	NA	NA
3	1,970	1,140	2,620	NA	170	330	200	90	220	400	NA	NA

Notes:

- (1) For Alt A, there is an option to comply with evaporative emission norm of 6g/test (instead of 2g/test). HC+NOx norms to be tightened by 200mg/km from the values given in table.
- (2) Applicable parts of driving cycle for Alt A are part 1 RS cold and part 1 RS hot, as against Euro 4 part 1 RS cold and part 2 RS hot.
- (3) For Alt A: Test values must be below the Alt A limits in the above table.
- (4) For Alt B: Test values multiplied by DF must be below the Alt B limits in the above table; DF for CO is 1.3, for NOx is 1.2 and for HC+NOx is 1.2
- (5) For Alt C limits, DF are not applicable.

Table B.1.-7: Alternate performance requirements.

B.2. Text of the regulation, Test Type I, Exhaust Emissions after Cold Start

1. Introduction

- 1.1. This section provides a harmonised method for the determination of the levels of gaseous pollutant emissions and particulate matter collected at the tailpipe, the emissions of carbon dioxide and is referred to in Annex B.4. to determine the energy efficiency in terms of fuel consumption of the vehicle types within the scope of this GTR that are representative for real world vehicle operation.
- 1.2. The results may form the basis for limiting gaseous pollutants, to report carbon dioxide and the energy efficiency of the vehicle in terms of fuel consumption by the manufacturer within the environmental performance approval procedures in a robust and harmonised way.

2. General Requirements

2.1. The components liable to affect the emission of gaseous pollutants, carbon dioxide emissions and affecting the energy efficiency of the vehicle shall be so designed, constructed and assembled as to enable the vehicle in normal use, despite the vibration to which it may be subjected, to comply with the provisions of this GTR.

Note 1: The symbols used in sections B.2., B.3. and B.4. are summarised in Annex B.5.1.

3. Test Conditions

3.1. Test room

- 3.1.1. The test room with the chassis dynamometer and the gas sample collection device shall have a temperature of 25± 5 °C. The room temperature shall be measured in the vicinity of the vehicle cooling blower (fan) before and after the type I test.
- 3.1.2. The absolute humidity (Ha) of either the air in the test cell or the intake air of the engine shall be measured, recorded and correction factors for NOx shall be applied.
- 3.1.3. The soak area shall have a temperature of 25 ± 5 °C and be such that the test vehicle which has to be preconditioned can be parked in accordance with para. 4.2.4. of part B2.

3.2. WMTC, test cycle parts

The WMTC test cycle (vehicle speed patterns) for type I, VII and VIII environmental tests consist of up to three parts as set out in Annex B.5.14. Depending on the vehicle classification in terms of engine displacement and maximum design vehicle speed in accordance with point 3. of section B.1., the following WMTC test cycle parts in Table B.2.-1 shall be run:

Vehicle Sub classification	Applicable Parts of WMTC as specified in Annex B5.15			
Class 0 subdivided in	:			
Sub-class 0-1:	part 1, RST25 in cold condition, followed by part 1,RST25 in warm condition			
Sub-class 0-2:	part 1, RST45 in cold condition, followed by part 1,RST45 in warm condition			
Class 1	part 1, reduced vehicle speed in cold condition,followed by part 1, reduced vehicle speed in warm condition			
Class 2 subdivided in				
Sub-class 2-1:	part 1, reduced vehicle speed in cold condition,followed by part 2, reduced vehicle speed in warm condition			
Sub-class 2-2:	part 1, in cold condition,followed by part 2, in warm condition			
Class 3 subdivided in	:			
Sub-class 3-1:	part 1, in cold condition,followed by part 2, in warm condition,followed by part 3, reduced vehicle speed in warm condition			
Sub-class 3-2:	part 1, in cold condition,followed by part 2, in warm condition,followed by part 3, in warm condition			

3.3. Specification of the reference fuel

The appropriate reference fuels as specified in Annex B.5.2. shall be used for conducting test type I.

Reference Fuel Specification	
Performance requirement	Reference fuel specification
Principal Norm requirements	See Annex B5.2
Alternative A	###
Alternative B	###
Alternative C	###

Principal norms for Type I test shall be with E0 or E5 reference fuel for gasoline vehicles. For alternate norms, regional reference fuels used for Type I test by contracting parties may be used.

3.4. Type I test procedure

3.4.1. Driver

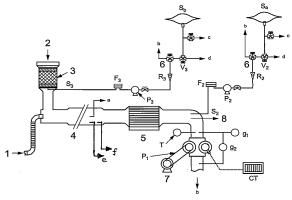
The test driver shall have a mass of 75 kg \pm 5 kg.

3.4.2. Test bench specifications and settings

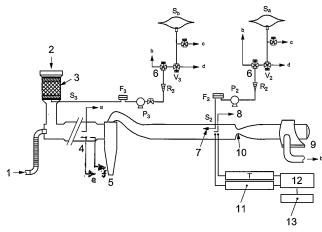
- 3.4.2.1. The chassis dynamometer shall have a single roller in the transverse plane with a diameter of at least 400 mm, alternatively, a chassis dynamometer equipped with two rollers on a single axle in the transverse plane (one for each wheel) is permitted when testing two-wheeled vehicles with twinned wheels.
- 3.4.2.2. The dynamometer shall be equipped with a roller revolution counter for measuring actual distance travelled.
- 3.4.2.3. Dynamometer flywheels or other means shall be used to simulate the inertia specified in point 4.2.2.
- 3.4.2.4. The dynamometer rollers shall be clean, dry and free from anything which might cause the tyre(s) to slip.

3.4.2.5. Cooling fan specifications as follows:

- 3.4.2.5.1. Throughout the test, a variable-rotation speed cooling blower (fan) shall be positioned in front of the vehicle so as to direct the cooling air onto it in a manner that simulates actual operating conditions. The blower rotation speed shall be such that, within the operating range of 10 to 50 km/h, the linear velocity of the air at the blower outlet is within ±5 km/h of the corresponding roller speed (from which the actual vehicle speed is calculated). At the range of over 50 km/h, the linear velocity of the air shall be within ±10 percent. At a desired vehicle speed of less than 10 km/h, air velocity may be zero.
- 3.4.2.5.2. The air velocity referred to in point 3.4.2.5.1. shall be determined as an averaged value of nine measuring points which are located at the centre of each rectangle dividing the whole of the blower outlet into nine areas (dividing both horizontal and vertical sides of the blower outlet into three equal parts). The value at each of the nine points shall be within 10 percent of the average of the nine values.
- 3.4.2.5.3. The blower outlet shall have a cross-section area of at least 0.4 m2 and the bottom of the blower outlet shall be between 5 and 20 cm above floor level. The blower outlet shall be perpendicular to the longitudinal axis of the vehicle, between 30 and 45 cm in front of its front wheel. The device used to measure the linear velocity of the air shall be located at between 0 and 20 cm from the air outlet.
- 3.4.2.6. The detailed requirements regarding the chassis dynamometer are listed in Annex B.5.7.
- 3.4.3. Exhaust gas measurement system
 - 3.4.3.1. The gas-collection device shall be a closed-type device that can collect all exhaust gases at the vehicle exhaust outlets on condition that it satisfies the backpressure condition of ± 1.225 Pa (125 mm H2O). An open system may be used instead if it is confirmed that all the exhaust gases are collected. The gas collection shall be such that there is no condensation which could appreciably modify the nature of exhaust gases at the test temperature. An example of a gas-collection device is illustrated in Figure B.2.-1 a and Figure B.2.-1 b:



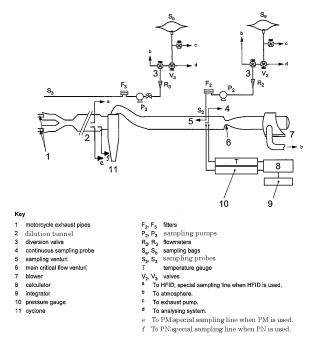
exhaust gas positive displacement pump dilution air sampling pumps dilution air filter dilution tunnel sampling bags heating exchange sampling probe temperature gauge motor valves To HFID; special sampling line when HFID is used. revolution counte filters To exhaust pump To analysing system.
To PM;special sampling line when PM is used To PN; special sampling line when PN is used



F₂, F₃ filters
P₂, P₃ sampling pumps
R₂, R₃ flowmeters exhaust gas dilution air dilution air filter dilution tunnel sampling bags sampling probes cyclone diversion valve temperature gauge ${
m V_2,\,V_3}$ valves $^{
m a}$ To HFID; special sampling line when HFID is used. sampling venturi continuous sampling prob blower To atmosphere. 10 main critical flow venturi To exhaust pump. 11 pressure gauge To analysing system. 12 calculator To PM;special sampling line when PM is used. 13 integrator f $\,$ To PN; special sampling line when PN is used.

Schematic diagram for the representative closed type CVS system with CFV

Figure B.2.-1 a. An example of closed-type systems for sampling gases and measuring their volume



Schematic diagram for the representative open type CVS system with CFV

Figure B.2.-1 b. An example of open-type system for sampling gases and measuring their volume.

3.4.3.2. A connecting tube shall be placed between the device and the exhaust gas sampling system. This tube and the device shall be made of stainless steel, or of some other

material which does not affect the composition of the gases collected and which withstands the temperature of these gases.

3.4.3.3. Positive displacement pump (PDP)

- 3.4.3.3.1. A positive displacement pump (PDP) full flow exhaust dilution system satisfies the requirements of this Sub-Annex by metering the flow of gas through the pump at constant temperature and pressure. The total volume is measured by counting the revolutions made by the calibrated positive displacement pump. The proportional sample is achieved by sampling with pump, flow meter and flow control valve at a constant flow rate.
- 3.4.3.3.2. A heat exchanger capable of limiting the temperature variation of the diluted gases in the pump intake to \pm 5 °C shall be in operation throughout the test. This exchanger shall be equipped with a preheating system capable of bringing the exchanger to its operating temperature (with the tolerance of \pm 5 °C before the test begins.
- 3.4.3.3.A positive displacement pump shall be used to draw in the diluted exhaust mixture. This pump shall be equipped with a motor with several strictly controlled uniform rotation speeds. The pump capacity shall be large enough to ensure the intake of the exhaust gases. A device using a critical-flow venturi (CFV) may also be used.
- 3.4.3.3.4. A device (T) shall be used for the continuous recording of the temperature of the diluted exhaust mixture entering the pump.
- 3.4.3.3.5. Two gauges shall be used, the first to ensure the pressure depression of the dilute exhaust mixture entering the pump relative to atmospheric pressure, and the second to measure the dynamic pressure variation of the positive displacement pump.

3.4.3.4. Critical flow venturi (CFV)

- 3.4.3.4.1. The use of a CFV for the full flow exhaust dilution system is based on the principles of flow mechanics for critical flow. The variable mixture flow rate of dilution and exhaust gas is maintained at sonic velocity that is inversely proportional to the square root of the gas temperature and directly proportional to gas pressure. Flow is continually monitored, computed and integrated throughout the test.
- 3.4.3.4.2. The use of an additional critical flow sampling venturi ensures the proportionality of the gas samples taken from the dilution tunnel. As both pressure and temperature are equal at the two venturi inlets, the volume of the gas flow diverted for sampling is proportional to the total volume of diluted exhaust gas mixture produced.
- 3.4.3.4.3. A CFV shall measure the flow volume of the diluted exhaust gas.
- 3.4.3.5. A probe shall be located near to, but outside, the gas-collecting device, to collect samples of the dilution air stream through a pump, a filter and a flow meter at constant flow rates throughout the test.
- 3.4.3.6. A sample probe pointed upstream into the dilute exhaust mixture flow, upstream of the positive displacement pump, shall be used to collect samples of the dilute exhaust mixture through a pump, a filter and a flow meter at constant flow rates throughout the test. The minimum sample flow rate in the sampling devices shown in Figure B.2.-1 and in point 3.4.3.7. I shall be at least 150 litre/hour.

3.4.3.7. Three-way valves shall be used on the sampling system described in points 3.4.3.5. and 3.4.3.8. to direct the samples either to their respective bags or to the outside throughout the test.

3.4.3.8. Gas-tight collection bags

- 3.4.3.8.1. For dilution air and dilute exhaust mixture the collection bags shall be of sufficient capacity not to impede normal sample flow and shall not change the nature of the pollutants concerned.
- 3.4.3.8.2. The bags shall have an automatic self-locking device and shall be easily and tightly fastened either to the sampling system or the analysing system at the end of the test.
- 3.4.3.9. A revolution counter shall be used to count the revolutions of the positive displacement pump throughout the test.
 - Note 2: Attention shall be paid to the connecting method and the material or configuration of the connecting parts, because each section (e.g. the adapter and the coupler) of the sampling system can become very hot. If the measurement cannot be performed normally due to heat damage to the sampling system, an auxiliary cooling device may be used as long as the exhaust gases are not affected.
 - Note 3: With open type devices, there is a risk of incomplete gas collection and gas leakage into the test cell. There shall be no leakage throughout the sampling period.
 - Note 4: If a constant volume sampler (CVS) flow rate is used throughout the test cycle that includes low and high vehicle speeds all in one (i.e. part 1, 2 and 3 cycles), special attention shall be paid to the higher risk of water condensation in the high vehicle speed range.

3.4.3.10. Particulate mass emissions measurement equipment

3.4.3.10.1. Specification

3.4.3.10.1.1. System overview

- 3.4.3.10.1.1.1. The particulate sampling unit shall consist of a sampling probe (PSP) located in the dilution tunnel, a particle transfer tube (PTT), a filter holder(s) (FH), pump(s), flow rate regulators and measuring units. See Figures A5/11 and A5/12.
- 3.4.3.10.1.1.2. A particle size pre-classifier (PCF) (e.g. cyclone or impactor) may be used. In such case, it is recommended that it is employed upstream of the filter holder. However, a sampling probe, acting as an appropriate size classification device such as that shown in Figure A5/13, is acceptable.

3.4.3.10.1.2. General Requirements

- 3.4.3.10.1.2.1. The sampling probe for the test gas flow for particulates shall be so arranged within the dilution tunnel that a representative sample gas flow can be taken from the homogeneous air/exhaust mixture and shall be upstream of a heat exchanger (if any).
- 3.4.3.10.1.2.2. The particulate sample flow rate shall be proportional to the total mass flow of diluted exhaust gas in the dilution tunnel to within a tolerance of ±5 per cent of the particulate sample flow rate. The verification of the proportionality of the PM sampling should be made during the commissioning of the system and as required by the responsible authority.

- 3.4.3.10.1.2.3. The sampled dilute exhaust gas shall be maintained at a temperature above 293 K (20 °C) and below 325 K (52 °C) within 20 cm upstream or downstream of the particulate filter face. Heating or insulation of components of the PM sampling system to achieve this is permissible. In the event that the 52 °C limit is exceeded during a test where periodic regeneration event does not occur, the CVS flow rate should be increased or double dilution should be applied (assuming that the CVS flow rate is already sufficient so as not to cause condensation within the CVS, sample bags or analytical system).
- 3.4.3.10.1.2.4. The particulate sample shall be collected on a single filter per cycle part applicable according to vehicle class. Weighting factor for PM to be same as applied for all gaseous pollutants. All parts of the dilution system and the sampling system from the exhaust pipe up to the filter holder, which are in contact with raw and diluted exhaust gas, shall be designed to minimise deposition or alteration of the particulates. All parts shall be made of electrically conductive materials that do not react with exhaust gas components, and shall be electrically grounded to prevent electrostatic effects.
- 3.4.3.10.1.2.5. If it is not possible to compensate for variations in the flow rate, provision shall be made for a heat exchanger and a temperature control device as specified in Annex B.5.8. so as to ensure that the flow rate in the system is constant and the sampling rate accordingly proportional.
- 3.4.3.10.1.2.6. Temperatures required for the PM mass measurement shall be measured with an accuracy of ± 1 °C and a response time (t_{10} - t_{90}) of fifteen seconds or less.
- 3.4.3.10.1.2.7. The PM sample flow from the dilution tunnel shall be measured with an accuracy of ±2.5 per cent of reading or ±1.5 per cent full scale, whichever is the least. The above accuracy of the PM sample flow from the CVS tunnel is also applicable where double dilution is used. Consequently, the measurement and control of the secondary dilution air flow and diluted exhaust flow rates through the PM filter must be of a higher accuracy. All data channels required for the PM mass measurement shall be logged at a frequency of 1 Hz or faster. Typically, these would include:
 - (a) Diluted exhaust temperature at the PM filter;
 - (b) PM sampling flow rate;
 - (c) PM secondary dilution air flow rate (if secondary dilution is used);
 - (d) PM secondary dilution air temperature (if secondary dilution is used).
- 3.4.3.10.1.2.8. For double dilution systems, the accuracy of the diluted exhaust transferred from the dilution tunnel, in the equation is not measured directly but determined by differential flow measurement:

Vep=Vset- Vssd

where:

Vep: is the volume of diluted exhaust gas flowing through particulate filter under standard conditions;

Vset: is the volume of the double diluted exhaust gas passing through the particulate collection filters;

Vssd: is the volume of secondary dilution air.

- 3.4.3.10.1.2.9. The accuracy of the flow meters used for the measurement and control of the double diluted exhaust passing through the particulate collection filters and for the measurement/control of secondary dilution air shall be sufficient so that the differential volume [(symbol)] shall meet the accuracy and proportional sampling requirements specified for single dilution. The requirement that no condensation of the exhaust gas should occur in the CVS dilution tunnel, diluted exhaust flow rate measurement system, CVS bag collection or analysis systems shall also apply in the case of double dilution systems.
- 3.4.3.10.1.2.10. Each flow meter used in a particulate sampling and double dilution system shall be subjected to a linearity verification as required by the instrument manufacturer.

Figure A5/11 Particulate Sampling System

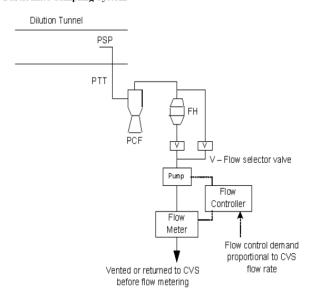
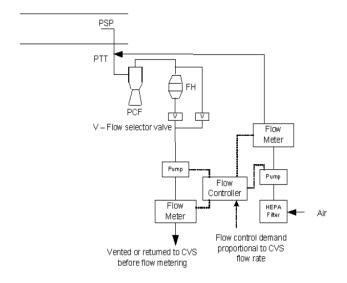


Figure A5/12 **Double Dilution Particulate Sampling System**



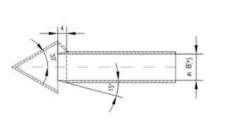
3.4.3.10.1.3. Specific requirements

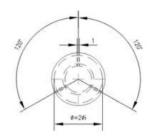
3.4.3.10.1.3.1. Particulate Matter (PM) sampling probe

3.4.3.10.1.3.1.1. The sample probe shall deliver the particle-size classification performance described in paragraph 4.2.1.3.1.4. below. It is recommended that this performance be achieved by the use of a sharp-edged, open-ended probe facing directly into the direction of flow plus a pre-classifier (cyclone impactor, etc.). An appropriate sampling probe, such as that indicated in Figure A5/13, may alternatively be used provided it achieves the pre-classification performance described in paragraph 4.2.1.3.1.4. below.

Figure A5/13

Alternative particulate sampling probe configuration





- (*) Minimum internal diameter
 Wall thickness ~ 1 mm Material stainless steel
- 3.4.3.10.1.3.1.2. The sample probe shall be installed at least 10 tunnel diameters downstream of the exhaust gas inlet to the tunnel and have an internal diameter of at least 8 mm.

If more than one simultaneous sample is drawn from a single sample probe, the flow drawn from that probe shall be split into identical sub-flows to avoid sampling artefacts.

If multiple probes are used, each probe shall be sharpedged, open-ended and facing directly into the direction of flow. Probes shall be equally spaced around the central longitudinal axis of the dilution tunnel, with the spacing between probes at least 5 cm.

- 3.4.3.10.1.3.1.3. The distance from the sampling tip to the filter mount shall be at least five probe diameters, but shall not exceed 2,000 mm.
- 3.4.3.10.1.3.1.4. The pre-classifier (e.g. cyclone, impactor, etc.) shall be located upstream of the filter holder assembly. The pre-classifier 50 percent cut point particle diameter shall be between 2.5 µm and 10 µm at the volumetric flow rate selected for sampling particulate mass emissions. The pre-classifier shall allow at least 99 percent of the mass concentration of 1 µm particles entering the pre-classifier to pass through the exit of the pre-classifier at the volumetric flow rate selected for sampling PM.

3.4.3.10.1.3.1.5. Particle transfer tube (PTT)

3.4.3.10.1.3.1.5.1. Any bends in the PTT shall be smooth and have the largest possible radii.

3.4.3.10.1.3.1.6. Secondary dilution

- 3.4.3.10.1.3.1.6.1. As an option, the sample extracted from the CVS for the purpose of PM measurement may be diluted at a second stage, subject to the following requirements:
 - i) Secondary dilution air shall be filtered through a medium capable of reducing particles in the most penetrating particle size of the filter material by ≥ 99.95 per cent, or through a HEPA filter of at least class H13 of EN 1822:2009. The dilution air may optionally be charcoal scrubbed before being passed to the HEPA filter. It is recommended that an additional coarse particle filter is situated before the HEPA filter and after the charcoal scrubber, if used.
 - ii) The secondary dilution air should be injected into the PTT as close to the outlet of the diluted exhaust from the dilution tunnel as possible.
 - iii) The residence time from the point of secondary diluted air injection to the filter face shall be at least 0.25 seconds (s), but no longer than five seconds.
 - iv) If the double diluted PM sample is returned to the CVS, the location of the sample return shall be selected so that it does not interfere with the extraction of other samples from the CVS.

3.4.3.10.1.3.2. Sample pump and flow meter

- 3.4.3.10.1.3.2.1. The sample gas flow measurement unit shall consist of pumps, gas flow regulators and flow measuring units.
- 3.4.3.10.1.3.2.2. The temperature of the gas flow in the flow meter may not fluctuate by more than ± 3 K except
 - (a) When the PM sampling flow meter has real time monitoring and flow control operating at 1 Hz or faster;
 - (b) During regeneration tests on vehicles equipped with periodically regenerating after-treatment devices.

Should the volume of flow change unacceptably as a result of excessive filter loading, the test shall be invalidated. When it is repeated, the rate of flow shall be decreased.

3.4.3.10.1.3.3. Filter and filter holder

- 3.4.3.10.1.3.3.1. A valve shall be located downstream of the filter in the direction of flow. The valve shall open and close within 1 s of the start and end of test.
- 3.4.3.10.1.3.3.2. For a given test, the gas filter face velocity shall be set to a single value within the range 20 cm/s to 105 cm/s and should be set at the start of the test so that 105 cm/s will not be exceeded when the dilution system is being operated with sampling flow proportional to CVS flow rate.

3.4.3.10.1.3.3.3. Fluorocarbon coated glass fibre filters or fluorocarbon membrane filters are required.

All filter types shall have a $0.3\mu m$ DOP (dioctylphthalate) or PAO (polyalpha-olefin) CS 68649-12-7 or CS 68037-01-4 collection efficiency of at least 99 per cent at a gas filter face velocity of 5.33 cm/s measured according to one of the following standards:

- (a) U.S.A. Department of Defense Test Method Standard, MIL-STD-282 method 102.8: DOP-Smoke Penetration of Aerosol-Filter Element
- (b) U.S.A. Department of Defense Test Method Standard, MIL-STD-282 method 502.1.1: DOP-Smoke Penetration of Gas-Mask Canisters
- (c) Institute of Environmental Sciences and Technology, IEST-RPCC021:

Testing HEPA and ULPA Filter Media.

- 3.4.3.10.1.3.3.4. The filter holder assembly shall be of a design that provides an even flow distribution across the filter stain area. The filter shall be round and have a stain area of at least 1075 mm².
- 3.4.3.10.1.3.4. Weighing chamber(or room) and analytical balance specifications
 - 3.4.3.10.1.3.4.1. Weighing chamber(or room) conditions
 - (a) The temperature of the chamber (or room) in which the particulate filters are conditioned and weighed shall be maintained to within 295 K \pm 2 K (22 °C \pm 2 °C, 22 °C \pm 1 °C if possible) during all filter conditioning and weighing.
 - (b) Humidity shall be maintained to a dew point of less than 283.5 K (10.5 $^{\circ}$ C) and a relative humidity of 45 per cent \pm 8 per cent.
 - (c) Limited deviations from weighing temperature and humidity specifications will be allowed provided their total duration does not exceed 30 minutes in any one filter conditioning period.
 - (d) The levels of ambient contaminants in the chamber (or room) environment that would settle on the particulate filters during their stabilization shall be minimised.
 - (e) During the weighing operation, no deviations from the specified conditions are permitted.
 - 3.4.3.10.1.3.4.1.1. Linear response of an analytical balance

The analytical balance used to determine the filter weight shall meet the linearity verification criterion of Table A5/1 below. This implies a precision (standard deviation) of at least 2 μ g and a resolution of at least 1 μ g. 1 digit = 1 μ g). At least 4 equally-spaced reference weights shall be tested. The zero value shall be within $\pm 1\mu$ g.

Table A5/1
Analytical balance verification criteria

Measurement system	Intercept b	Slope m	Standard error SEE	Coefficient of determination r ²
PM Balance	≤ 1per cent max	0.99 - 1.01	≤ 1per cent max	≥ 0.998

Table A5/1 Analytical balance verification criteria

3.4.3.10.1.3.4.2. Buoyancy Correction

The sample and reference filter weights shall be corrected for their buoyancy in air. The buoyancy correction is a function of sampling filter density, air density and the density of the balance calibration weight, and does not account for the buoyancy of the PM itself.

If the density of the filter material is not known, the following densities shall be used:

- (a) PTFE coated glass fiber filter: 2,300 kg/m3;
- (b) PTFE membrane filter: 2,144 kg/m3;
- (c) PTFE membrane filter with polymethyl pentene support ring: 920 kg/m3.

For stainless steel calibration weights, a density of 8,000 kg/m³ shall be used. If the material of the calibration weight is different, its density must be known. International Recommendation OIML R 111-1 Edition 2004(E) from International Organization of Legal Metrology on calibration weights should be followed.

The following equation shall be used:

$$m_{\rm f} = m_{\rm uncorr} \times \left(\frac{1 - \frac{\rho_{\rm a}}{\rho_{\rm w}}}{1 - \frac{\rho_{\rm a}}{\rho_{\rm f}}} \right)$$

where:

m_f is the corrected particulate sample mass, mg;

m_{uncorr} is the uncorrected particulate sample mass, mg;

ρ_a is the density of the air, kg/m³;

p_w is the density of balance calibration weight, kg/m³;

ρ_f is the density of the particulate sampling filter, kg/m³.

The density of the air ρ_a shall be calculated as follows:

$$\rho_{a} = \frac{p_{b} \times 28.836}{8.3144 \times T_{a}}$$

pb is the total atmospheric pressure, kPa;

T_a is the air temperature in the balance environment, Kelvin (K).

The chamber (or room) environment shall be free of any ambient contaminants (such as dust) that would settle on the particulate filters during their stabilisation.

Limited deviations from weighing room temperature and humidity specifications shall be allowed provided their total duration does not exceed 30 minutes in any one filter conditioning period. The weighing room shall meet the required specifications prior to personal entrance into the weighing room. No deviations from the specified conditions are permitted during the weighing operation.

3.4.3.10.1.3.4.3. The effects of static electricity shall be nullified. This may be achieved by grounding the balance through placement on an antistatic mat and neutralisation of the particulate filters prior to weighing using a Polonium neutraliser or a device of similar effect. Alternatively, nullification of static effects may be achieved through equalisation of the static charge.

3.4.3.10.1.3.4.4. A test filter shall be removed from the chamber no earlier than an hour before the test begins.

3.4.3.10.1.4. Recommended system description

Figure B.2.-2 is a schematic drawing of the recommended particulate sampling system. Since various configurations can produce equivalent results, exact conformity with this figure is not required. Additional components such as instruments, valves, solenoids, pumps and switches may be used to provide additional information and coordinate the functions of component systems. Further components that are not needed to maintain accuracy with other system configurations may be excluded if their exclusion is based on good engineering judgment.

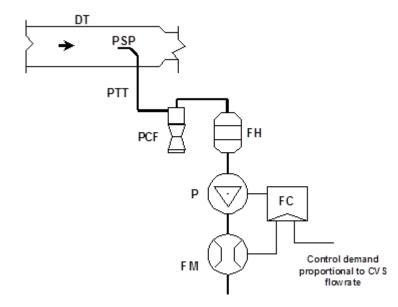


Figure B.2.-2: Particulate sampling system

A sample of the diluted exhaust gas is taken from the full flow dilution tunnel (DT) through the particulate sampling probe (PSP) and the particulate transfer tube (PTT) by means of the pump (P). The sample is passed through the particle size pre-classifier (PCF) and the filter holders (FH) that contain the particulate sampling filters. The flow rate for sampling is set by the flow controller (FC).

3.4.4. Driving schedules

The WMTC test cycles (vehicle speed patterns vs. test time) for the type I test consist of up to three parts, as laid down in Annex B.5.15. The applicable part of WMTC for each sub category shall be as per 3.2 of this section.

3.4.4.2. Vehicle speed tolerances

3.4.4.2.1. The vehicle speed tolerance at any given time on the test cycles prescribed in Annex B.5.14. is defined by upper and lower limits. The upper limit is 3.2 km/h higher than the highest point on the trace within one second of the given time. The lower limit is 3.2 km/h lower than the lowest point on the trace within one second of the given time. Vehicle speed variations greater than the tolerances (such as may occur during gear changes) are acceptable provided they occur for less than two seconds on any occasion. Vehicle speeds lower than those prescribed are acceptable provided the vehicle is operated at maximum available power during such occurrences. Figure B.2.-3 shows the range of acceptable vehicle speed tolerances for typical points.

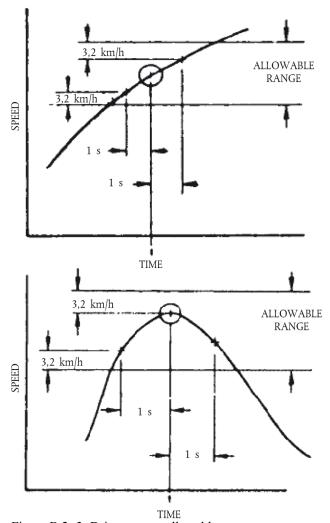


Figure B.2.-3: Drivers trace, allowable range

3.4.4.2.2. If the acceleration capability of the vehicle is not sufficient to carry out the acceleration phases or if the maximum design speed of the vehicle is lower than the prescribed cruising vehicle speed within the prescribed limits of tolerances, the vehicle shall be driven with the throttle fully open until the desired vehicle speed is reached or at the maximum design vehicle speed achievable with fully opened throttle during the time that desired vehicle speed exceeds the maximum design vehicle speed. In both cases, point 3.4.4.2.1. is not applicable. The test cycle shall be carried on normally when desired vehicle speed is again lower than the maximum design speed of the vehicle.

- 3.4.4.2.3. If the period of deceleration is shorter than that prescribed for the corresponding phase, due to the vehicle characteristics, desired vehicle speed shall be restored by a constant vehicle speed or idling period merging into succeeding constant vehicle speed or idling operation. In such cases, point 3.4.4.2.1. is not applicable.
- 3.4.4.2.4. Apart from these exceptions, the deviations of the roller speed (from which the actual vehicle speed is calculated) in comparison to the desired vehicle speed of the cycles shall meet the requirements described in point 3.4.4.2.1. If not, the test results shall not be used for further analysis and the test run shall be repeated.
- 3.4.5. Gearshift prescriptions for the WMTC prescribed for the test cycles set out in Annex B.5.15. and explained in more detail in Annex B.5.15.
 - 3.4.5.1. Test vehicles equipped with an automatic transmission
 - 3.4.5.1.1. Vehicles equipped with transfer cases, multiple sprockets, etc., shall be tested in the configuration recommended by the manufacturer for street or highway use.
 - 3.4.5.1.2. Idle modes shall be run with automatic transmissions in 'Drive' and the wheels braked. After initial engagement, the selector shall not be operated at any time during the test.
 - 3.4.5.1.3. Automatic transmissions shall shift automatically through the normal sequence of gears. The torque converter clutch, if applicable, shall operate as under real-world conditions.
 - 3.4.5.1.4. The deceleration modes shall be run in gear using brakes or throttle as necessary to maintain the desired vehicle speed.
 - 3.4.5.2. Test vehicles equipped with a semi-automatic transmission
 - 3.4.5.2.1. Vehicles equipped with semi-automatic transmissions shall be tested using the gears normally employed for driving, and the gear shift used in accordance with the instructions in the owner's manual.
 - 3.4.5.2.2. Idle modes shall be run with semi-automatic transmissions in 'Drive' and the wheels braked. After initial engagement, the selector shall not be operated at any time during the test.
 - 3.4.5.3. Test vehicles equipped with manual transmission
 - 3.4.5.3.1. Mandatory requirements
 - 3.4.5.3.1.1. Step 1 Calculation of desired vehicle speeds to shift gear
 Upshift desired vehicle speeds (v1→2 and vi→i+1) in km/h during acceleration phases shall be calculated using the following formulae:

Equation B.2.-3:

$$v_{1\to 2} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{mref})}{mref}} - 0.1) \times (s - n_{idle}) + n_{idle} \right] \times \frac{1}{n dv_1}$$

Equation B.2.-4:

$$v_{i \to i+1} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_{ii}}{mref})}{mref}}) \times (s - n_{idle}) + n_{idle} \right] \times \frac{1}{ndv_i}$$

i = 2 to ng - 1

where:

'i' is the gear number (≥ 2)

'ng' is the total number of forward gears

'P_n' is the rated power in kW

'm_{ref}'is the reference mass in kg

'n_{idle}' is the idling engine speed in min⁻¹

's' is the rated engine speed in min⁻¹

'nd v_i ' is the ratio between engine speed in min-1 and vehicle speed in km/h in gear 'i'.

Downshift desired vehicle speeds $(v_{i \rightarrow i-1})$ in km/h during cruise or deceleration phases in gears 4 (4th gear) to ng shall be calculated using the following formula:

Equation B.2.-5:

$$v_{i \to i-1} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{\mathsf{mref}})}{\mathsf{mref}}}) \times (\mathsf{s} - \mathsf{n}_{idle}) + \mathsf{n}_{idle} \right] \times \frac{1}{\mathsf{ndv}_{i-2}}$$

i = 4 to ng

where:

i is the gear number (≥ 4)

ng is the total number of forward gears

P_n is the rated power in kW

m_{ref} is the reference mass in kg

n_{idle} is the idling engine speed in min⁻¹

s is the rated engine speed in min⁻¹

 $\text{ndv}_{\text{i-2}}$ is the ratio between engine speed in min-1 and vehicle speed in km/h in gear i-2

The downshift desired vehicle speed from gear 3 to gear 2 (v $_{3\rightarrow2}$) shall be calculated using the following equation:

Equation B.2.-6:

$$v_{2\rightarrow3} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{n})}{mref}} - 0.1) \times (s - n_{idle}) + n_{idle} \right] \times \frac{1}{ndv_1}$$

where:

P_n is the rated power in kW

m_{ref} is the reference mass in kg

n_{idle} is the idling engine speed in min⁻¹

s is the rated engine speed in min⁻¹

 ndv_1 is the ratio between engine speed in min-1 and vehicle speed in km/h in gear 1.

The downshift desired vehicle speed from gear 2 to gear 1 (v $_{2\rightarrow1}$) shall be calculated using the following equation:

Equation B.2.-7:

$$v_{2\rightarrow 1} = \left[0.03 \times (s - n_{idle}) + n_{idle}\right] \times \frac{1}{ndv_2}$$

where

 ndv_2 is the ratio between engine speed in min-1 and vehicle speed in km/h in gear 2.

Since the cruise phases are defined by the phase indicator, slight vehicle speed increases could occur and it may be appropriate to apply an upshift. The upshift desired vehicle speeds $(v_{1\rightarrow 2},\ v_{2\rightarrow 3}$ and $v_{i\rightarrow i+1})$ in km/h during cruise phases shall be calculated using the following equations:

Equation B.2.-8:

$$v_{1\rightarrow 2} = \left[0.03 \times (s - n_{idle}) + n_{idle}\right] \times \frac{1}{ndv_2}$$

Equation B.2.-9:

$$v_{2\rightarrow3} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{mref})}{mref}} - 0.1) \times (s - n_{idle}) + n_{idle} \right] \times \frac{1}{ndv_1}$$

Equation B.2.-10:

$$v_{i \rightarrow i+1} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{mref})}{mref}}) \times (s - n_{idle}) + n_{idle} \right] \times \frac{1}{ndv_{i-1}}, i = 3 \text{ to ng}$$

3.4.5.3.1.2. Step 2 — Gear choice for each cycle sample

In order to avoid different interpretations of acceleration, deceleration, cruise and stop phases, corresponding indicators are added to the vehicle speed pattern as integral parts of the cycles (see tables in Annex B.5.15.).

The appropriate gear for each sample shall then be calculated according to the vehicle speed ranges resulting from equations to determine the desired vehicle speeds to shift gears of point 3.4.5.3.1.1. and the phase indicators for the cycle parts appropriate for the test vehicle, as follows:

Gear choice for stop phases:

For the last five seconds of a stop phase, the gear lever shall be set to gear 1 and the clutch shall be disengaged. For the previous part of a stop phase, the gear lever shall be set to neutral or the clutch shall be disengaged.

Gear choice for acceleration phases:

$$\begin{array}{l} \text{gear 1, if } v \leq v_{1 \rightarrow 2} \\ \text{gear 2, if } v_{1 \rightarrow 2} < v \leq v_{2 \rightarrow 3} \\ \text{gear 3, if } v_{2 \rightarrow 3} < v \leq v_{3 \rightarrow 4} \\ \text{gear 4, if } v_{3 \rightarrow 4} < v \leq v_{4 \rightarrow 5} \\ \text{gear 5, if } v_{4 \rightarrow 5} < v \leq v_{5 \rightarrow 6} \\ \text{gear 6, if } v > v_{5 \rightarrow 6} \end{array}$$

Gear choice for deceleration or cruise phases:

gear 1, if
$$v < v_{2\rightarrow 1}$$

```
gear 2, if v < v_{3\rightarrow 2}
gear 3, if v_{3\rightarrow 2} \le v < v_{4\rightarrow 3}
gear 4, if v_{4\rightarrow 3} \le v < v_{5\rightarrow 4}
gear 5, if v_{5\rightarrow 4} \le v < v_{6\rightarrow 5}
gear 6, if v \ge v_{4\rightarrow 5}
```

The clutch shall be disengaged, if:

- (a) the vehicle speed drops below 10 km/h, or
- (b) the engine speed drops below $n_{idle} + 0.03 \times (s n_{idle})$;
- (c) there is a risk of engine stalling during cold-start phase.

3.4.5.3.1.3. Step 3 — Corrections according to additional requirements

3.4.5.3.1.3.1. The gear choice shall be modified according to the following requirements:

- (a) no gearshift at a transition from an acceleration phase to a deceleration phase. The gear that was used for the last second of the acceleration phase shall be kept for the following deceleration phase unless the vehicle speed drops below a downshift desired vehicle speed;
- (b) no upshifts or downshifts by more than one gear, except from gear 2 to neutral during decelerations down to stop;
- (c) upshifts or downshifts for up to four seconds are replaced by the gear before, if the gears before and after are identical, e.g. 2 3 3 3 2 shall be replaced by 2 2 2 2 2, and 4 3 3 3 3 4 shall be replaced by 4 4 4 4 4 4.

In the cases of consecutive circumstances, the gear used longer takes over, e.g. 2 2 2 3 3 3 2 2 2 2 3 3 3 will be replaced by 2 2 2 2 2 2 2 2 2 3 3 3

If used for the same time, a series of succeeding gears shall take precedence over a series of preceding gears, e.g. 2 2 2 3 3 3 2 2 2 3 3 3 will be replaced by 2 2 2 2 2 2 2 3 3 3;

(d) no downshift during an acceleration phase.

3.4.5.3.2. Optional provisions

The gear choice may be modified according to the following provisions: The use of gears lower than those determined by the requirements described in point 3.4.5.2.1. is permitted in any cycle phase. Manufacturers' recommendations for gear use shall be followed if they do not result in gears higher than determined by the requirements of point 3.4.5.2.1.

3.4.5.3.3. Optional provisions

Note 5: The calculation programme to be found on the UN website at the following URL may be used as an aid for the gear selection: http://live.unece.org/trans/main/wp29/wp29wgs/wp29grpe/wmtc.html

Explanations of the approach and the gearshift strategy and a calculation example are given in Annex B.5.15.

3.4.5.3.4. Idle modes shall be run with manual transmissions with wheels braked.

3.4.6. Dynamometer settings

A full description of the chassis dynamometer and instruments shall be provided in accordance with Annex B.5.13. Measurements shall be taken to the accuracies specified in point 3.4.7. The running resistance force for the chassis dynamometer settings can be derived either from on-road coast-down measurements or from a running resistance table, with reference to Annexes B.5.4. or B.5.5. for a vehicle equipped with one wheel on the powered axle and to Annexes B.5.4. or B.5.6. for a vehicle with two wheels on the powered axles in case of twinned wheel vehicles.

3.4.6.1. Chassis dynamometer setting derived from on-road coast-down measurements To use this alternative, on-road coast-down measurements shall be carried out as specified in Annex B.5.5. for a vehicle equipped with one wheel on the powered axle and Annex B.5.6. for a vehicle equipped with two wheels on the powered axles in case of twinned wheel vehicles.

(Secretariat note: The Annex numbers above, to check after finalization)

3.4.6.1.1. Requirements for the equipment

The instrumentation for the roller speed (actual vehicle speed), desired vehicle speed and time measurement shall have the accuracies specified in point 3.4.7.

3.4.6.1.2. Inertia mass setting

- 3.4.6.1.2.1. The equivalent inertia mass mi for the chassis dynamometer shall be the flywheel equivalent inertia mass, mfi, closest to the sum of the mass in running order of the vehicle, the mass of the driver (75 kg). Alternatively, the equivalent inertia mass mi can be derived from Annex B.5.4.
- 3.4.6.1.2.2. If the reference mass m_{ref} cannot be equalised to the flywheel equivalent inertia mass mi, to make the target running resistance force F* equal to the running resistance force F_E (which is to be set to the chassis dynamometer), the corrected coast-down time ΔT_{E} may be adjusted in accordance with the total mass ratio of the target coastdown time $\Delta T_{\mbox{road}}$ in the following sequence:

Equation B.2.-11:

$$\Delta T_{road} = \frac{1}{3.6} (m_a + m_{r1}) \frac{2\Delta v}{F^*}$$

Equation B.2.-12:
$$\Delta T_E = \frac{1}{3.6} (m_i + m_{r1}) \frac{2\Delta v}{F_E}$$

Equation B.2.-13: $F_E = F^*$

$$F_E = F$$

Equation B.2.-14:

$$\Delta T_E = \Delta T_{road} \times \frac{m_i + m_{r1}}{m_a + m_{r1}}$$

with
$$0.95 < \frac{m_i + m_{r1}}{m_a + m_{r1}} < 1.05$$

m_{r1} may be measured or calculated, in kilograms, as appropriate. As an alternative, m_{r1} may be estimated as 4 percent of m.

For measurement accuracy, see Table B.2.-2

- 3.4.6.2. Running resistance force derived from a running resistance table or on road coast
 - 3.4.6.2.1. The chassis dynamometer may be set by the use of the running resistance table instead of the running resistance force obtained by the coast-down method. In this table method, the chassis dynamometer shall be set by the mass in running order regardless of particular vehicle characteristics.

Note 6: Care shall be taken when applying this method to vehicles with extraordinary characteristics.

- 3.4.6.2.2. The flywheel equivalent inertia mass $m_{\rm fi}$ shall be the equivalent inertia mass $m_{\rm fi}$ specified in Annexes B.5.4., B.5.5. or B.5.6. where applicable. The chassis dynamometer shall be set by the rolling resistance of the non-driven wheels (a) and the aero drag coefficient (b) specified in Annex B.5.4., or determined in accordance with the procedures set out in B.5.5. or B.5.6. respectively. (Secretariat note: The Annex numbers above, to check after finalization)
- 3.4.6.2.3. The running resistance force on the chassis dynamometer FE shall be determined using the following equation: Equation B.2.-15:

$$F_E = F_T = a + b \cdot v^2$$

3.4.6.2.4. The target running resistance force F* shall be equal to the running resistance force obtained from the running resistance table FT, because the correction for the standard ambient conditions is not necessary.

3.4.7. Measurement accuracies

Measurements shall be taken using equipment that fulfils the accuracy requirements in Table B.2.-2:

Measurement items.	At measured value.	Resolution.
a) Running resistance force, F.,	+ 2 percent.	-4
b) Vehicle speed (v1, v2).	± 1 percent.	0.2 km/h.,
c) Coast-down vehicle speed interval (2Δv = v1 — v2).	± 1 percent.	0.1 km/h.,
d) Coast-down time (Δt).	± 0.5 percent.	0.01 s.,
e) Total vehicle mass (mk).	± 0.5 percent.	1.0 kg.,
f) Wind speed.	± 10 percent.	0.1 m/s.,
g) Wind direction.		5 deg
h) Temperature.	± 1 °C.,	1 °C.
i) Barometric pressure.		0.2 kPa.,
j) Distance.	± 0.1 percent.	1 m.,
k) Time.	± 0.1 s.,	0.1 s.,

Table B.2.-2: Required accuracy of measurements

4. Test procedures

4.1. Description of the type I test

The test vehicle shall be subjected, according to its category, to test type I requirements as specified in this point 4 and comply with the requirements set out in Annex B.5.3.

4.1.1. Type I test (verifying the average emission of gaseous pollutants, PM for GDI and diesel vehicle, CO2 emissions and fuel consumption in a characteristic driving cycle)

4.1.1.1. The test shall be carried out by the method described in point 4.2. The gases shall be collected and analysed by the prescribed methods.

4.1.1.2. Number of tests

- 4.1.1.2.1. The number of tests shall be determined as shown in Figure B.2.-4. Ri1 to Ri3 describe the final measurement results for the first (No 1) test to the third (No 3) test and the gaseous pollutant, carbon dioxide emission, fuel consumption as laid down in Annex B.4. 'Lx' represents the limit values L1 to L5 as defined in the emission limits in point B.1.9.
- 4.1.1.2.2. In each test, the masses of the carbon monoxide, hydrocarbons, nitrogen oxides, carbon dioxide and the fuel consumed during the test shall be determined. The mass of particulate matter shall be determined only for vehicles equipped with a CI or a direct injected PI combustion engine.

Note for secretariat: Once the procedure for CO2 and FE is finalized, we need to revisit this flow chart and text for appropriate changes to take care of calculations of CO2, for the number of tests required e.g.---Ri1, Ri2, Ri3.

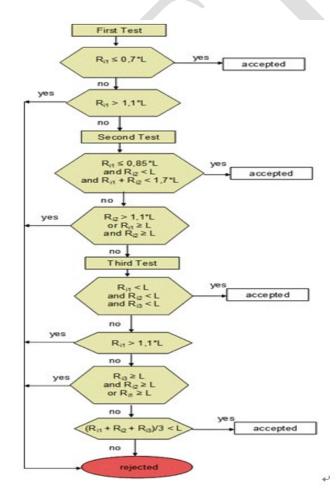


Figure B.2.-4: Flowchart for the number of type I tests Exhaust emissions may be sampled during preparation tests for type I testing or during verification tests for test types IV, VII or VIII but the results of these tests shall not be used for the purpose of exhaust emission [approval / certification] to satisfy the requirements set out in point 4.1.1.2.2.

4.2. Type I test

- 4.2.1.1. The type I test consists of prescribed sequences of dynamometer preparation, fuelling, parking, and operating conditions.
- 4.2.1.2. The test is designed to determine hydrocarbon, carbon monoxide, oxides of nitrogen, carbon dioxide, particulate matter mass emissions if applicable and fuel consumption while simulating real-world operation. The test consists of engine start-ups and vehicle operation on a chassis dynamometer, through a specified driving cycle. A proportional part of the diluted exhaust emissions is collected continuously for subsequent analysis, using a constant volume (variable dilution) sampler (CVS).
- 4.2.1.3. Except in cases of component malfunction or failure, all emission-control systems installed on or incorporated in a tested vehicle shall be functioning during all procedures.
- 4.2.1.4. Background concentrations are measured for all emission constituents for which emissions measurements are taken. For exhaust testing, this requires sampling and analysis of the dilution air.

4.2.1.5. Background particulate mass measurement

The particulate background level of the dilution air may be determined by passing filtered dilution air through the particulate filter. This shall be drawn from the same point as the particulate matter sample, if a particulate mass measurement is applicable according to point 4.1.1.2.2. One measurement may be performed prior to or after the test. Particulate mass measurements may be corrected by subtracting the background contribution from the dilution system. The permissible background contribution shall be ≤ 1 mg/km (or equivalent mass on the filter). If the background contribution exceeds this level, the default figure of 1 mg/km (or equivalent mass on the filter) shall be used. Where subtraction of the background contribution gives a negative result, the particulate mass result shall be considered to be zero.

4.2.2. Dynamometer settings and verification

4.2.2.1. Test vehicle preparation

The test vehicle shall comply with the requirements set out in Annex B.5.3.

- 4.2.2.1.1. The manufacturer shall provide additional fittings and adapters, as required to accommodate a fuel drain at the lowest point possible in the tanks as installed on the vehicle, and to provide for exhaust sample collection.
- 4.2.2.1.2. The tyre pressures shall be adjusted to the manufacturer's specifications to the satisfaction of the technical service or so that the speed of the vehicle during the road test and the vehicle speed obtained on the chassis dynamometer are equal.
- 4.2.2.1.3. The test vehicle shall be warmed up on the chassis dynamometer to the same condition as it was during the road test.
- 4.2.2.2. Chassis dynamometer preparation, if settings are derived from on-road coast-down measurements:

Before the test, the chassis dynamometer shall be appropriately warmed up to the stabilised frictional force Ff. The load on the chassis dynamometer FE is, in view of its construction, composed of the total friction loss Ff, which is the sum of the chassis dynamometer rotating frictional resistance, the tyre rolling resistance, the frictional resistance of the rotating parts in the powertrain of the vehicle and the braking force of the power absorbing unit (pau) Fpau, as in the following equation: Equation B.2.-16:

$$\mathbf{F}_E = \mathbf{F}_f + \mathbf{F}_{pau}$$

The target running resistance force F* derived from Annex B.5.4. and; for a vehicle equipped with one wheel on the powered axle Annex B.5.5. or for a vehicle with two or more wheels on the powered axles Annex B.5.6., shall be reproduced on the chassis dynamometer in accordance with the vehicle speed, i.e.:

Equation B.2.-17

$$\mathbf{F}_{E}(\mathbf{v}_{i}) = \mathbf{F}^{*}(\mathbf{v}_{i})$$

The total friction loss Ff on the chassis dynamometer shall be measured by the method in point 4.2.2.2.1. or 4.2.2.2.2.

4.2.2.2.1. Motoring by chassis dynamometer

This method applies only to chassis dynamometers capable of driving an vehicle. The test vehicle shall be driven steadily by the chassis dynamometer at the reference vehicle speed v0 with the drive train engaged and the clutch disengaged. The total friction loss Ff (v0) at the reference vehicle speed v0 is given by the chassis dynamometer force.

4.2.2.2. Coast-down without absorption

The method for measuring the coast-down time is the coast-down method for the measurement of the total friction loss Ff. The vehicle coast-down shall be performed on the chassis dynamometer by the procedure described in Annexes B.5.4. and B.5.5. for a vehicle equipped with one wheel on the powered axle and Annexes B.5.4. and B.5.6. for a vehicle equipped with two or more wheels on the powered axles, with zero chassis dynamometer absorption. The coast-down time Δt_i corresponding to the reference vehicle speed v0 shall be measured. The measurement shall be carried out at least three times, and the mean coast-down time $\overline{\Delta t}$ shall be calculated using the following equation:

Equation B.2.-18:

$$\overline{\Delta t} = \frac{1}{n} \sum_{i=1}^{n} \Delta t_{i}$$

4.2.2.2.3. Total friction loss

The total friction loss $Ff_{(v0)}$ at the reference vehicle speed v_0 is calculated using the following equation:

Equation B.2.-19:

$$F_f(\mathbf{v}_0) = \frac{1}{3.6} (\mathbf{m}_i + \mathbf{m}_{r1}) \frac{2\Delta \mathbf{v}}{\Delta \mathbf{t}}$$

4.2.2.2.4. Calculation of power-absorption unit force

The force $F_{pau}(v_0)$ to be absorbed by the chassis dynamometer at the reference vehicle speed v0 is calculated by subtracting Ff(v0) from the target running resistance force $F^*(v0)$ as shown in the following equation:

Equation B.2.-20:

$$\mathbf{F}_{pau}(\mathbf{v}_0) = \mathbf{F}^*(\mathbf{v}_0) - \mathbf{F}_f(\mathbf{v}_0)$$

4.2.2.2.5. Chassis dynamometer setting

Depending on its type, the chassis dynamometer shall be set by one of the methods described in points 4.2.2.2.5.1. to 4.2.2.2.5.4. The chosen setting shall be applied to the pollutant and CO2 emission measurements as well as fuel consumption laid down in Annex B.4.

4.2.2.5.1. Chassis dynamometer with polygonal function

In the case of a chassis dynamometer with polygonal function, in which the absorption characteristics are determined by load values at several specified vehicle speed points, at least three specified vehicle speeds, including the reference vehicle speed, shall be chosen as the setting points. At each setting point, the chassis dynamometer shall be set to the value Fpau (vj) obtained in point 4.2.2.2.4.

4.2.2.2.5.2. Chassis dynamometer with coefficient control

In the case of a chassis dynamometer with coefficient control, in which the absorption characteristics are determined by given coefficients of a polynomial function, the value of Fpau (vj) at each specified vehicle speed shall be calculated by the procedure in point 4.2.2.2.

Assuming the load characteristics to be:

Equation B.2.-21:

$$F_{pau}(v) = a \cdot v^2 + b \cdot v + c$$

where:

the coefficients a, b and c shall be determined by the polynomial regression method.

The chassis dynamometer shall be set to the coefficients a, b and c obtained by the polynomial regression method.

4.2.2.2.5.3. Chassis dynamometer with F* polygonal digital setter

In the case of a chassis dynamometer with a polygonal digital setter, where a central processor unit is incorporated in the system, F*is input directly, and $\Delta t_{\rm I}$, $F_{\rm f}$ and $F_{\rm pau}$ are automatically measured and calculated to set the chassis dynamometer to the target running resistance force: Equation B.2.-22:

$$F^* = f_0 + f_2 \cdot v^2$$

In this case, several points in succession are directly input digitally from the data set of F*j and v_j , the coast-down is performed and the coast-down time Δt_j is measured. After the coast-down test has been repeated several times, F_{pau} is automatically calculated and set at vehicle speed intervals of 0.1 km/h, in the following sequence: Equation B2.-23:

$$F^* + F_f = \frac{1}{3.6} (m_i + m_{r1}) \frac{2\Delta v}{\Delta t_i}$$

Equation B.2.-24:

$$F_f = \frac{1}{3.6} (m_i + m_{r1}) \frac{2\Delta v}{\Delta t_i} - F^*$$

Equation B.2.-25:

$$\mathbf{F}_{pau} = \mathbf{F}^* - \mathbf{F}_f$$

4.2.2.2.5.4. Chassis dynamometer with f*₀, f*₂ coefficient digital setter

In the case of a chassis dynamometer with a coefficient digital setter, where a central processor unit is incorporated in the system, the target running resistance force $F^* = f_0 + f_2 \cdot v^2$ is automatically set on the chassis dynamometer.

In this case, the coefficients f^*_0 and f^*_2 are directly input digitally; the coast-down is performed and the coast-down time Δt_i is measured. F_{pau} is automatically calculated and set at vehicle speed intervals of 0.06 km/h, in the following sequence:

Equation B.2.-26:

$$F^* + F_f = \frac{1}{3.6} (m_i + m_{r1}) \frac{2\Delta v}{\Delta t_i}$$

Equation B.2.-27:

$$F_f = \frac{1}{3.6} (m_i + m_{r1}) \frac{2\Delta v}{\Delta t_i} - F^*$$

Equation B.2.-28:

$$\mathbf{F}_{pau} = \mathbf{F}^* - \mathbf{F}_f$$

4.2.2.2.6. Dynamometer settings verification

4.2.2.2.6.1. Verification test

Immediately after the initial setting, the coast-down time Δt_E on the chassis dynamometer corresponding to the reference vehicle speed (v_0) shall be measured by the procedure set out in Annexes B.5.4. and B.5.5. for a vehicle equipped with one wheel on the powered axle and in Annexes B.5.4. and B.5.6. for a vehicle with two or more wheels on the powered axles. The measurement shall be carried out at least three times, and the mean coast-down time Δt_E shall be calculated from the results. The set running resistance force at the reference vehicle speed, F_E (v_0) on the chassis dynamometer is calculated by the following equation:

Equation B.2.-29:

$$F_E(v_0) = \frac{1}{3.6} (m_i + m_{r1}) \frac{2\Delta v}{\Delta t_E}$$

4.2.2.2.6.2. Calculation of setting error

The setting error ε is calculated by the following equation:

Equation B.2.-30:

$$\varepsilon = \frac{\left| F_E(\mathbf{v}_0) - F^*(\mathbf{v}_0) \right|}{F^*(\mathbf{v}_0)} \times 100$$

The chassis dynamometer shall be readjusted if the setting error does not satisfy the following criteria:

 $\epsilon \le 2$ percent for $v_0 \ge 50$ km/h

 $\varepsilon \le 3$ percent for 30 km/h $\le v_0 < 50$ km/h

 $\varepsilon \le 10$ percent for $v_0 < 30$ km/h

The procedure in points 4.2.2.2.6.1. to 4.2.2.2.6.2. shall be repeated until the setting error satisfies the criteria. The chassis dynamometer setting and the observed errors shall be recorded. Template record forms are provided in the template in accordance with Annex B.5.13.

4.2.2.3. Chassis dynamometer preparation, if settings are derived from a running resistance table

4.2.2.3.1. The specified vehicle speed for the chassis dynamometer

The running resistance on the chassis dynamometer shall be verified at the specified vehicle speed v. At least four specified vehicle speeds shall be verified. The range of specified vehicle speed points (the interval between the maximum and minimum points) shall extend either side of the reference vehicle speed or the reference vehicle speed range, if there is more than one reference vehicle speed, by at least Δv , as defined in Annex B.5.4. and B.5.5. for a vehicle equipped with one wheel on the powered axle and in Annex B.5.4. and B.5.6. for a vehicle with two or more wheels on the powered axles. The specified vehicle speed points, including the reference vehicle speed points, shall be at regular intervals of no more than 20 km/h apart.

4.2.2.3.2. Verification of chassis dynamometer

- 4.2.2.3.2.1. Immediately after the initial setting, the coast-down time on the chassis dynamometer corresponding to the specified vehicle speed shall be measured. The vehicle shall not be set up on the chassis dynamometer during the coast-down time measurement. The coast-down time measurement shall start when the chassis dynamometer vehicle speed exceeds the maximum vehicle speed of the test cycle.
- 4.2.2.3.2.2. The measurement shall be carried out at least three times, and the mean coast-down time Δt_E shall be calculated from the results.
- 4.2.2.3.2.3. The set running resistance force $FE(v_i)$ at the specified vehicle speed on the chassis dynamometer is calculated using the following equation:

Equation B.2.-31:

$$F_{\varepsilon}(v_{j}) = \frac{1}{3.6} \cdot m_{i} \cdot \frac{2 \Delta v}{\Delta t_{\varepsilon}}$$

4.2.2.3.2.4. The setting error ε at the specified vehicle speed is calculated using the following equation:

Equation B.2.-32:

$$\varepsilon = \frac{\left| F_E(v_j) - F_T \right|}{F_T} \times 100$$

4.2.2.3.2.5. The chassis dynamometer shall be readjusted if the setting error does not satisfy the following criteria:

 $\varepsilon \le 2$ percent for $v \ge 50$ km/h

 $\epsilon \le 3$ percent for 30 km/h $\le v \le 50$ km/h

 $\epsilon \le 10$ percent for $v \le 30$ km/h

- 4.2.2.3.2.6. The procedure described in points 4.2.2.3.2.1. to 4.2.2.3.2.5. shall be repeated until the setting error satisfies the criteria. The chassis dynamometer setting and the observed errors shall be recorded.
- 4.2.2.4. The chassis dynamometer system shall comply with the calibration and verification methods laid down in Annex B.5.6.
- 4.2.3. Calibration of analysers
 - 4.2.3.1. Analyzer calibration procedures

Each analyser shall be calibrated as specified by the instrument manufacturer or at least as often as described in Table A5/3.

Table A5/3 Instrument calibration intervals

Instrument checks	Interval	Criteria	
Gas analyser linearization (calibration)	Every 6 months	±2 per cent of reading	
Mid span	Every 6 months	±2 per cent	
CO NDIR: CO ₂ /H ₂ O interference	Monthly	-1 to 3 ppm	
NO _x converter check	Monthly	> 95 per cent	
CH ₄ cutter check	Yearly	98per cent of Ethane	
FID CH ₄ response	Yearly	See 5.4.3. 5.1.1.4.4	
FID air/fuel flow	At major maintenance	According to instrument mfr.	
NO/NO ₂ NDUV: H ₂ O, HC interference	At major maintenance	According to instrument mfr.	
Laser infrared spectrometers (modulated high resolution narrow band infrared analysers): interference check	Yearly or at major maintenance	According to instrument mfr.	
GC methods	See paragraph 7.2.	See paragraph 7.2.	
FTIR: linearity verification	Within 370 days before testing and after major maintenance	See paragraph 7.1.	
Microgram balance linearity	Yearly or at major maintenance	See paragraph 4.2.2.2.	3.10.1.3.4
PNC (particle number counter)	See paragraph 5.7.1.1.	See paragraph 5.7.1.3.	
VPR (volatile particle remover)	See paragraph 5.7.2.1.	See paragraph 5.7.2.	

Non-dispersive infrared absorption analysers shall be checked at the same intervals using nitrogen/ CO and nitrogen/ CO2 mixtures in nominal concentrations equal to 10, 40, 60, 85 and 90 percent of full scale.

- 4.2.3.2. Each normally used operating range shall be linearized by the following procedure:
 - 4.2.3.2.1. The analyser linearization curve shall be established by at least five calibration points spaced as uniformly as possible. The nominal concentration of the calibration gas of the highest concentration shall be not less than 80 per cent of the full scale.
 - 4.2.3.2.2. The calibration gas concentration required may be obtained by means of a gas divider, diluting with purified N_2 or with purified synthetic air.
 - 4.2.3.2.3. The linearization curve shall be calculated by the least squares method. If the resulting polynomial degree is greater than 3, the number of calibration points shall be at least equal to this polynomial degree plus 2.
 - 4.2.3.2.4. The linearization curve shall not differ by more than ± 2 per cent from the nominal value of each calibration gas.
 - 4.2.3.2.5. From the trace of the linearization curve and the linearization points, it is possible to verify that the calibration has been carried out correctly. The different characteristic parameters of the analyser shall be indicated, particularly:
 - (a) Scale;
 - (b) Sensitivity;
 - (c) Zero point;

- (d) Date of the linearization.
- 4.2.3.2.6. If it can be shown to the satisfaction of the responsible authority that alternative technologies (e.g. computer, electronically controlled range switch, etc.) can give equivalent accuracy, these alternatives may be used.
- 4.2.3.3. Analyser zero and calibration verification procedure
 - 4.2.3.3.1. Each normally used operating range shall be checked prior to each analysis in accordance with the following subparagraphs.
 - 4.2.3.3.1.1. The calibration shall be checked by use of a zero gas and by use of a calibration gas according to paragraph 5.1.1.2. (a),(b),(c).
 - 4.2.3.3.1.2. After testing, zero gas and the same calibration gas shall be used for rechecking according to paragraph 5.1.1.2. (e).
- 4.2.3.4. FID hydrocarbon response check procedure
 - 4.2.3.4.1. Detector response optimisation

The FID shall be adjusted as specified by the instrument manufacturer. Propane in air should be used on the most common operating range.

4.2.3.4.2. Calibration of the HC analyser

The analyser shall be calibrated using propane in air and purified synthetic air. A calibration curve as described in paragraph 5.2.2. shall be established.

4.2.3.4.3. Response factors of different hydrocarbons and recommended limits

The response factor (R_f), for a particular hydrocarbon compound is the ratio of the FID C1 reading to the gas cylinder concentration, expressed as ppm C1. The concentration of the test gas shall be at a level to give a response of approximately 80 per cent of full-scale deflection, for the operating range. The concentration shall be known to an accuracy of ± 2 per cent in reference to a gravimetric standard expressed in volume. In addition, the gas cylinder shall be pre-conditioned for 24 hours at a temperature between 293 K and 303 K (20 and 30 °C).

Response factors shall be determined when introducing an analyser into service and thereafter at major service intervals. The test gases to be used and the recommended response factors are:

Methane and purified air: 1.00 < Rf < 1.15 or 1.00 < Rf < 1.05 for

NG/biomethane-fuelled vehicles

Propylene and purified air: 0.90 < Rf < 1.00

Toluene and purified air: 0.90 < Rf < 1.00

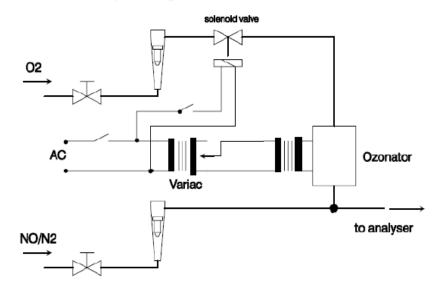
These are relative to a response factor (Rf) of 1.00 for propane and purified air.

- 4.2.3.4.4. NOx converter efficiency test procedure
 - 4.2.3.4.4.1. Using the test set up as shown in Figure A5/15 and the procedure described below, the efficiency of converters for the conversion of NO₂ into NO shall be tested by means of an ozonator as follows:
 - 4.2.3.4.4.1.1. The analyser shall be calibrated in the most common operating range following the manufacturer's specifications using zero and calibration gas (the NO content of which shall amount to approximately 80 per cent of the operating range and the NO_2

concentration of the gas mixture shall be less than 5 per cent of the NO concentration). The NOx analyser shall be in the NO mode so that the calibration gas does not pass through the converter. The indicated concentration shall be recorded.

- 4.2.3.4.4.1.2. Via a T-fitting, oxygen or synthetic air shall be added continuously to the calibration gas flow until the concentration indicated is approximately 10 per cent less than the indicated calibration concentration given in paragraph 4.2.3.4.4.1.1 above. The indicated concentration (c) shall be recorded. The ozonator shall be kept deactivated throughout this process.
- 4.2.3.4.4.1.3. The ozonator shall now be activated to generate enough ozone to bring the NO concentration down to 20 per cent (minimum 10 per cent) of the calibration concentration given in paragraph 4.2.3.4.4.1.1 above. The indicated concentration (d) shall be recorded.\
- 4.2.3.4.4.1.4. The NOx analyser shall then be switched to the NOx mode, whereby the gas mixture (consisting of NO, NO₂, O₂ and N₂) now passes through the converter. The indicated concentration (a) shall be recorded.
- 4.2.3.4.4.1.5. The ozonator shall now be deactivated. The mixture of gases described in paragraph 4.2.3.4.4.1.2 above shall pass through the converter into the detector. The indicated concentration (b) shall be recorded.

Figure A5/15 NO_x converter efficiency test configuration



- 4.2.3.4.4.1.6. With the ozonator deactivated, the flow of oxygen or synthetic air shall be shut off. The NO₂ reading of the analyser shall then be no more than 5 per cent above the figure given in paragraph 4.2.3.4.4.1.1 above.
- 4.2.3.4.4.1.7. The efficiency of the NOx converter shall be calculated using the concentrations a, b, c and d determined in paragraphs 4.2.3.4.4.1.2 through 4.2.3.4.4.1.5 above as follows:

Efficiency (per cent) =
$$\left(1 + \frac{a-b}{c-d}\right) \times 100$$

The efficiency of the converter shall not be less than 95 per cent. The efficiency of the converter shall be tested in the frequency defined in Table A5/3.

4.2.3.5. Calibration of the microgram balance

The calibration of the microgram balance used for particulate filter weighing shall be traceable to a national or international standard. The balance shall comply with the linearity requirements given in paragraph 3.4.3.10.1.3.4.1.1. The linearity verification shall be performed at least every 12 months or whenever a system repair or change is made that could influence the calibration.

Calibration and validation of the particle sampling system

Examples of calibration/validation methods are available at: http://www.unece.org/trans/main/wp29/wp29wgs/wp29grpe/pmpFCP.html.

4.2.3.5.1. Flow meter calibration

The technical service shall check that a calibration certificate has been issued for the flow meter demonstrating compliance with a traceable standard within a 12-month period prior to the test, or since any repair or change which could influence calibration.

4.2.3.5.2. Microbalance calibration

The technical service shall check that a calibration certificate has been issued for the microbalance demonstrating compliance with a traceable standard within a 12-month period prior to the test.

4.2.3.5.3. Reference filter weighing

To determine the specific reference filter weights, at least two unused reference filters shall be weighed within eight hours of, but preferably at the same time as, the sample filter weighing. Reference filters shall be of the same size and material as the sample filter.

If the specific weight of any reference filter changes by more than \pm 5 μg between sample filter weighings, the sample filter and reference filters shall be reconditioned in the weighing room and then reweighed.

This shall be based on a comparison of the specific weight of the reference filter and the rolling average of that filter's specific weights.

The rolling average shall be calculated from the specific weights collected in the period since the reference filters were placed in the weighing room. The averaging period shall be between one day and 30 days.

Multiple reconditioning and re-weighings of the sample and reference filters are permitted up to 80 hours after the measurement of gases from the emissions test.

If, within this period, more than half the reference filters meet the \pm 5 μg criterion, the sample filter weighing can be considered valid.

If, at the end of this period, two reference filters are used and one filter fails to meet the \pm 5 μg criterion, the sample filter weighing may be considered valid provided that the sum of the absolute differences between specific and rolling averages from the two reference filters is no more than 10 μg .

If fewer than half of the reference filters meet the \pm 5 μg criterion, the sample filter shall be discarded and the emissions test repeated. All reference filters shall be discarded and replaced within 48 hours.

In all other cases, reference filters shall be replaced at least every 30 days and in such a manner that no sample filter is weighed without comparison with a reference filter that has been in the weighing room for at least one day.

If the weighing room stability criteria outlined in point 3.4.3.12.1.3.4. are not met but the reference filter weighings meet the criteria listed in point 4.2.3.5.3., the vehicle manufacturer has the option of accepting the sample filter weights or voiding the tests, fixing the weighing room control system and re-running the test.

4.2.3.6. Reference gases

4.2.3.6.1. Pure gases

The following pure gases shall be available, if necessary, for calibration and operation:

Purified nitrogen: (purity: ≤ 1 ppm C1, ≤ 1 ppm CO, ≤ 400 ppm CO₂, ≤ 0.1 ppm NO);

Purified synthetic air: (purity: ≤ 1 ppm C1, ≤ 1 ppm CO, ≤ 400 ppm CO₂, ≤ 0.1 ppm NO); oxygen content between 18 and 21 percent by volume;

Purified oxygen: (purity > 99.5 percent vol. O₂);

Purified hydrogen (and mixture containing helium): (purity ≤ 1 ppm C1, ≤ 400 ppm CO₂);

Carbon monoxide: (minimum purity 99.5 percent);

Propane: (minimum purity 99.5 percent).

4.2.3.6.2. Calibration gases

The true concentration of a calibration gas shall be within ± 1 per cent of the stated value or as given below. Mixtures of gases having the following compositions shall be available with a bulk gas specification according to paragraphs 4.2.3.6.1:

- (a) C_3H_8 in synthetic air (see point 4.2.3.6.1 above);
- (b) CO in nitrogen;
- (c) CO₂ in nitrogen;
- (d) CH₄ in synthetic air
- (e) NO in Nitrogen (the amount of NO₂ contained in this calibration gas shall not exceed 5 percent of the NO content).
- (f) NO₂ in nitrogen (tolerance ± 2 per cent);

4.2.3.7. Calibration and verification of the dilution system

The dilution system shall be calibrated and verified and shall comply with the requirements of Annex B.5.7.

4.2.4. Test vehicle preconditioning

- 4.2.4.1. The test vehicle shall be moved to the test area and the following operations performed:
 - The fuel tanks shall be drained through the drains of the fuel tanks provided and charged with the test fuel requirement as specified in Annex B.5.2. to half the capacity of the tanks.
 - The test vehicle shall be placed, either by being driven or pushed, on a dynamometer and operated through the applicable test cycle as specified for the vehicle (sub-)category in Annex B.5.14. The vehicle need not be cold, and may be used to set dynamometer power.
- 4.2.4.2. Practice runs over the prescribed driving schedule may be performed at test points, provided an emission sample is not taken, for the purpose of finding the minimum throttle action to maintain the proper vehicle speed-time relationship, or to permit sampling system adjustments.
- 4.2.4.3. Within five minutes of completion of preconditioning, the test vehicle shall be removed from the dynamometer and may be driven or pushed to the soak area to be parked. The vehicle shall be stored for between six and 36 hours prior to the cold start type I test or until the engine oil temperature TO or the coolant temperature TC or the sparkplug seat/gasket temperature TP (only for air-cooled engine) equals the air temperature of the soak area within 2 °C.
- 4.2.4.4. For the purpose of measuring particulates, between six and 36 hours before testing, the applicable test cycle set out in Annex B.5.14. shall be conducted. The technical details of the applicable test cycle are laid down in Annex B.5.14. and the

applicable test cycle shall also be used for vehicle pre-conditioning. Three consecutive cycles shall be driven. The dynamometer setting shall be indicated as in point 3.4.6.

4.2.4.5. At the request of the manufacturer, vehicles fitted with indirect injection positive-ignition engines may be preconditioned with one Part One, one Part Two and two Part Three driving cycles, if applicable, from the WMTC.

In a test facility where a test on a low particulate emitting vehicle could be contaminated by residue from a previous test on a high particulate emitting vehicle, it is recommended that, in order to pre-condition the sampling equipment, the low particulate emitting vehicle undergo a 20 minute 120 km/h steady state drive cycle or at 70% of the maximum design vehicle speed for vehicles not capable of attaining 120 km/h followed by three consecutive Part Two or Part Three WMTC cycles, if feasible.

After this preconditioning, and before testing, vehicles shall be kept in a room in which the temperature remains relatively constant at 25 ± 5 °C. This conditioning shall be carried out for at least six hours and continue until the engine oil temperature and coolant, if any, are within ± 2.0 °C of the temperature of the room.

If the manufacturer so requests, the test shall be carried out not later than 30 hours after the vehicle has been run at its normal temperature.

4.2.5. Emissions tests

4.2.5.1. Engine starting and restarting

- 4.2.5.1.1. The engine shall be started according to the manufacturer's recommended starting procedures. The test cycle run shall begin when the engine starts.
- 4.2.5.1.2. Test vehicles equipped with automatic chokes shall be operated according to the instructions in the manufacturer's operating instructions or owner's manual covering choke-setting and 'kick-down' from cold fast idle. In the case of the WMTC set out in Annex B.5.14., the transmission shall be put in gear 15 seconds after the engine is started. If necessary, braking may be employed to keep the drive wheels from turning.
- 4.2.5.1.3. Test vehicles equipped with manual chokes shall be operated according to the manufacturer's operating instructions or owner's manual. Where times are provided in the instructions, the point for operation may be specified, within 15 seconds of the recommended time.
- 4.2.5.1.4. The operator may use the choke, throttle, etc. where necessary to keep the engine running.
- 4.2.5.1.5. If the manufacturer's operating instructions or owner's manual do not specify a warm engine starting procedure, the engine (automatic and manual choke engines) shall be started by opening the throttle about half way and cranking the engine until it starts.
- 4.2.5.1.6. If, during the cold start, the test vehicle does not start after ten seconds of cranking or ten cycles of the manual starting mechanism, cranking shall cease and the reason for failure to start determined. The revolution counter on the constant volume sampler shall be turned off and the sample solenoid valves placed in the 'standby' position during this diagnostic period. In addition, either the CVS blower shall be turned off or the exhaust tube disconnected from the tailpipe during the diagnostic period.
- 4.2.5.1.7. In case of an operational error, that causes a delay in the starting of sampling collection at the initiation of engine start up procedure, the test vehicle shall be rescheduled for testing from a cold start. If failure to start is caused by

vehicle malfunction, corrective action (following the unscheduled maintenance provisions) lasting less than 30 minutes may be taken and the test continued (During the corrective action sampling system shall be deactivated). The sampling system shall be reactivated at the same time cranking is started. The driving schedule timing sequence shall begin when the engine starts. If failure to start is caused by vehicle malfunction and the vehicle cannot be started, the test shall be voided, the vehicle removed from the dynamometer, corrective action taken (following the unscheduled maintenance provisions) and the vehicle rescheduled for test from a cold start. The reason for the malfunction (if determined) and the corrective action taken shall be reported.

- 4.2.5.1.8. If the test vehicle does not start during the warm start after ten seconds of cranking or ten cycles of the manual starting mechanism, cranking shall cease, the test shall be voided, the vehicle removed from the dynamometer, corrective action taken and the vehicle rescheduled for test. The reason for the malfunction (if determined) and the corrective action taken shall be reported.
- 4.2.5.1.9. If the engine 'false starts', the operator shall repeat the recommended starting procedure (such as resetting the choke, etc.)

4.2.5.2. Stalling

- 4.2.5.2.1. If the engine stalls during an idle period, it shall be restarted immediately and the test continued. If it cannot be started soon enough to allow the vehicle to follow the next acceleration as prescribed, the driving schedule indicator shall be stopped. When the vehicle restarts, the driving schedule indicator shall be reactivated.
- 4.2.5.2.2. If the engine stalls during some operating mode other than idle, the driving schedule indicator shall be stopped, the test vehicle restarted and accelerated to the vehicle speed required at that point in the driving schedule, and the test continued. During acceleration to this point, gearshifts shall be performed in accordance with point 3.4.5.
- 4.2.5.2.3. If the test vehicle will not restart within one minute, the test shall be voided, the vehicle removed from the dynamometer, corrective action taken and the vehicle rescheduled for test. The reason for the malfunction (if determined) and the corrective action taken shall be reported.

4.2.6. Drive instructions

- 4.2.6.1. In case of multi-mode vehicles, the vehicle shall be tested in the worst case based on the different tailpipe emissions. It may be in one mode or more than one mode. The decision for the worst case will be based on the documentation provided by the vehicle manufacturers and mutually agreed by the approval authority.
- 4.2.6.2. The test vehicle shall be driven with minimum throttle movement to maintain the desired vehicle speed. No simultaneous use of brake and throttle shall be permitted.
- 4.2.6.3. If the test vehicle cannot accelerate at the specified rate, it shall be operated with the throttle fully opened until the roller speed (actual vehicle speed) reaches the value prescribed for that time in the driving schedule.

4.2.7. Dynamometer test runs

- 4.2.7.1. The complete dynamometer test consists of consecutive parts as described in Annex B.5.14.
- 4.2.7.2. The following steps shall be taken for each test:
 - (a) place drive wheel of vehicle on dynamometer without starting engine;

- (b) activate vehicle cooling fan;
- (c) for all test vehicles, with the sample selector valves in the 'standby' position, connect evacuated sample collection bags to the dilute exhaust and dilution air sample collection systems;
- (d) start the CVS (if not already on), the sample pumps and the temperature recorder. (The heat exchanger of the constant volume sampler, if used, and sample lines shall be preheated to their respective operating temperatures before the test begins);
- (e) adjust the sample flow rates to the desired flow rate and set the gas flow measuring devices to zero;
 - For gaseous bag (except hydrocarbon) samples, the minimum flow rate is 0.08 litre/second;
 - For hydrocarbon samples, the minimum flame ionisation detection (FID) (or heated flame ionisation detection (HFID) in the case of methanol-fuelled vehicles) flow rate is 0.031 litre/second;
- (f) attach the flexible exhaust tube to the vehicle tailpipes;
- (g) start the gas flow measuring device, position the sample selector valves to direct the sample flow into the 'transient' exhaust sample bag, the 'transient' dilution air sample bag, turn the key on and start cranking the engine;
- (h) put the transmission in gear;
- (i) begin the initial vehicle acceleration of the driving schedule;
- (j) operate the vehicle according to the driving cycles specified in Annex B.5.14.;
- (k) at the end of part 1 or part 1 in cold condition, simultaneously switch the sample flows from the first bags and samples to the second bags and samples, switch off gas flow measuring device No 1 and start gas flow measuring device No 2;
- (l) in case of vehicles capable of running Part 3 of the WMTC, at the end of Part 2 simultaneously switch the sample flows from the second bags and samples to the third bags and samples, switch off gas flow measuring device No 2 and, start gas flow measuring device No 3;
- (m) before starting a new part, record the measured roll or shaft revolutions and reset the counter or switch to a second counter. As soon as possible, transfer the exhaust and dilution air samples to the analytical system and process the samples according to point 5., obtaining a stabilised reading of the exhaust bag sample on all analysers within 20 minutes of the end of the sample collection phase of the test;
- (n) turn the engine off two seconds after the end of the last part of the test;
- (o) immediately after the end of the sample period, turn off the cooling fan;
- (p) turn off the constant volume sampler (CVS) or critical-flow venturi (CFV) or disconnect the exhaust tube from the tailpipes of the vehicle;
- (q) disconnect the exhaust tube from the vehicle tailpipes and remove the vehicle from the dynamometer;
- (r) for comparison and analysis reasons, second-by-second emissions (diluted gas) data shall be monitored as well as the bag results.

5. Analysis of results

5.1. Type I tests

5.1.1. Exhaust emission and fuel consumption analysis

5.1.1.1. Analysis of the samples contained in the bags

The analysis shall begin as soon as possible, and in any event not later than 20 minutes after the end of the tests, in order to determine:

- the concentrations of hydrocarbons, carbon monoxide, nitrogen oxides, particulate matter if applicable and carbon dioxide in the sample of dilution air contained in bag(s) B;
- the concentrations of hydrocarbons, carbon monoxide, nitrogen oxides, carbon dioxide and particulate matter if applicable in the sample of diluted exhaust gases contained in bag(s) A.

5.1.1.2. Calibration of analysers and concentration results

The analysis of the results has to be carried out in the following steps:

- (a) prior to each sample analysis, the analyser range to be used for each pollutant shall be set to zero with the appropriate zero gas;
- (b) the analysers are set to the calibration curves by means of span gases of nominal concentrations of 70 to 100 percent of the range;
- (c) the analysers' zeroes are rechecked. If the reading differs by more than 2 percent of range from that set in (b), the procedure is repeated;
- (d) the samples are analysed;
- (e) after the analysis, zero and span points are rechecked using the same gases. If the readings are within 2 percent of those in point (c), the analysis is considered acceptable;
- (f) at all points in this section the flow-rates and pressures of the various gases shall be the same as those used during calibration of the analysers;
- (g) the figure adopted for the concentration of each pollutant measured in the gases is that read off after stabilisation on the measuring device.

5.1.1.3. Measuring the distance covered

The distance (S) actually covered for a test part shall be calculated by multiplying the number of revolutions read from the cumulative counter (see point 3.4.2.2.) by the circumference of the roller. This distance shall be expressed in km to three decimal places.

5.1.1.4. Determination of the quantity of gas emitted

The reported test results shall be computed for each test and each cycle part by use of the following formulae. The results of all emission tests shall be rounded.

5.1.1.4.1. Total volume of diluted gas (PDP)

The total volume of diluted gas, expressed in m³/cycle part, adjusted to the reference conditions of 0 °C and 101.3 kPa, is calculated by Equation B.2.-33:

$$V = \frac{V_0 \times N \times (P_a - P_i) \times 273.15}{101.3 \times (T_P + 273.15)}$$

where:

 V_0 is the volume of gas displaced by pump P during one revolution, expressed in m^3 /revolution. This volume is a function of the differences between the intake and output sections of the pump;

N is the number of revolutions made by pump P during each part of the test;

P_a is the ambient pressure in kPa;

 p_i is the average under-pressure during the test part in the intake section of pump P, expressed in kPa;

 T_p is the temperature (expressed in $^\circ C$) of the diluted gases during the test part, measured in the intake section of pump P.

5.1.1.4.2. Total volume of diluted gas (CFV)

The calibration procedure described in points B5 2.3.3. to 2.3.7..

Total volume of diluted gas is based on the flow equation for a critical-flow venturi:

$$Q_s = \frac{K_{\pi}P}{\sqrt{T}}$$

where:

 $Qs = flow in m^3/min$

Kv = calibration coefficient;

P = absolute pressure (kPa);

T = absolute temperature (K).

Gas flow is a function of inlet pressure and temperature.

$$K_{\pi} = \frac{Q_{s} \sqrt{T_{\pi}}}{P_{\pi}}$$

where

Qs = flow-rate in m^3 /min at 0 °C and 101.3 kPa;

Tv = temperature at the venturi inlet (K);

Pv = absolute pressure at the venturi inlet (kPa).

$$V = K v \int_0^{te} \frac{P v(t)}{\sqrt{T v(t)}} dt$$

te=measuring time (s)

5.1.1.4.3. Hydrocarbons (HC)

The mass of unburned hydrocarbons emitted by the exhaust of the vehicle during the test shall be calculated using the following formula:

Equation B.2.-34:

$$HC_m = \frac{1}{S} \cdot V \cdot d_{HC} \cdot \frac{HC_C}{10^6}$$

where:

HC_m is the mass of hydrocarbons emitted during the test part, in mg/km;

S is the distance defined in point 5.1.1.3.;

V is the total volume, defined in point 5.1.1.4.1.;

 d_{HC} is the density of the hydrocarbons at reference temperature and pressure (0.0 °C and 101.3 kPa);

 d_{HC}

 $=619x10^3$ mg/m³ for petrol (E0) C₁H_{1.85};

 $=631 \times 10^3 \text{mg/m}^3$ for petrol (E5) $C_1 H_{1.89} O_{0.016}$;

 $=646 \times 10^3 \text{mg/m}^3$ for petrol (E10) $C_1 H_{1.93} O_{0.033}$;

=619x103mg/m3 for diesel (B0) $C_1H_{1.86}$)

 $=622 \times 103 \text{ mg/m}$ 3 for diesel (B5/B7) C₁H_{1.86}O_{0.005}

 HC_C is the concentration of diluted gases, expressed in parts per million (ppm) of carbon equivalent (e.g. the concentration in propane multiplied by three), corrected to take account of the dilution air by the following equation:

Equation B.2.-35:

$$HC_c = HC_e - HC_d * (1 - \frac{1}{DiF})$$

where:

HC_e is the concentration of hydrocarbons expressed in parts per million (ppm) of carbon equivalent, in the sample of diluted gases collected in bag(s) A;

HC_d is the concentration of hydrocarbons expressed in parts per million (ppm) of carbon equivalent, in the sample of dilution air collected in bag(s) B;

DiF is the coefficient defined in point 5.1.1.4.7.

5.1.1.4.4. Non-methane hydrocarbon (NMHC)

5.1.1.4.4.1. For methane measurement using a GC-FID, the non-methane hydrocarbon (NMHC) concentration shall be calculated using the following equations: Equation B.2.-37:

$$NMHC_C = HC_C - \left(Rf_{CH_4} \cdot CH_{4C}\right)$$

where:

 HC_C is the concentration of hydrocarbons (HC) in the diluted exhaust gas, expressed in ppm carbon equivalent and corrected by the amount of HC contained in the dilution air, defined in point 5.1.1.4.3.

Rf_{CH4} is the FID response factor to methane as defined in point 4.2.3.4.3.

CH_{4C} is the concentration of methane (CH₄) in the diluted exhaust gas, expressed in ppm carbon equivalent, corrected to take account of the dilution air by the following equation:

Equation B.2.-38:

$$CH_{4C} = CH_{4e} - CH_{4d} \cdot \left(1 - \frac{1}{DiF}\right)$$

where:

CH_{4e} is the concentration of methane expressed in parts per million (ppm), in the sample of diluted gases collected in bag(s) A;

CH_{4d} is the concentration of methane expressed in parts per million (ppm), in the sample of dilution air collected in bag(s) B;

DiF is the coefficient defined in point 5.1.1.4.9.

5.1.1.4.4.2. The mass of non-methane hydrocarbon (NMHC) emitted by the exhaust of the vehicle during the test shall be calculated using the following equation:

Equation B.2.-36:

$$NMHC_m = \frac{1}{S} \cdot V \cdot d_{NMHC} \cdot \frac{NMHC_C}{10^6}$$

where:

 $NMHC_m$ is the mass of non-methane hydrocarbon (NMHC) emitted during the test part, in mg/km;

S is the distance defined in point 5.1.1.3.;

V is the total volume, defined in point 5.1.1.4.1. and 5.1.1.4.2.;

 d_{NMHC} is the density for NMHC which shall be equal to that of hydrocarbons at reference temperature and pressure (0.0 °C and 101.3 kPa) and is fuel-dependent;

 $\mathrm{NMHC}_{\mathrm{C}}$ is the corrected concentration of the diluted exhaust gas, expressed in ppm carbon equivalent.

- 5.1.1.4.4.3. For methane measurement using an NMC-FID, the calculation of NMHC depends on the calibration gas/method used for the zero/calibration adjustment. The FID used for the HC measurement (without NMC) shall be calibrated with propane/air in the normal manner. For the calibration of the FID in series with an NMC, the following methods are permitted:
 - (a) The calibration gas consisting of propane /air bypasses the NMC;
 - (b) The calibration gas consisting of methane/air passes through the NMC.

It is highly recommended to calibrate the methane FID with methane/air through the NMC.

In case (a), the concentration of CH 4 and NMHC shall be calculated using the following equations:

Equation B.2.39:

$$CH_{4C} = \frac{HC_{(W/NMC)C} - HC_{(W/ONMC)C} \times (1 - E_E)}{R_f \times (E_E - E_M)}$$

Equation B.2.40:

$$NMHC_C = \frac{HC_{(W/ONMC)C} \times (1 - E_M) - HC_{(W/NMC)C}}{E_E - E_M}$$

In case (b), the concentration of CH₄ and NMHC shall be calculated using the following equations:

Equation B.2.41:

$$CH_{4C} = \frac{HC_{(W/NMC)C} \times R_f \times \left(1 - E_M\right) - HC_{(W/ONMC)C} \times \left(1 - E_E\right)}{R_f \times \left(E_E - E_M\right)}$$

Equation B.2.42:

$$NMHC_C = \frac{HC_{(W/ONMC)C} \times (1 - E_M) - HC_{(W/NMC)C} \times R_f \times (1 - E_M)}{E_E - E_M}$$

where:

Rf is the methane response factor as defined in point 4.2.3.4.3.;

 E_M is the methane efficiency as determined per paragraph 5.1.1.4.4.3.2. below; E_E is the ethane efficiency as determined per paragraph 5.1.1.4.4.3.3. below.

If Rf < 1.05, it may be omitted in the equations B.2. 39, 41 and 42.

HC_{(w/NMC)C} is the HC concentration with sample gas flowing through the NMC, ppm C,corrected to take account of the dilution air by the following equation B.2.43:

HC_{(w/oNMC)C} is the HC concentration with sample gas bypassing the NMC, ppm C,corrected to take account of the dilution air by the following equation B.2.-44:

Equation B.2.-43:

$$HC_{(W/NMC)C} = HC_{(W/NMC)e} - HC_{(W/NMC)d} \cdot \left(1 - \frac{1}{DiF}\right)$$

where:

 $HC_{(W/NMC)e}$ is the concentration of HC expressed in parts per million (ppm), in the sample of diluted gases flowing through the NMC, collected in bag(s) A;

HCH_{(W/NMC)d} is the concentration of HC expressed in parts per million (ppm), in the sample of dilution air flowing through the NMC, collected in bag(s) B; DiF is the coefficient defined in point 5.1.1.4.9.

Equation B.2.-44:

$$HC_{(W/oNMC)C} = HC_{(W/oNMC)e} - HC_{(W/oNMC)d} \cdot \left(1 - \frac{1}{DiF}\right)$$

where:

 $HC_{(W/oNMC)e}$ is the concentration of HC expressed in parts per million (ppm), in the sample of diluted gases bypassing the NMC, collected in bag(s) A;

 $HCH_{(W/oNMC)d}$ is the concentration of HC expressed in parts per million (ppm), in the sample of dilution air bypassing the NMC, collected in bag(s) B;

DiF is the coefficient defined in point 5.1.1.4.9.

5.1.1.4.4.3.1. Conversion efficiencies of the non-methane cutter (NMC)

The NMC is used for the removal of the non-methane hydrocarbons from the sample gas by oxidizing all hydrocarbons except methane. Ideally, the conversion for methane is 0 per cent, and for the other hydrocarbons represented by ethane is 100 per cent. For the accurate measurement of NMHC, the two efficiencies shall be determined and used for the calculation of the NMHC emission.

5.1.1.4.4.3.2. Methane conversion efficiency

The methane/air calibration gas shall be flowed to the FID through the NMC and bypassing the NMC and the two

concentrations recorded. The efficiency shall be determined using the following equations:

Equation B.2.45

$$E_{\scriptscriptstyle M} = 1 - \frac{HC_{\scriptscriptstyle CH_4(W/NMC)C}}{HC_{\scriptscriptstyle CH_4(W/ONMC)C}}$$

where:

 $HC_{CH4(w/NMC)C}$ is the HC concentration with CH_4 flowing through the NMC, ppm C;

HC_{CH4(w/oNMC)C} is the HC concentration with CH₄ bypassing the NMC, ppm C.

5.1.1.4.4.3.3. Ethane conversion efficiency

The ethane/air calibration gas shall be flowed to the FID through the NMC and bypassing the NMC and the two concentrations recorded. The efficiency shall be determined using the following equations:

Equation B.2.46

$$E_{E} = 1 - \frac{HC_{C_{2}H_{6}(W/NMC)C}}{HC_{C_{2}H_{6}(W/ONMC)C}}$$

where:

 $HC_{C2H6(w/NMC)C}$ is the HC concentration with C_2H_6 flowing through the NMC, ppm C;

 $HC_{C2H6(w/oNMC)C}$ is the HC concentration with C_2H_6 bypassing the NMC in ppm C.

If the ethane conversion efficiency of the NMC is 0.98 or above, E_E shall be set to 1 for any subsequent calculation.

5.1.1.4.4.3.4. If the methane FID is calibrated through the cutter, then E_{M} shall be 0.

Equation B.2.41 from above becomes:

Equation B.2.47

$$CH_{4C} = HC_{(W/NMC)C}$$

Equation B.2.42 from above becomes:

Equation B.2.48

$$NMHC_C = HC_{(W/ONMC)C} - HC_{(W/NMC)C} \times R_f$$

5.1.1.4.5. Carbon monoxide (CO)

The mass of carbon monoxide emitted by the exhaust of the vehicle during the test shall be calculated using the following formula:

Equation B.2.-37:

$$CO_m = \frac{1}{S} \cdot V \cdot d_{CO} \cdot \frac{CO_C}{10^6}$$

where

 CO_{m} is the mass of carbon monoxide emitted during the test part, in mg/km;

S is the distance defined in point 5.1.1.3.;

V is the total volume defined in point 5.1.1.4.1.;

 d_{CO} is the density of the carbon monoxide, $d_{CO} = 1.25 \cdot 10^6$ mg/m³ at reference temperature and pressure (0 °C and 101.3 kPa);

 ${\rm CO_c}$ is the concentration of diluted gases, expressed in parts per million (ppm) of carbon monoxide, corrected to take account of the dilution air by the following equation: Equation B.2.-38:

$$CO_c = CO_e - CO_d \cdot \left(1 - \frac{1}{DiF}\right)$$

CO_e is the concentration of carbon monoxide expressed in parts per million (ppm), in the sample of diluted gases collected in bag(s) A;

CO_d is the concentration of carbon monoxide expressed in parts per million (ppm), in the sample of dilution air collected in bag(s) B;

DiF is the coefficient defined in point 5.1.1.4.9.

5.1.1.4.6. Nitrogen oxides (NOx)

The mass of nitrogen oxides emitted by the exhaust of the vehicle during the test shall be calculated using the following formula:

Equation B.2.-39:

$$NO_{Xm} = \frac{1}{S} \cdot V \cdot d_{NO_2} \cdot \frac{NO_{XC} \cdot K_h}{10^6}$$

NO_{xm} is the mass of nitrogen oxides emitted during the test part, in mg/km;

S is the distance defined in point 5.1.1.3.;

V is the total volume defined in point 5.1.1.4.1.;

d_{NO2} is the density of the nitrogen oxides in the exhaust gases, assuming that they will be in the form of nitric oxide, $d_{NO_2}=2.05\cdot10^6$ mg/m³ at reference temperature and pressure (0 °C and 101.3 kPa);

NO_{xc} is the concentration of diluted gases, expressed in parts per million (ppm), corrected to take account of the dilution air by the following equation: Equation B.2.-40:

$$NO_{xc} = NO_{xe} - NO_{xd} \cdot \left(1 - \frac{1}{DiF}\right)$$

where:

NO_{xe} is the concentration of nitrogen oxides expressed in parts per million (ppm) of nitrogen oxides, in the sample of diluted gases collected in bag(s) A;

NO_{xd} is the concentration of nitrogen oxides expressed in parts per million (ppm) of nitrogen oxides, in the sample of dilution air collected in bag(s) B;

DiF is the coefficient defined in point 5.1.1.4.7.;

 K_b is the humidity correction factor, calculated using the following formula:

Equation B.2.-41:

$$K_h = \frac{1}{1 - 0.0329 \cdot (H - 10.7)}$$

H is the absolute humidity in g of water per kg of dry air:

Equation B.2.-42:

$$H = \frac{6.2111 \cdot U \cdot p_d}{p_a - p_d \cdot \frac{U}{100}}$$

where:

U is the relative humidity as a percentage;

p_d is the saturated pressure of water at the test temperature in kPa; p_a is the atmospheric pressure in kPa.

5.1.1.4.7. Particulate matter mass

Particulate emission Mp (mg/km) is calculated by means of the following equation:

Equation 2-43:

$$\boldsymbol{M}_{p} = \frac{\left(\boldsymbol{V}_{mix} + \boldsymbol{V}_{ep}\right) \cdot \boldsymbol{P}_{e}}{\boldsymbol{V}_{ep} \cdot \boldsymbol{S}}$$

where exhaust gases are vented outside the tunnel;

Equation B.2.-43:

$$M_p = \frac{V_{mix} \cdot P_e}{V_{en} \cdot S}$$

where exhaust gases are returned to the tunnel;

where.

 V_{mix} = volume V of diluted exhaust gases under standard conditions;

V_{ep} = volume of exhaust gas flowing through particulate filter under standard conditions;

 P_e = particulate mass collected by filter(s);

S = is the distance defined in point 5.1.1.3.;

 M_p = particulate emission in mg/km.

Where correction for the particulate background level from the dilution system has been used, this shall be determined in accordance with point 4.2.1.5. In this case, the particulate mass (mg/km) shall be calculated as follows:

Equation B.2.-44:

$$M_{p} = \left\lceil \frac{P_{e}}{V_{ep}} - \left(\frac{P_{a}}{V_{ap}} \cdot \left(1 - \frac{1}{\textit{DiF}} \right) \right) \right\rceil \cdot \frac{\left(V_{mix} + V_{ep} \right)}{\textit{S}}$$

where exhaust gases are vented outside the tunnel;

Equation B.2.-45:

$$\mathbf{M}_{p} = \left[\frac{\mathbf{P}_{e}}{\mathbf{V}_{ep}} - \left(\frac{\mathbf{P}_{a}}{\mathbf{V}_{ap}} \cdot \left(1 - \frac{1}{\mathbf{D}iF} \right) \right) \right] \cdot \frac{\mathbf{V}_{mix}}{\mathbf{S}}$$

where exhaust gases are returned to the tunnel;

where

V_{ap} = volume of tunnel air flowing through the background particulate filter under standard conditions;

P_a = particulate mass collected by background filter;

DiF = dilution factor as determined in point 5.1.1.4.9.

Where application of a background correction results in a negative particulate mass (in mg/km), the result shall be considered to be zero mg/km particulate mass.

5.1.1.4.8. Carbon dioxide (CO₂)

The mass of carbon dioxide emitted by the exhaust of the vehicle during the test shall be calculated using the following formula:

Equation B.2.-46:

$$CO_{2m} = \frac{1}{S} \cdot V \cdot d_{co_2} \cdot \frac{CO_{2c}}{10^2}$$

where:

CO_{2m} is the mass of carbon dioxide emitted during the test part, in g/km;

S is the distance defined in point 5.1.1.3.;

V is the total volume defined in point 5.1.1.4.1.;

 d_{CO2} is the density of the carbon monoxide, $d_{CO2} = 1.964 \cdot 10^3$ g/m³ at reference temperature and pressure (0 °C) and 101.3 kPa);

CO_{2c} is the concentration of diluted gases, expressed as a percentage of carbon dioxide equivalent, corrected to take account of the dilution air by the following equation: Equation B.2.-47:

$$CO_{2c} = CO_{2e} - CO_{2d} \times (1 - \frac{1}{piF})$$

where:

CO_{2e} is the concentration of carbon dioxide expressed as a percentage of the sample of diluted gases collected in bag(s) A;

CO_{2d} is the concentration of carbon dioxide expressed as a percentage of the sample of dilution air collected in bag(s) B;

DiF is the coefficient defined in point 5.1.1.4.9.

5.1.1.4.9. Dilution factor (DiF)

The dilution factor is calculated as follows:

For each reference fuel, except hydrogen:

Equation B.2.-48:

$$DiF = \frac{X}{C_{CO2} + (C_{HC} + C_{CO}) \cdot 10^{-4}}$$

For a fuel of composition $C_xH_yO_z$, the general formula is:

Equation B.2.-49:

$$X = 100 \cdot \frac{x}{x + \frac{y}{2} + 3.76 \cdot \left(x + \frac{y}{4} - \frac{z}{2}\right)}$$

For the reference fuels contained in annex B.5.2., the values of 'X' are as follows:

Fuel	X
Petrol(E0~E10)	13.4
Diesel(B5) / (B7)	13.5

Table B.2.-3: Factor 'X' in formulae to calculate DiF In these equations:

 C_{CO2} = concentration of CO_2 in the diluted exhaust gas contained in the sampling bag, expressed in percent by volume,

 C_{HC} = concentration of HC in the diluted exhaust gas contained in the sampling bag, expressed in ppm carbon equivalent,

 C_{CO} = concentration of CO in the diluted exhaust gas contained in the sampling bag, expressed in ppm,

5.1.1.5. Weighting of type I test results

5.1.1.5.1. With repeated measurements (see point 4.1.1.2.), the pollutant (mg/km), and CO₂ (g/km) emission results obtained by the calculation method described in point 5.1.1. and fuel consumption determined according to Section B.4. are averaged for each cycle part.

5.1.1.6. Weighting of WMTC results

The (average) result of Part 1 or Part 1 reduced vehicle speed is called R_1 , the (average) result of Part 2 or Part 2 reduced vehicle speed is called R_2 and the (average) result of Part 3 or part 3 reduced vehicle speed is called R_3 . Using these emission (mg/km) and fuel consumption (litres/100 km) results, the final result R_F , depending on the vehicle category as defined in point 5.1.1.6.1., shall be calculated using the following equations:

Equation B.2.-52:

 $R_F = R1.w1 + R1.w2$

Equation B.2.-53:

$$R_{\mathbf{F}} = R_1 \cdot w_1 + R_2 \cdot w_2$$

where:

 w_1 = weighting factor cold phase w_2 = weighting factor warm phase Equation B.2.-54:

$$R_{\mathbf{F}} = R_1 \cdot w_1 + R_2 \cdot w_2 + R_3 \cdot w_3$$

where:

 w_n = weighting factor phase n (n=1, 2 or 3)

5.1.1.6.1. For each gaseous pollutant, PM and carbon dioxide emission the weightings shown in Tables B.2.-4 shall be used.

Vehicle Class	Equation	Weighting Factor
0		$w_1 = 0.50$
		$w_2 = 0.50$
1	B.2 - 52	$w_1 = 0.30$
		$w_2 = 0.70$
2		$w_1 = 0.30$
		$w_2 = 0.70$
3		$w_1 = 0.25$
		$w_2 = 0.50$
		$w_3 = 0.25$

Table B.2.-4: Type I test cycles (also applicable for test Types VII and VIII), applicable weighting equations and weighting factors.

6. Records required

- 6.1. The following information shall be recorded with respect to each test:
 - (a) test number;
 - (b) vehicle, system or component identification;
 - (c) date and time of day for each part of the test schedule;
 - (d) instrument operator;
 - (e) driver or operator;
 - (f) test vehicle: make, vehicle identification number, model year, drivetrain / transmission type, odometer reading at initiation of preconditioning, engine displacement, engine family, emission-control system, recommended engine speed at idle, nominal fuel tank capacity, inertial loading, reference mass recorded at 0 kilometre, and drive-wheel tyre pressure;

- (g) dynamometer serial number: as an alternative to recording the dynamometer serial number, a reference to a vehicle test cell number may be used, with the advance approval of the Administration, provided the test cell records show the relevant instrument information;
- (h) all relevant instrument information, such as tuning, gain, serial number, detector number, range. As an alternative, a reference to a vehicle test cell number may be used, with the advance approval of the Administration, provided test cell calibration records show the relevant instrument information;
- (i) recorder charts: identify zero point, span check, exhaust gas, and dilution air sample traces;
- (j) test cell barometric pressure, ambient temperature and humidity; Note 7: A central laboratory barometer may be used; provided that individual test cell barometric pressures are shown to be within ± 0.1 percent of the barometric pressure at the central barometer location.
- (k) pressure of the mixture of exhaust and dilution air entering the CVS metering device, the pressure increase across the device, and the temperature at the inlet. The temperature shall be recorded continuously or digitally to determine temperature variations;
- (l) the number of revolutions of the positive displacement pump accumulated during each test phase while exhaust samples are being collected. The number of standard cubic meters metered by a critical-flow venturi (CFV) during each test phase would be the equivalent record for a CFV-CVS;
- (m) the humidity of the dilution air.
 - Note 8: If conditioning columns are not used, this measurement can be deleted. If the conditioning columns are used and the dilution air is taken from the test cell, the ambient humidity can be used for this measurement:
 - (n) the driving distance for each part of the test, calculated from the measured roll or shaft revolutions;
 - (o) the actual roller vehicle speed pattern for the test;
 - (p) the gear use schedule for the test;
 - (q) the emissions results of the type I test for each part of the test and the total weighted test results;
 - (r) the second-by-second emission values of the type I tests, if deemed necessary;
 - (s) the emissions results of the type II test (see Annex B.3.).

B.3. Text of the regulation, Test Type II, Tailpipe Emissions at (increased) Idle and at Free Acceleration

1. Introduction

This section describes the procedure for type II testing designed to ensure the on- road pollution under control requisite measurement of emissions during for in-use vehicle roadworthiness testing. The purpose of the requirements laid down in this section is to demonstrate that the [approved] / [certified] vehicle complies with the minimum requirements with regard to in-use vehicle roadworthiness testing.

2. Scope

- 2.1. During the environmental performance [approval] / [certification] process, it shall be demonstrated to the technical service and responsible authority that the vehicles shall comply with the test type II requirements prescribed in regional regulation of contracting parties applicable at the time of certification.
- 2.2. Vehicles equipped with a propulsion unit type of which a positive ignition combustion engine forms part shall be subject only to a type II emission test as set out in points 3., 4., 5. and 6.
- 2.3. Vehicles equipped with a propulsion unit type of which a compression ignition combustion engine forms part shall be subject only to a type II free acceleration emission test as set out in points 3., 7. and 8. In this case point 3.8. is not applicable.

3. General conditions of type II emission testing

- 3.1. In general practice, Type II test shall be carried out immediately after Type I test, if not, a visual inspection of any emission-control equipment shall be conducted prior to start of the type II emission test in order to check that the vehicle is complete, in a satisfactory condition and that there are no leaks in the fuel, air supply or exhaust systems. The test vehicle shall be properly maintained and used.
- 3.2. The fuel used to conduct the type II test shall be the reference fuel applicable for Type I test.
- 3.3. During the test, the environmental temperature shall be between 20 °C and 30 °C.
- 3.4. In the case of vehicles with manually-operated or semi-automatic-shift transmission, the test type II test shall be carried out with the gear lever in the 'neutral' position and the clutch engaged.
- 3.5. In the case of vehicles with automatic-shift transmission, the idle type II test shall be carried out with the gear selector in either the 'neutral' or the 'park' position. Where an automatic clutch is also fitted, the driven axle shall be lifted up to a point at which the wheels can rotate freely.
- 3.6. The type II emission test shall be conducted immediately after the type I emission test. In any other event, if type-II test is required to be conducted independently of Type-I test, the vehicle shall be warmed up until one of the following conditions is satisfied:
 - a) conditions at the end of type 1 test or, if not feasible,
 - b) conditions according to ISO 17479 or, if not feasible,
 - c) lubricant temperature of at least 70°C, or
 - d) minimum of 600 seconds of continuous driving under normal traffic conditions.
- 3.7. The exhaust outlets shall be provided with an air-tight extension, so that the sample probe used to collect exhaust gases may be inserted at least 60 cm into the exhaust outlet without increasing the back pressure of more than 125 mm H2O and without disturbing operation of the vehicle. This extension shall be so shaped as to avoid any appreciable dilution of exhaust gases in the air at the location of the sample probe. Where a vehicle is equipped with an exhaust system with multiple outlets, either these shall be joined to a common pipe or the

- measured pollutants carbon monoxide content shall be collected from each of them and an arithmetical average taken.
- 3.8. The emission test equipment and analysers to perform the type II testing shall be regularly calibrated and maintained. A flame ionisation detection or nondispersive infrared (NDIR) analyser may be used for measuring hydrocarbons.
- 3.9. For vehicles equipped with a stop-start system, the manufacturer shall provide a type II test 'service mode' that makes it possible to inspect the vehicle for this roadworthiness test on a running fuel-consuming engine, in order to determine its performance in relation to the data collected. Where this inspection requires a special procedure, this shall be detailed in the service manual (or equivalent media). That special procedure shall not require the use of special equipment other than that provided with the vehicle.

4. Test type II – description of test procedure to measure tailpipe emissions at (increased) idle and free acceleration

- 4.1. The possible positions of the adjustment components shall be limited by any of the following:
 - 4.1.1. The larger of the following two values:
 - (a) the lowest idling engine speed which the engine can reach;
 - (b) the engine speed recommended by the manufacturer, minus 100 revolutions per minute;
 - 4.1.2 The smallest of the following three values:
 - (a) the highest rotation speed which the crankshaft of the engine can attain by activation of the idling engine speed components;
 - (b) the rotation speed recommended by the manufacturer, plus 250 revolutions per minute:
 - (c) the cut-in rotation speed of automatic clutches.
- 4.2 Settings incompatible with the correct running of the engine shall not be adopted as measurement settings. In particular, if the engine is equipped with several carburettors, all the carburettors shall have the same setting.
- 4.3 The following parameters shall be measured and recorded at normal idling engine speed and at high idle engine speed, at the choice of CP:
 - (a) the carbon monoxide (CO) content by volume of the exhaust gases emitted (in vol%);
 - (b) the carbon dioxide (CO2) content by volume of the exhaust gases emitted (in vol%);
 - (c) hydrocarbons (HC) in ppm;
 - (d) the oxygen (O2) content by volume of the exhaust gases emitted (in vol%) or lambda, as chosen by the manufacturer;
 - (e) the engine speed during the test, including any tolerances;
 - (f) the engine oil temperature at the time of the test. Alternatively, for liquid cooled engines, the coolant temperature shall be acceptable. Alternatively for vehicles with air cooling the sparkplug seat/gasket temperature (TP) shall be acceptable.
- 4.3.1 With respect to the parameters under point 4.3. (d), the following shall apply:
- 4.3.1.1 the measurement shall only be conducted at high idle engine speed
 - 4.3.1.2 vehicles in the scope of this measurement are only those equipped with a closed loop fuel system;
 - 4.3.1.3 exemptions for vehicle with:
 - 4.3.1.3.1 engines equipped with a mechanically-controlled (spring, vacuum) secondary air system;
 - 4.3.1.3.2 two-stroke engines operated on a mix of fuel and lubrication oil.

5. CO concentration calculation in the type II idle test

- 5.1 The CO (C_{CO}) and CO_2 (C_{CO2}) concentration shall be determined from the measuring instrument readings or recordings, by use of appropriate calibration curves.
- 5.2 The corrected concentration for carbon monoxide is:

Equation B.3.-1, for 4-Stroke vehicles:

$$C_{COcorr} = 15 \times \frac{C_{CO}}{C_{CO} + C_{CO}}$$

Equation B.3.-2, for 2-Stroke vehicles:

$$C_{COcorr} = 10 \times \frac{C_{CO}}{C_{CO} + C_{CO_2}}$$

 c_{CO} is the measured concentration of carbon monoxide, in vol. %;

c_{CO2} is the measured concentration of carbon dioxide, in vol. %;

 $c_{\mbox{\tiny COcorr}}$ is the corrected concentration for carbon monoxide, in vol. %;

 \mathbf{c}_{HC} is the measured concentration of hydrocarbon, in vol. ppm;

c_{HCcorr} is the corrected concentration for hydrocarbon, in vol. ppm, expressed by methane CH4 equivalent;

a is 1,8 when concentration of hydrocarbon is measured by NDIR (Non-Dispersion Infra Red), and a is 1 when the concentration of hydrocarbon is measured by FID (Flame Ionization Detector);

b is *m* when the concentration of hydrocarbon is expressed by ppm Cm (for example *b* is 6 for n-hexane C6H14 equivalent *or b* is 1 for methane C1H4 equivalent).

- 5.3 The C_{CO} concentration (see point 5.1.) shall be measured in accordance with the formula in point 5.2. and does not need to be corrected if the total of the concentrations measured ($C_{CO} + C_{CO2}$) is at least:
 - (a) for petrol (E5): 15%;

6. Fail criteria test type II for vehicles equipped with a PI combustion engine

6.1 The test shall only be regarded as failed if the reported values exceed the limit values prescribed in the regulation of the contracting parties

7. Test type II – free acceleration test procedure

- 7.1. The exhaust gas opacity shall be measured during free acceleration (no load from idle up to cut-off engine speed) with gear lever in neutral and clutch engaged.
- 7.2. Vehicle preconditioning:

Vehicles may be tested without preconditioning although for safety reasons checks should be made that the engine is warm and in a satisfactory mechanical condition. The following precondition requirements shall apply:

7.2.1. The engine shall be fully warm, for instance the engine oil temperature measured by a probe in the oil level dipstick tube to be at least 70°C, or normal operating temperature if lower, or the engine block temperature measured by the level of infrared radiation to be at least an equivalent temperature. If, owing to vehicle configuration, this measurement is

- impractical, the establishment of the engine's normal operating temperature may be made by other means for example by the operation of the engine cooling fan;
- 7.2.2. The exhaust system shall be purged by at least three free acceleration cycles or by an equivalent method;
- 7.2.3. For vehicles equipped with continuously variable transmission (CVT) and automatic clutch, the driven wheels may be lifted from the ground;
- 7.2.4. For engines with safety limits in the engine control (e.g. max. 1500 rpm without running wheels or without gear), this maximum engine speed shall be reached.

7.3. Test procedure

The following test procedure shall be conducted:

- 7.3.1. The combustion engine and any turbocharger or super-charger fitted shall be running at idle before the start of each free acceleration test cycle;
- 7.3.2. To initiate each free acceleration cycle, the throttle shall be fully applied gradually but not violently to reach full throttle operating condition within 5 seconds quickly and continuously (in less than one second) but not violently, so as to obtain maximum delivery from the Fuel injection pump;
- 7.3.3. During each free acceleration cycle, the engine shall reach cut-off engine speed or, for vehicles with automatic transmissions, the engine speed specified by the manufacturer or if this data is not available then two thirds of the cut-off engine speed, before the throttle is released. This could be checked, for instance, by monitoring engine speed or by allowing a sufficient time to elapse between initial throttle depression and release, which should be at least Five seconds elapsing between initial throttle depression and release.
- 7.3.4. The average concentration level of the particulate matter opacity (in m-1) measured in the exhaust flow (opacity) for the 3 consecutive free acceleration test shall be measured during five free acceleration tests taken for decision making. The time duration between the two consecutive free accelerations tests shall be between 5-20 s.

8. Fail criteria test type II for vehicles equipped with a CI combustion engine

8.1. The test shall only be regarded as failed if the arithmetic means of at least the last three free acceleration cycles are in excess of the limit value as prescribed in the regulation of the contracting parties. This may be calculated by ignoring any measurement that departs significantly from the measured mean, or the result of any other statistical calculation that takes account of the scattering of the measurements.

B.4. Text of the regulation, test type VII, energy efficiency

1. Introduction

- 1.1. This section sets out requirements with regard to energy efficiency of vehicles, in particular with respect to the measurements of CO2 emissions and fuel consumption.
- 1.2. The requirements laid down in this section apply to the following tests of vehicles equipped with associated powertrain configurations:
 - a) the measurement of the emission of carbon dioxide (CO2) and fuel consumption;
- 1.3. A standardised method for measuring vehicles' energy efficiency (fuel consumption and carbon dioxide emissions) is necessary to ensure that customers and users are supplied with objective and precise information.

2. Specification and tests

2.1. General

The components liable to affect CO2 emissions and fuel consumption shall be so designed, constructed and assembled as to enable the vehicle, in normal use, despite the vibrations to which it may be subjected, to comply with the provisions of this section. The test vehicles shall be properly maintained and used.

- 2.2. Description of tests for vehicles powered by a combustion engine only
 - 2.2.1. The emissions of CO2 and fuel consumption shall be measured according to the test procedure described in Annex B.4.1. The test procedure, test fuel,

conditioning of vehicle, other requirements, etc, are to be followed for Type VII test same as for Type I test described in Section B2.

- 2.2.2.For CO2 emissions, the test results shall be expressed in grams per kilometre (g/km) rounded to the nearest one decimal place.
- 2.2.3. Fuel consumption values shall be expressed in terms of both litres per 100 km and also kilometer per litre and their values shall be rounded off to two decimals and one decimal respectively. The values shall be calculated according to point 1.4.3. of Annex B.4.1. by the carbon balance method, using the measured emissions of CO2 and the other carbon-related emissions (CO and HC).
- 2.2.4. The appropriate reference fuels as set out in Annex B.5.2. shall be used for testing.

For the purpose of the calculation referred in point 2.2.3., the fuel consumption shall be expressed in appropriate units and the following fuel characteristics shall be used:

- (a) density: measured on the test fuel according to ISO 3675:1998 or an equivalent method. For petrol and diesel fuel, the density measured at 15 °C and 101.3 kPa shall be used
- (b) hydrogen-carbon ratio: fixed values will be used, as follows:

 $C_{1:1.85} O_{0.0}$ for E0 petrol;

 $C_{1:1.89} O_{0.016}$ for E5 petrol;

 $C_{1:1.93} O_{0.033}$ for E10 petrol;

 $C_{1:1.80} O_{0.0}$ for B0 diesel;

C_{1:1.86} O_{0.005} for B5/B7 diesel

2.3. Interpretation of test results

- 2.3.1.The CO2 value or the value of fuel consumption adopted as the approval/certification value shall be that declared by the manufacturer if this is not exceeded by more than 4 percent by the value measured by the technical service. The measured value may be lower without any limitations.
- 2.3.2.If the measured value of CO2 emissions or fuel consumption exceeds the manufacturer's declared CO2 emissions or fuel consumption by more than 4 percent, another test shall be run on the same vehicle.

Where the average of the two test results does not exceed the manufacturer's declared value by more than 4 percent, the value declared by the manufacturer shall be taken as the approval/certification value.

- 2.3.3.If, in the event of another test being run, the average still exceeds the declared value by more than 4 percent, a final test shall be run on the same vehicle. The average of the three test results shall be taken as the approval/certification value.
- **3.** For Contracting Parties applying type-approval requirements with respect to modification and extension of approval of the approved type
 - 3.1. For all approved types, the approval authority that approved the type shall be notified of any modification of it. The approval authority may then either:
 - 3.1.1.consider that the modifications made are unlikely to have an appreciable adverse effect on the CO2 emissions and fuel consumption values and that the original environmental performance approval will be valid for the modified vehicle type with regard to the environmental performance, or

- 3.1.2.require a further test report from the technical service responsible for conducting the tests in accordance with point 4.
- 3.2. For Contracting Parties applying type-approval confirmation or extension of approval specifying the alterations, shall be communicated by the following procedure:
 - 3.2.1.If particulars recorded in the information package have changed, without requiring inspections or tests to be repeated, the amendment shall be designated a 'revision'.

In such cases, the approval authority shall issue the revised pages of the information package as necessary, marking each revised page to show clearly the nature of the change and,

- 3.2.2. The amendment shall be designated an 'extension' when particulars recorded in the information package have changed and any of the following occurs:
 - (a) further inspections or tests are required;
 - (b) any information on the approval certificate with the exception of its attachments, has changed;
 - (c) new requirements become applicable to the approved vehicle type or to the approved system, component or separate technical unit.

In the event of an extension, the approval authority shall issue an updated approval certificate denoted by an extension number, incremented in accordance with the number of successive extensions already granted. That approval certificate shall clearly show the reason for the extension and the date of re-issue.

- 3.3. The approval authority that grants the extension of the approval shall assign a serial number for such an extension according to the procedure below:
 - 3.3.1. Whenever amended pages or a consolidated, updated version are issued, the index to the information package attached to the approval certificate shall be amended accordingly to show the date of the most recent extension or revision, or the date of the most recent consolidation of the updated version.
 - 3.3.2.No amendment to the approval of a vehicle shall be required if the new requirements referred to in point (c) of paragraph 3.2.2. are, from a technical point of view, irrelevant to that type of vehicle or concern categories of vehicle other than the category to which it belongs.

4. For Contracting Parties applying type-approval requirements with respect to conditions of extension of vehicle environmental performance approval

4.1. Vehicles powered by an internal combustion engine only

An approval may be extended to vehicles produced by the same manufacturer that are of the same type or of a type that differs with regard to the following characteristics:

- 4.1.1.reference mass;
- 4.1.2.maximum authorised mass.;
- 4.1.3.type of bodywork;
- 4.1.4. overall gear ratios;
- 4.1.5. engine equipment and accessories;
- 4.1.6.engine speed versus vehicle speed in highest gear with an accuracy of +/- 5 %; provided the CO2 emissions or fuel consumption as measured in Annex B.4.1 by the technical service do not exceed the approval value by more than 4 percent.

B.4.1. Annex: method of measuring carbon dioxide emissions and fuel consumption of vehicles powered by a combustion engine only

1. Specification of the test

- 1.1. The carbon dioxide (CO2) emissions and fuel consumption of vehicles powered by a combustion engine only shall be determined according to the procedure for the type I test in section B.2. in force at the time of the approval/certification of the vehicle.
- 1.2. In addition to the CO2 emission and fuel consumption results for the entire type I test, CO2 emissions and fuel consumption shall also be determined separately for parts 1, 2 and 3, if applicable, by using the applicable type I test procedure.
- 1.3. In addition to the conditions in section B.2. in force at the time of the approval/certification of the vehicle, the following conditions shall apply:
 - 1.3.1.Only the equipment necessary for the operation of the vehicle during the test shall be in use. If there is a manually controlled device for the engine intake air temperature, it shall be in the position prescribed by the manufacturer for the ambient temperature at which the test is performed. In general, the auxiliary devices required for the normal operation of the vehicle shall be in use.
 - 1.3.2.If the radiator fan is temperature-controlled, it shall be in normal operating condition. The passenger compartment heating system, if present, shall be switched off, as shall any air-conditioning system, but the compressor for such systems shall be functioning normally.
 - 1.3.3.If a super-charger is fitted, it shall be in normal operating condition for the test conditions.
 - 1.3.4.All lubricants shall be those recommended by the manufacturer of the vehicle and shall be specified in the test report.
 - 1.3.5. The widest tyre shall be chosen, except where there are more than three tyre sizes, in which case the second widest shall be chosen. The pressures shall be indicated in the test report.
- 1.4. Calculation of CO2 and fuel consumption values
 - 1.4.1. The mass emission of CO2, expressed in g/km, shall be calculated from the measurements taken in accordance with the provisions of point 5 of section B.2.
 - 1.4.1.1. For this calculation, the density of CO2 shall be assumed to be $Q_{CO2} = 1.964 \cdot 10^3 \text{ g/m}^3$.
 - 1.4.2. The fuel consumption values shall be calculated from the hydrocarbon, carbon monoxide and carbon dioxide emission measurements taken in accordance with the provisions of point 4 of section B.2. in force at the time of the approval/certification of the vehicle.
 - 1.4.3. Fuel consumption (FC), expressed in litres per 100 km (in the case of petrol,:
 - 1.4.3.1. for vehicles with a positive ignition engine fuelled with petrol (E5): Equation B.4.1-1:

```
\vec{FC} = (0.118/D) \cdot ((0.848 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO2));
```

1.4.3.2. for vehicles with a compression ignition engine fuelled with diesel (B5):

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Equation B.4.1-9:
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 $FC = (0.116/D) \cdot ((0.861 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO2));$

1.4.4.In these formulae:

FC = the fuel consumption in litres per 100 km in the case of petrol, diesel or biodiesel, in m3 per 100 km

HC = the measured emission of hydrocarbons in g/km

CO = the measured emission of carbon monoxide in g/km

CO2 = the measured emission of carbon dioxide in g/km D = the density of the test fuel.



B.5. TEXT OF THE REGULATION, COMMON ANNEXES

Annexes to to	est type I, II and VII	
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B.5.1. <u>Annex: symbols</u>

Symbol	Definition	Unit
a	Coefficient of polygonal function	-
a_{T}	Rolling resistance force of front wheel	N
A	NG / biomethane quantity within the H ₂ NG mixture	percent vol.
b	Coefficient of polygonal function	
b_{T}	Coefficient of aerodynamic function	$N/(km/h)^2$
C	Coefficient of polygonal function	-
C _{co}	Concentration of carbon monoxide	ppm
C _{CO2}	Concentration of CO2 in the diluted exhaust gas contained in the sampling bag	percent vol.
C _{COcorr}	Corrected concentration of carbon monoxide	percent vol.
CO _{2c}	Carbon dioxide concentration of diluted gas, corrected to take account of diluent air	percent
CO _{2d}	Carbon dioxide concentration in the sample of diluent air collected in bag B	percent
CO _{2e}	Carbon dioxide concentration in the sample of diluent air collected in bag A	percent
CO _{2m}	Mass of carbon dioxide emitted during the test part	mg/km
CO _c	Carbon monoxide concentration of diluted gas, corrected to take account of diluent air	ppm
CO_d	Carbon monoxide concentration in the sample of diluent air, collected in bag B	ppm
CO _e	Carbon monoxide concentration in the sample of diluent air, collected in bag A	ppm
CO _m	Mass of carbon monoxide emitted during the test part	mg/km
C _{H2}	Concentration of hydrogen in the diluted exhaust gas contained in sampling bag	ppm
C _{H2O}	Concentration of H2O in the diluted exhaust gas contained in the sampling bag	percent vol.
C _{H2O-DA}	Concentration of H2O in the air used for dilution	percent vol.
C _{HC}	Concentration of HC in the diluted exhaust gas contained in the sampling bag	ppm (carbon equivalent)
d_0	Standard ambient relative air density	-
d _{CO}	Density of carbon monoxide	mg/cm ³
d_{CO_2}	Density of carbon dioxide	g/dm ³
d_{HC}	Density of hydrocarbon	mg/cm ³
D _{av}	Average distance between two battery recharges	km
D _{av}	Electric range of the vehicle	km
DiF	Dilution factor	-
Doyc	Distance from externally chargeable vehicle	km
S/d	Distance driven in a cycle part	km
d _{NOx}	Density of nitrogen oxide	mg/m ³
d _T	Relative air density under test condition	-
Δt	Coast-down time	S
Δt_{a_i}	Coast-down time measured in the first road test	S
Δt_{b_i}	Coast-down time measured in the second road test	S
$\Delta T_{\rm E}$	Coast-down time corrected for the inertia mass	s
$\Delta t_{ m E}$	Mean coast-down time on the chassis dynamometer at the reference vehicle speed	s
ΔT_{i}	Average coast-down time at specified vehicle speed	S
Δt_i	Coast-down time at corresponding s vehicle peed	S
ΔT_i	Average coast-down time at specified vehicle speed	S
$\Delta T_{\rm road}$	Target coast-down time	s
$\frac{\Delta t_{\text{road}}}{\Delta t_{\text{t}}}$	Mean coast-down time on the chassis dynamometer without absorption	S
Δv	Coast-down vehicle speed interval $(2\Delta v = v_1 - v_2)$	km/h
ε	Chassis dynamometer setting error	percent
F	Running resistance force	N
F*	Target running resistance force	N

F* _(v0)	Target running resistance force at reference vehicle speed on chassis dynamometer	N
$F^*_{(v_i)}$	Target running resistance force at specified vehicle speed on chassis dynamometer	N
f* ₀	Corrected rolling resistance in the standard ambient condition	N
f* ₂	Corrected coefficient of aerodynamic drag in the standard ambient condition	$N/(km/h)^2$
F*;	Target running resistance force at specified vehicle speed	N
$\frac{\mathbf{f}_{0}}{\mathbf{f}_{0}}$	Rolling resistance	N
f_2	Coefficient of aerodynamic drag	1
$\frac{r_2}{F_E}$	Set running resistance force on the chassis dynamometer	N/(km/h) ² N
$F_{E(v_0)}$	Set running resistance force at the reference s vehicle peed on the chassis dynamometer	N
$F_{E(v_2)}$	Set running resistance force at the specified vehicle speed on the chassis	N
$F_{\rm f}$	dynamometer Total friction loss	N
$F_{f(v_0)}$	Total friction loss at the reference vehicle speed	N
$\frac{1 f(v_0)}{F_i}$	Running resistance force	N
$F_{i(v_0)}$	Running resistance force at the reference vehicle speed	N
F_{pau}	Braking force of the power absorbing unit	N
F _{pau(v0)}	Braking force of the power absorbing unit at the reference vehicle speed	N
F (::)	Braking force of the power absorbing unit at the reference vehicle speed Braking force of the power absorbing unit at the specified vehicle speed	N
$\frac{F_{\text{pau}(v_j)}}{F_T}$	Running resistance force obtained from the running resistance table	N
1 T	Running resistance force obtained from the running resistance table	g of water /
Н	Absolute humidity	kg of dry
	110001010 1101111011	air
HC _c	Concentration of diluted gases expressed in the carbon equivalent, corrected to	nnm
TIC _c	take account of diluent air	ppm
HC_d	Concentration of hydrocarbons expressed in the carbon equivalent, in the sample of diluent air collected in bag B	ppm
HC_e	Concentration of hydrocarbons expressed in the carbon equivalent, in the sample of diluent air collected in bag A	ppm
HC_m	Mass of hydrocarbon emitted during the test part	mg/km
i	gear number	-
K_0	Temperature correction factor for rolling resistance	-
K _h	Humidity correction factor	-
L	Approval limit values of gaseous pollutant emission	mg/km
m	Test vehicle mass	kg
ma	Actual mass of the test vehicle	kg
m _{corr}	PM mass corrected for buoyancy	mg
$m_{\mathrm{f}i}$	Flywheel equivalent inertia mass	kg
mi	Equivalent inertia mass	kg
m _{mix}	molar mass of air in balance environment (28.836 gmol ⁻¹)	gmol ⁻¹
m_{ri}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with	kg kg
m _r	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel	kg kg
$m_{ m r}$ $m_{ m ri}$ $m_{ m k~or~m_{ref}}$	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle	kg kg kg
$m_{ m r}$ $m_{ m ri}$ $m_{ m k~or~m_{ref}}$ $m_{ m rf}$	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel	kg kg kg kg
m_{r} m_{ri} $m_{k \text{ or } m_{ref}}$ m_{rf}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel Rider mass	kg kg kg kg kg
m_{ri} m_{ri} $m_{k \text{ or } m_{ref}}$ m_{rf} m_{rid} m_{uncorr}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel Rider mass PM mass uncorrected for buoyancy	kg kg kg kg kg kg mg
m_{r} m_{ri} $m_{k \text{ or } m_{ref}}$ m_{rf}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel Rider mass PM mass uncorrected for buoyancy Mass emission of the pollutant i in mg/km	kg kg kg kg kg mg
m_{ri} m_{ri} $m_{k \text{ or } m_{ref}}$ m_{rf} m_{rid} m_{uncorr}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel Rider mass PM mass uncorrected for buoyancy Mass emission of the pollutant i in mg/km Average mass emission of the pollutant i with an electrical energy/power storage device in minimum state of charge (maximum discharge of capacity)	kg kg kg kg kg kg mg
m _r m _{ri} m _{k or m_{ref} m_{rf} m_{rid} m_{uncorr} M_i}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel Rider mass PM mass uncorrected for buoyancy Mass emission of the pollutant i in mg/km Average mass emission of the pollutant i with an electrical energy/power storage device in minimum state of charge (maximum discharge of capacity) Average mass emission of the pollutant i with a fully charged electrical	kg kg kg kg kg mg mg
m_{r} m_{ri} $m_{k \text{ or } m_{ref}}$ m_{rf} m_{rid} m_{uncorr} M_{i}	Equivalent inertia mass of all the wheels Equivalent inertia mass of all the rear wheel and vehicle parts rotating with wheel Reference mass of the vehicle Rotating mass of the front wheel Rider mass PM mass uncorrected for buoyancy Mass emission of the pollutant i in mg/km Average mass emission of the pollutant i with an electrical energy/power storage device in minimum state of charge (maximum discharge of capacity)	kg kg kg kg kg mg mg mg/km

n	Number of data regarding the emission or the test	_
N N	Number of revolution made by pump P	<u>-</u>
nd _{vi}	Ratio between engine speed in min ⁻¹ and vehicle speed in km/h in gear 'i'	-
ng	Number of forward gears	-
n_{idle}	Idling engine speed	min-1
$n_{max}_{acc_{(1)}}$	Upshift engine speed from gear 1 to gear 2 during acceleration phases	min-1
n_max_acc(i)	Up shift engine speed from gear i to gear i+1 during acceleration phases, i>1	min-1
n min acc(i)	Minimum engine speed for cruising or deceleration in gear 1	min-1
NO _{xc}	Nitrogen oxide concentration of diluted gases, corrected to take account of diluent air	ppm
NO_{xd}	Nitrogen oxide concentration in the sample of diluent air collected in bag B	ppm
NO _{xe}	Nitrogen oxide concentration in the sample of diluent air collected in bag A	ppm
NO_{xm}	Mass of nitrogen oxides emitted during the test part	mg/km
p_0	Standard ambient pressure	kPa
pa	Ambient/atmospheric pressure	kPa
p_{abs}	absolute pressure in balance environment	
$p_{\rm d}$	Saturated pressure of water at the test temperature	kPa
p _i	Average under-pressure during the test part in the section of pump P	kPa
p_{T}	Mean ambient pressure during the test	kPa
Pn	Rated power	kW
Q	Electric energy balance	Ah
ρ_0	Standard relative ambient air volumetric mass	mg/cm ³
$ ho_{air}$	density of air in balance environment	mg/cm ³
ρ_{weight}	density of calibration weight used to span balance	mg/cm ³
ρ _{media}	density of PM sample medium (filter) with filter medium Teflon coated glass fibre (e.g. TX40): $\rho_{media} = 2.300 \text{ kg/m}3$	mg/cm ³
r(i)	Gear ratio in gear i	-
R	molar gas constant (8.314 Jmol ⁻¹ K ⁻¹)	Jmol ⁻¹ K ⁻¹
R_{f}	Response factor to calibrate HC analyser	_
R_{F}	Final test result of pollutant emissions, carbon dioxide emission or fuel consumption	mg/km, g/km, 1/100km
R_1	Test results of pollutant emissions, carbon dioxide emission or fuel consumption for cycle part 1 with cold start	mg/km, g/km, 1/100km
R ₂	Test results of pollutant emissions, carbon dioxide emission or fuel consumption for cycle part 2 with warm condition	mg/km, g/km, 1/100km
R_3	Test results of pollutant emissions, carbon dioxide emission or fuel consumption for cycle part 1 with warm condition	mg/km, g/km, 1/100km
Ri ₁	First type I test results of pollutant emissions	mg/km
Ri ₂	Second type I test results of pollutant emissions	mg/km
Ri ₃	Third type I test results of pollutant emissions	mg/km
S	Rated engine speed	min-1
S	Accumulated distance in test cycle (point 5.1.1.3 of Annex B.2)	km
T _{amb}	absolute ambient temperature of balance environment	°C
T _C	Temperature of the coolant	°C
To	Temperature of the engine oil	°C
$T_{\rm P}$	Temperature of the engine on Temperature of the spark-plug seat/gasket	°C
T_0	Standard ambient temperature	°C
	Temperature of the diluted gases during the test part, measured in the intake	°C
T _p	section of pump P	
T_{T}	Mean ambient temperature during the test	°C
U	Relative humidity	percent
V	Specified vehicle speed	km/h

V	Total volume of diluted gas	m3
V _{max}	Maximum design vehicle speed of test vehicle	km/h
v_0	Reference vehicle speed	km/h
V_0	Volume of gas displaced by pump P during one revolution	m ³ /rev.
\mathbf{v}_1	Vehicle speed at which the measurement of the coast-down time begins	km/h
v_2	Vehicle speed at which the measurement of the coast-down time ends	km/h
vi	Specified vehicle speed selected for the coast-down time measurement	km/h
\mathbf{w}_1	Weighting factor of cycle part 1 with cold start	-
W _{1warm}	Weighting factor of cycle part 1 with warm condition	-
\mathbf{w}_2	Weighting factor of cycle part 2 with warm condition	-
\mathbf{w}_3	Weighting factor of cycle part 3 with warm condition	-

Table B.5.1-1: symbols used

B.5.2. Annex: reference fuels

- 1. Specifications of reference fuels for testing vehicles in environmental tests, in particular for tailpipe and evaporative emissions testing
- 1.1. The following tables list the technical data on liquid reference fuels that Contracting Parties may require to be used for environmental performance testing of two-wheeled vehicles. These reference fuels were used to define the emission limits set out in point 9. of section B.1.



Fuel Property or Substance Name	Unit	Standard		Test method
1 2		Minimum	Maximum	
Research octane number, RON		90	92	JIS K2280
Motor octane number, MON		80	82	JIS K2280
Density	g/cm ³	0.72	0.77	JIS K2249
Vapour pressure	kPa	56	60	JIS K2258
Distillation:				
— 10 % distillation temperature	K (°C)	318 (45)	328 (55)	JIS K2254
— 50 % distillation temperature	K (°C)	363 (90)	373 (100)	JIS K2254
— 90 % distillation temperature	K (°C)	413 (140)	443 (170)	JIS K2254
— final boiling point	K (°C)		488 (215)	JIS K2254
— olefins	% v/v	15	25	JIS K2536-1
— oleims	% V/V	13	23	JIS K2536-2
				JIS K2536-1
— aromatics	% v/v	20	45	JIS K2536-2
				JIS K2536-3
				JIS K2536-2
— benzene	% v/v		1.0	JIS K2536-3
				JIS K2536-4
				JIS K2536-2
Oxygen content		not to be de	tected	JIS K2536-4
				JIS K2536-6
Existent gum	mg/100ml		5	JIS K2261
				JIS K2541-1
Sulphur content	Wt ppm		10	JIS K2541-2
Sulphur Content	wt ppin		10	JIS K2541-6
				JIS K2541-7
Lead content		not to be de	tected	JIS K2255
				JIS K2536-2
Ethanol		not to be de	tected	JIS K2536-4
				JIS K2536-6
				JIS K2536-2
Methanol		not to be de	tected	JIS K2536-4
Wethanor		not to be de	iccica	JIS K2536-5
				JIS K2536-6
				JIS K2536-2
MTBE		not to be de	tected	JIS K2536-4
		not to be de		JIS K2536-5
				JIS K2536-6
Kerosene		not to be de	tected	JIS K2536-2
1111000110		1101 10 00 de		ЛS K2536-4

B.5.2.2. Type: Petrol E0 (nominal 95 RON)							
		Limi	ts (1)	T 4 4 1			
Parameter	Unit	Minimum	Maximum	Test method	Publication		
Research octane number, RON		95.0		EN 25164	1993		
Motor octane number, MON		85.0		EN 25163	1993		
Density at 15 °C	kg/m ³	748	762	ISO 3675	1995		
Reid vapour pressure	kPa	56.0	60.0	EN 12	1993		
Distillation:							
- initial boiling point	°C	24	40	EN-ISO 3205	1988		
- evaporated at 100 °C	per cent v/v	49.0	57.0	EN-ISO 3205	1988		
- evaporated at 150 °C	per cent v/v	81.0	87.0	EN-ISO 3205	1988		
- final boiling point	°C	190	215	EN-ISO 3205	1988		
Residue	per cent		2	EN-ISO 3205	1988		
Hydrocarbon analysis:							
- olefins	per cent v/v		10	ASTM D 1319	1995		
- aromatics(3)	per cent v/v	28.0	40.0	ASTM D 1319	1995		
- benzene	per cent v/v		1.0	pr. EN 12177	1998 (2)		
- saturates	per cent v/v		balance	ASTM D 1319	1995		
Carbon/hydrogen ratio		report	report				
Oxidation stability (4)	min.	480		EN-ISO 7536	1996		
Oxygen content (5)	per cent m/m		2.3	EN 1601	1997 (2)		
Existent gum	mg/ml		0.04	EN-ISO 6246	1997 (2)		
Sulphur content (6)	mg/kg		100	pr.EN-ISO/DIS 14596	1998 (2)		
Copper corrosion at 50 °C			1	EN-ISO 2160	1995		
Lead content	g/l		0.005	EN 237	1996		
Phosphorus content	g/l		0.0013	ASTM D 3231	1994		

(1) The values quoted in the specification are "true values". In establishment of their limit values the terms of ISO 4259 "Petroleum products - Determination and application of precision data in relation to methods of test,' have been applied and in fixing a minimum value, a minimum difference of 2R above zero has been taken into account; in fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility).

Notwithstanding this measure, which is necessary for statistical reasons, the manufacturer of fuels should nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value in the case of quotations of maximum and minimum limits. Should it be necessary to clarify the question as to whether a fuel meets the requirements of the specifications, the terms of ISO 4259 should be applied.

- (2) The month of publication will be completed in due course.
- (3) The reference fuel used shall have a maximum aromatics content of 35 per cent v/v.
- (4) The fuel may contain oxidation inhibitors and metal deactivators normally used to stabilise refinery gasoline streams, but detergent/dispersive additives and solvent oils shall not be added.
- (5) The actual oxygen content of the fuel for the tests shall be reported. In addition the maximum oxygen content of the reference fuel shall be 2.3 per cent.
- (6) The actual sulphur content of the fuel used for the tests shall be reported. In addition the reference fuel shall have a maximum sulphur content of 50 ppm.

B.5.2.3. Type: Petrol E0 (nominal	100 RON)			
Fuel Property or Substance Name	Unit	Standard		Test method
2 7		Minimum Maximum		
Research octane number, RON		99	101	JIS K2280
Motor octane number, MON		86	88	JIS K2280
Density	g/cm ³	0.72	0.77	JIS K2249
Vapour pressure	kPa	56	60	JIS K2258
Distillation:				
— 10 % distillation temperature	K (°C)	318 (45)	328 (55)	JIS K2254
— 50 % distillation temperature	K (°C)	363 (90)	373 (100)	JIS K2254
— 90 % distillation temperature	K (°C)	413 (140)	443 (170)	JIS K2254
— final boiling point	K (°C)		488 (215)	JIS K2254
	0/ /	1.5	25	JIS K2536-1
— olefins	% v/v	15	25	JIS K2536-2
				JIS K2536-1
— aromatics	% v/v	20	45	JIS K2536-2
				JIS K2536-3
				JIS K2536-2
— benzene	% v/v		1.0	JIS K2536-3
				JIS K2536-4
				JIS K2536-2
Oxygen content		not to be detected		JIS K2536-4
, 5				JIS K2536-6
Existent gum	mg/100ml		5	JIS K2261
	3			JIS K2541-1
0.1.1	****		1.0	JIS K2541-2
Sulphur content	Wt ppm		10	JIS K2541-6
				JIS K2541-7
Lead content		not to be de	tected	JIS K2255
				JIS K2536-2
Ethanol		not to be de	tected	JIS K2536-4
				JIS K2536-6
				JIS K2536-2
N. d. 1		1 1	1	JIS K2536-4
Methanol		not to be de	tected	JIS K2536-5
				JIS K2536-6
				JIS K2536-2
MTDE		not to be de-	taatad	JIS K2536-4
MTBE		not to be de	ieciea	JIS K2536-5
				JIS K2536-6
Varagana		not to be 1-	taatad	JIS K2536-2
Kerosene		not to be de	ieciea	JIS K2536-4

B.5.2.4. Type: Petrol E5 (nominal 95 Octane)							
D	I I:4	Lii	nits ¹	Total and a d			
Parameter	Unit	Minimum	Maximum	Test method			
Research octane number, RON		95.0	-	EN 25164 / prEN ISO 5164			
Motor octane number, MON		85.0	-	EN 25163 / prEN ISO 5163			
Density at 15 °C	kg/m ³	743	756	EN ISO 3675 / EN ISO 12185			
Vapour pressure	kPa	56.0	60.0	EN ISO 13016-1 (DVPE)			
Water content	% v/v		0.015	ASTM E 1064			
Distillation:							
− Evaporated at 70 °C	% v/v	24.0	44.0	EN ISO 3405			
− Evaporated at 100 °C	% v/v	48.0	60.0	EN ISO 3405			
− Evaporated at 150 °C	% v/v	82.0	90.0	EN ISO 3405			
 Final boiling point 	°C	190	210	EN ISO 3405			
Residue	% v/v	_	2.0	EN ISO 3405			
Hydrocarbon analysis:							
– Olefins	% v/v	3.0	13.0	ASTM D 1319			
- Aromatics	% v/v	29.0	35.0	ASTM D 1319			
- Benzene	% v/v	-	1.0	EN 12177			
- Saturates	% v/v	Re	port	ASTM 1319			
Carbon/hydrogen ratio		Re	port				
Carbon/oxygen ratio		Re	port				
Induction period ²	minutes	480	-	EN ISO 7536			
Oxygen content ⁴	% m/m	Re	port	EN 1601			
Existent gum	mg/ml	-	0.04	EN ISO 6246			
Sulphur content ³	mg/kg	-	10	EN ISO 20846 / EN ISO 20884			
Copper corrosion		-	Class 1	EN ISO 2160			
Lead content	mg/l	-	5	EN 237			
Phosphorus content	mg/l	-	1.3	ASTM D 3231			
Ethanol ⁵	% v/v	4.7	5.3	EN 1601 / EN 13132			

The values quoted in the specifications are 'true values'. For establishing the limit values, the terms of ISO 4259:2006 (Petroleum products — Determination and application of precision data in relation to methods of test) have been applied and for fixing a minimum value, a minimum difference of 2R above zero has been taken into account; for fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility).

Notwithstanding this measure, which is necessary for technical reasons, the fuel manufacturer shall nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value when quoting maximum and minimum limits. Should it be necessary to clarify whether a fuel meets the requirements of the specifications, the terms of ISO 4259:2006 shall be applied.

- The fuel may contain oxidation inhibitors and metal deactivators normally used to stabilise refinery petrol streams, but detergent/dispersive additives and solvent oils shall not be added.
- The actual sulphur content of the fuel used for the type I test shall be reported.
- ⁴ Ethanol meeting the specification of prEN 15376 is the only oxygenate that shall be intentionally added to the reference fuel.
- There shall be no intentional addition to this reference fuel of compounds containing phosphorus, iron, manganese or lead.

B.5.2.5. Type: Diesel fuel (B0)								
Parameter	Unit	Limits (1)		Test method	Publication			
Parameter	Onit	Minimum	Maximum	Test method	Publication			
Cetane number (2)		52.0	54.0	EN-ISO 5165	1998 (3)			
Density at 15°C	kg/m³	833	837	EN-ISO 3675	1995			
Distillation:								
- 50 per cent point	°C	245	-	EN-ISO 3405	1988			
- 95 per cent	°C	345	350	EN-ISO 3405	1988			
- final boiling point	°C	=	370	EN-ISO 3405	1988			
Flash point	°C	55	-	EN 22719	1993			
CFPP	°C	-	-5	EN 116	1981			
Viscosity at 40 °C	mm²/s	2.5	3.5	EN-ISO 3104	1996			
Polycyclic aromatic hydrocarbons	per cent m/m	3	6.0	IP 391	1995			
Sulphur content (4)	mg/kg	-	300	pr. EN-ISO/DIS 14596	1998(3)			
Copper corrosion		-	1	EN-ISO 2160	1995			
Conradson carbon residue (10 per cent DR)	per cent m/m	-	0.2	EN-ISO 10370	1995			
Ash content	per cent m/m	-	0.01	EN-ISO 6245	1995			
Water content	per cent m/m	-	0.05	EN-ISO 12937	1998 (3)			
Neutralisation (strong acid) number	mg KOH/g	-	0.02	ASTM D 974-95	1998 (3)			
Oxidation stability (5)	mg/ml	-	0.025	EN-ISO 12205	1996			

- (1) The values quoted in the specification are "true values". In establishment of their limit values the terms of ISO 4259 "Petroleum products Determination and application of precision data in relation to methods of test" have been applied and in fixing a minimum value, a minimum difference of 2R above zero has been taken into account; in fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility).
 - Notwithstanding this measure, which is necessary for statistical reasons, the manufacturer of fuels should nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value in the case of quotations of maximum and minimum limits. Should it be necessary to clarify the question as to whether a fuel meets the requirements of the specifications, the terms of ISO 4259 should be applied.
- (2) The range for the Cetane number is not in accordance with the requirement of a minimum range of 4R. However, in the case of a dispute between fuel supplier and fuel user, the terms in ISO 4259 may be used to resolve such disputes provided replicate measurements, of sufficient number to archive the necessary precision, are made in preference to single determinations.
- (3) The month of publication will be completed in due course.
- (4) The actual sulphur content of the fuel used for the Type I test shall be reported. In addition the reference fuel shall have a maximum sulphur content of 50 ppm.
- (5) Even though oxidation stability is controlled, it is likely that shelf life will be limited. Advice should be sought from the supplier as to storage conditions and life.

B.5.2.6. Type: Diesel fuel (B5)				
Parameter	Unit	Limits ¹		Test method
		Minimum	Maximum	Test method
Cetane number ²		52.0	54.0	EN ISO 5165
Density at 15 °C	kg/m³	833	837	EN ISO 3675
Distillation:				
- 50% point	°C	245	-	EN ISO 3405
- 95% point	°C	345	350	EN ISO 3405
- Final boiling point	°C	-	370	EN ISO 3405
Flash point	°C	55	-	EN 22719
CFPP	°C	-	- 5	EN 116
Viscosity at 40°C	mm^2/s	2.3	3.3	EN ISO 3104
Polycyclic aromatic hydrocarbons	% m/m	2.0	6.0	EN 12916
Sulphur content ³	mg/kg	-	10	EN ISO 20846 / EN ISO 20884
Copper corrosion		-	Class 1	EN ISO 2160
Conradson carbon residue (10 % DR)	% m/m	1	0.2	EN ISO 10370
Ash content	% m/m	-	0.01	EN ISO 6245
Water content	% m/m	-	0.02	EN ISO 12937
Neutralisation (strong acid) number	mg KOH/g	-	0.02	ASTM D 974
Oxidation stability ⁴	mg/ml	-	0.025	EN ISO 12205
Lubricity (HFRR wear scan diameter at 60 °C)	μm	-	400	EN ISO 12156
Oxidation stability at 110 °C ^{4.6}	h	20.0		EN 14112
FAME ⁵	% v/v	4.5	5.5	EN 14078

The values quoted in the specifications are 'true values'. For establishing the limit values, the terms of ISO 4259:2006 (Petroleum products — Determination and application of precision data in relation to methods of test) have been applied and for fixing a minimum value, a minimum difference of 2R above zero has been taken into account; for fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility).

Notwithstanding this measure, which is necessary for technical reasons, the fuel manufacturer shall nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value when quoting maximum and minimum limits. Should it be necessary to clarify whether a fuel meets the requirements of the specifications, the terms of ISO 4259:2006 shall be applied.

- The range for Cetane number is not in accordance with the requirements of a minimum range of 4R. However, the terms of ISO 4259:2006 may be used to resolve disputes between fuel supplier and fuel user, provided replicate measurements, of sufficient number to archive the necessary precision, are taken in preference to single determinations.
- The actual sulphur content of the fuel used for the type I test shall be reported.
- Even though oxidation stability is controlled, it is likely that shelf life will be limited. Advice shall be sought from the supplier as to storage conditions and shelf life.
- FAME content to meet the specification of EN 14214.
- Oxidation stability can be demonstrated by EN ISO 12205:1995 or EN 14112:1996. This requirement shall be reviewed based on CEN/TC19 evaluations of oxidative stability performance and test limits.

[EPPR-IWG to add proposal for B7 fuel – proposed draft as below:

Technical specifications of the reference Diesel Fuel (B7)						
Parameter	Unit	Lin	nits 1	Test method		
Parameter	Cini	Minimum	Maximum			
Cetane Index		46.0		EN ISO 4264		
Cetane number ²		52.0	56.0	EN ISO 5165		
Density at 15 °C	kg/m³	833.0	837.0	EN ISO 12185		
Distillation:						
- 50% point	°C	245.0	_	EN ISO 3405		
- 95% point	°C	345.0	360.0	EN ISO 3405		
- final boiling point	°C	_	370.0	EN ISO 3405		
Flash point	°C	55	_	EN ISO 2719		
Cloud point	°C	-	-10	EN 23015		
Viscosity at 40 °C	mm²/s	2.30	3.30	EN ISO 3104		
Polycyclic aromatic hydrocarbons	% m/m	2.0	4.0	EN 12916		
Sulphur content	mg/kg		10.0	EN ISO 20846		
Supua Conen	mg/ag		10.0	EN ISO 20884		
Copper corrosion 3hrs, 50 °C		_	Class 1	EN ISO 2160		
Conradson carbon residue (10 % DR)	% m/m	_	0.20	EN ISO 10370		
Ash content	% m/m	_	0.010	EN ISO 6245		
Total contamination	mg/kg	-	24	EN 12662		
Water content	mg/kg	_	200	EN ISO 12937		
Acid number	mg KOH/g	_	0.10	EN ISO 6618		
Lubricity (HFRR wear scan diameter at 60 °C)	μm	_	400	EN ISO 12156		
Oxidation stability @ 110 °C 3	h	20.0		EN 15751		
FAME 4	% v/v	6.0	7.0	EN 14078		

- 1 The values quoted in the specifications are 'true values'. In establishment of their limit values the terms of ISO 4259 Petroleum products Determination and application of precision data in relation to methods of test have been applied and in fixing a minimum value, a minimum difference of 2R above zero has been taken into account; in fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility). Notwithstanding this measure, which is necessary for technical reasons, the manufacturer of fuels shall nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value in the case of quotations of maximum and minimum limits. Should it be necessary to clarify whether a fuel meets the requirements of the specifications, the terms of ISO 4259 shall be applied.
- 2 The range for cetane number is not in accordance with the requirements of a minimum range of 4R. However, in the case of a dispute between fuel supplier and fuel user, the terms of ISO 4259 may be used to resolve such disputes provided replicate measurements, of sufficient number to archive the necessary precision, are made in preference to single determinations.
- 3 Even though oxidation stability is controlled, it is likely that shelf life will be limited. Advice shall be sought from the supplier as to storage conditions and life.
- 4 FAME content to meet the specification of EN 14214.

B.5.3. Annex: test vehicle requirements Test types I, II and VII

1. General

- 1.1. All components of the test vehicle shall conform to those of the production series or, if the test vehicle is different from the production series, a full description shall be given in the test report. In selecting the test vehicle, the vehicle manufacturer and the technical service shall agree to the satisfaction of the [approval authority] / [certification authority] which tested parent vehicle is representative of the related vehicle propulsion unit family as laid down in Annex B.5.10.
- 1.2. Unless specified differently elsewhere within the GTR, the vehicle shall be used, adjusted, specified, maintained, fuelled and lubricated as it would be in the production series and as recommended to the user. Parts and consumables shall be used which are or will be commercially available and are permitted for use on the intended roads and for the atmospheric and road conditions experienced while under test.
- 1.3. The lighting and signalling and auxiliary devices, except those required for the testing and usual daytime operation of the vehicle, shall be switched off.
- 1.4. If the batteries are operated above the ambient temperature, the operator shall follow the procedure recommended by the vehicle manufacturer in order to keep the battery temperature in the normal operating range. The vehicle manufacturer shall be in a position to attest that the thermal management system of the battery is neither disabled nor reduced.

2. Run-in

The vehicle shall be presented in good mechanical condition, properly maintained and used. It shall have been run in and driven at least 1,000 km before the test. The engine, pollutant emission abatement equipment, drive train, and vehicle shall be properly run in, in accordance with the vehicle manufacturer's requirements.

3. Adjustments

The test vehicle shall be adjusted in accordance with the vehicle manufacturer's requirements, e.g. as regards the viscosity of the oils, or, if it differs from the production series, a full description shall be given in the test report. In case of a four by four drive, the axle to which the lowest torque is delivered may be deactivated in order to allow testing on a standard chassis dynamometer.

4. Test mass and load distribution

The test mass, including the masses of the rider and the instruments, shall be measured before the beginning of the tests. The load shall be distributed across the wheels in conformity with the vehicle manufacturer's instructions.

5. Tyres

The tyres shall be of a type specified as original equipment by the vehicle manufacturer. The tyre pressures shall be adjusted to the specifications of the vehicle manufacturer or to those where the speed of the vehicle during the road test and the vehicle speed obtained on the chassis dynamometer are equalised. The tyre pressure shall be indicated in the test report.

B.5.4. <u>Annex: classification of equivalent inertia mass and running resistance, applicable for two-wheeled vehicles (table method)</u>

- 1. The chassis dynamometer can be set using the running resistance table instead of the running resistance force obtained by the coast-down methods set out in sections B.5.5. or B.5.6. In this table method, the chassis dynamometer shall be set by the reference mass regardless of particular light motor vehicle characteristics.
- 2. The flywheel equivalent inertia mass m_{ref} shall be the equivalent inertia mass m_i specified in point 3.4.6.1.2 of section B.2. The chassis dynamometer shall be set by the rolling resistance of front wheel 'a' and the aerodynamic drag coefficient 'b' specified in the following table.

Reference mass m _{ref} (kg)	Equivalent inertia mass m _i (kg)	Rolling resistance of front wheel a (N)	Aero drag coefficient b (N/(km/h) ²)
$0 < m_{ref} \le 25$	20	1.8	0.0203
$25 < m_{ref} \le 35$	30	2.6	0.0205
$35 < m_{ref} \le 45$	40	3.5	0.0206
$45 < m_{ref} \le 55$	50	4.4	0.0208
$55 < m_{ref} \le 65$	60	5.3	0.0209
$65 < m_{ref} \le 75$	70	6.8	0.0211
$75 < m_{ref} \le 85$	80	7.0	0.0212
$85 < m_{ref} \le 95$	90	7.9	0.0214
$95 < m_{ref} \le 105$	100	8.8	0.0215
$105 < m_{ref} \le 115$	110	9.7	0.0217
$115 < m_{ref} \le 125$	120	10.6	0.0218
$125 < m_{ref} \le 135$	130	11.4	0.0220
$135 < m_{ref} \le 145$	140	12.3	0.0221
$145 < m_{ref} \le 155$	150	13.2	0.0223
$155 < m_{ref} \le 165$	160	14.1	0.0224
$165 < m_{ref} \le 175$	170	15.0	0.0226
$175 < m_{ref} \le 185$	180	15.8	0.0227

$185 < m_{ref} \le 195$	190	16.7	0.0229
$195 < m_{ref} \le 205$	200	17.6	0.0230
$205 < m_{ref} \le 215$	210	18.5	0.0232
$215 < m_{ref} \le 225$	220	19.4	0.0233
$225 < m_{ref} \le 235$	230	20.2	0.0235
$235 < m_{ref} \le 245$	240	21.1	0.0236
$245 < m_{ref} \le 255$	250	22.0	0.0238
$255 < m_{ref} \le 265$	260	22.9	0.0239
$265 < m_{ref} \le 275$	270	23.8	0.0241
$275 < m_{ref} \le 285$	280	24.6	0.0242
$285 < m_{ref} \le 295$	290	25.5	0.0244
$295 < m_{ref} \le 305$	300	26.4	0.0245
$305 < m_{ref} \le 315$	310	27.3	0.0247
$315 < m_{ref} \le 325$	320	28.2	0.0248
$325 < m_{ref} \le 335$	330	29.0	0.0250
$335 < m_{ref} \le 345$	340	29.9	0.0251
$345 < m_{ref} \le 355$	350	30.8	0.0253
$355 < m_{ref} \le 365$	360	31.7	0.0254
$365 < m_{ref} \le 375$	370	32.6	0.0256
$375 < m_{ref} \le 385$	380	33.4	0.0257
$385 < m_{ref} \le 395$	390	34.3	0.0259
$395 < m_{ref} \le 405$	400	35.2	0.0260
$405 < m_{ref} \le 415$	410	36.1	0.0262
$415 < m_{ref} \le 425$	420	37.0	0.0263
$425 < m_{ref} \le 435$	430	37.8	0.0265
$435 < m_{ref} \le 445$	440	38.7	0.0266

$445 < m_{ref} \le 455$	450	39.6	0.0268
$455 < m_{ref} \le 465$	460	40.5	0.0269
$465 < m_{ref} \le 475$	470	41.4	0.0271
$475 < m_{ref} \le 485$	480	42.2	0.0272
$485 < m_{ref} \le 495$	490	43.1	0.0274
$495 < m_{ref} \le 505$	500	44.0	0.0275
At every 10 kg	At every 10 kg	$a = 0.088 \times m_1^*/$	$b = 0.000015 \times \\ m_i + 0.02 \; \underline{**}/$

^{*/}The value shall be rounded to one decimal place.

Table B.5.4.-1: Classification of equivalent inertia mass and running resistance used for two- and three wheeled vehicles.

 $[\]underline{**}$ /The value shall be rounded to four decimal places.

B.5.5. <u>Annex: road tests of two-wheeled vehicles equipped with one wheel on the driven axle for the determination of test bench settings</u>

1. Requirements for the rider

- 1.1. The rider shall wear a well-fitting (one-piece) suit or similar clothing and a protective helmet, eye protection, boots and gloves.
- 1.2. The rider, dressed and equipped as described in point 1.1., shall have a mass of $75 \text{ kg} \pm 5 \text{ kg}$ and be 1.75 m ± 0.05 m tall.
- 1.3. The rider shall be seated on the seat provided, with his feet on the footrests and his arms extended normally. This position shall allow the rider to have proper control of the vehicle at all times during the tests.

2. Requirement for the road and ambient conditions

- 2.1. The test road shall be flat, level, straight and smoothly paved. The road surface shall be dry and free of obstacles or wind barriers that might impede the measurement of the running resistance. The slope of the surface shall not exceed 0.5% between any two points at least 2 m apart.
- 2.2. During data collecting periods, the wind shall be steady. The wind speed and the direction of the wind shall be measured continuously or with adequate frequency at a location where the wind force during coast-down is representative.
- 2.3. The ambient conditions shall be within the following limits:
 - maximum wind speed: 3 m/s
 - maximum wind speed for gusts: 5 m/s
 - average wind speed, parallel: 3 m/s
 - average wind speed, perpendicular: 2 m/s
 - maximum relative humidity: 95%
 - air temperature: 5 °C to 35 °C
- 2.4. Standard ambient conditions shall be as follows:
 - pressure, P₀: 101.3 kPa
 - temperature, T₀: 20 °C
 - relative air density, d₀: 0.9197
 - air volumetric mass, $\rho_0{:}~1.189~kg/m^3$
- 2.5. The relative air density when the vehicle is tested, calculated in accordance with the equation B.5.5.-1, shall not differ by more than 7.5% from the air density under the standard conditions.
- 2.6. The relative air density, d_T , shall be calculated using the following formula:

Equation B.5.5.-1

$$d_T = d_0 \cdot \frac{p_T}{p_0} \cdot \frac{T_0}{T_T}$$

where:

d₀ is the reference relative air density at reference conditions (0.9197)

p_T is the mean ambient pressure during the test, in kPa;

p₀ is the reference ambient pressure (101.3 kPa);

 T_T is the mean ambient temperature during test, in K;

 T_0 is the reference ambient temperature 20 °C.

3. Condition of the test vehicle

- 3.1. The test vehicle shall comply with the conditions described in point 1.1. of annex B.5.6.
- 3.2. When installing the measuring instruments on the test vehicle, care shall be taken to minimise their effects on the distribution of the load across the wheels. When installing the vehicle speed sensor outside the vehicle, care shall be taken to minimise the additional aerodynamic loss.

3.3. Checks

The following checks shall be made in accordance with the manufacturer's specifications for the use considered: wheels, wheel rims, tyres (make, type and pressure), front axle geometry, brake adjustment (elimination of parasitic drag), lubrication of front and rear axles, adjustment of the suspension and vehicle ground clearance, etc. Check that during freewheeling, there is no electrical braking.

4. Specified coast-down vehicle speeds

4.1. The coast-down times shall be measured between v_1 and v_2 as specified in Table B.5.5.-1, depending on the vehicle class as defined in point 3. of section B.1.

4.2

Motorcycle Class	v; in km/h	v₁ in km/h	v2 in km/h
	20	25	15
0-1	15	20	10
	10	15	5
	40	45	35
0-2	30	35	25
	20	25	15
	50	55	45
1	40	45	35
_	30	35	25
	20	25	15
	100	110	90
	80 [※]	90	70
2	60 [※]	70	50
	4 0 [*]	45	35
	20 [*]	25	15
	120	130	110
	100 [※]	110	90
	80 [*]	90	70
3	60 ^{**}	70	50
	4 0 [*]	45	35
	20 ^{**}	25	15

[☆] Specified coast down speeds for motorcycles that have to drive the part in the "reduced speed" version.

Table B.5.5.-1: Coast-down time measurement beginning vehicle speed and ending vehicle speed.

4.3. When the running resistance is verified in accordance with point 4.2.2.3.2. of section B.2., the test can be executed at $v_j \pm 5$ km/h, provided that the coast-down time accuracy referred to in point 3.4.7. of section B.2. is ensured.

5. Measurement of coast-down time

- 5.1. After a warm-up period, the vehicle shall be accelerated to the coast-down starting vehicle speed, at which point the coast-down measurement procedure shall be started.
- 5.2. Since shifting the transmission to neutral can be dangerous and complicated by the construction of the vehicle, the coasting may be performed solely with the clutch disengaged. Vehicles that have no means of cutting the transmitted engine power off prior to coasting may be towed until they reach the coast-down starting

vehicle speed. When the coast-down test is reproduced on the chassis dynamometer, the drive train and clutch shall be in the same condition as during the road test.

- 5.3. The vehicle steering shall be altered as little as possible and the brakes shall not be operated until the end of the coast-down measurement period.
- 5.4. The first coast-down time Δt_{ai} corresponding to the specified vehicle speed v_j shall be measured as the time taken for the vehicle to decelerate from $v_j + \Delta v$ to $v_j \Delta v$.
- 5.5. The procedure described in points 5.1. to 5.4. shall be repeated in the opposite direction to measure the second coast-down time Δt_{bi} .
- 5.6. The average Δt_i of the two coast-down times Δt_{ai} and Δt_{bi} shall be calculated using the following equation:

Equation B.5.5.-2:

$$\Delta t_i = \frac{\Delta t_{ai} + \Delta t_{bi}}{2}$$

5.7. At least four tests shall be performed and the average coast-down time ΔT_j calculated using the following equation:

Equation B.5.5.-3

$$\Delta t_j = \frac{I}{n} \cdot \sum_{i=1}^n \Delta t_i$$

5.8. Tests shall be performed until the statistical accuracy P is equal to or less than 3% (P \leq 3%).

The statistical accuracy P (as a percentage) is calculated using the following equation:

Equation B.5.5.-4

$$P = \frac{t \cdot s}{\sqrt{n}} \cdot \frac{100}{\Delta t_i}$$

where:

t is the coefficient given in Table B.5.5.-2;

s is the standard deviation given by the following formula:

Equation B.5.5.-5

$$S = \sqrt{\sum_{i=1}^{n} \frac{\left(\Delta t_{i} - \Delta t_{j}\right)^{2}}{n - I}}$$

where:

n is the number of tests.

n	t	$\frac{t}{\sqrt{n}}$
4	3.2	1.60
5	2.8	1.25
6	2.6	1.06
7	2.5	0.94
8	2.4	0.85
9	2.3	0.77
10	2.3	0.73
11	2.2	0.66
12	2.2	0.64
13	2.2	0.61
14	2.2	0.59
15	2.2	0.57

Table B.5.5.-2: Coefficients for statistical accuracy

- 5.9. In repeating the test, care shall be taken to start the coast-down after observing the same warm-up procedure and at the same coast-down starting vehicle speed.
- 5.10. The coast-down times for multiple specified vehicle speeds may be measured in a continuous coast-down. In this case, the coast-down shall be repeated after observing the same warm-up procedure and at the same coast-down starting vehicle speed.
- 5.11. The coast-down time shall be recorded. A specimen record form is given in the Regulation for administrative requirements.

6. Data processing

- 6.1. Calculation of running resistance force
- 6.1.1. The running resistance force F_j , in Newton, at the specified vehicle speed v_j shall be calculated using the following equation:

Equation B.5.5.-6

$$F_{j} = \frac{1}{3.6} \cdot m_{ref} \cdot \frac{2 \cdot \Delta v}{\Delta t}$$

where:

 m_{ref} = reference mass (kg);

 Δv = vehicle speed deviation (km/h);

 Δt = calculated coast down time difference (s);

- 6.1.2. The running resistance force F₁ shall be corrected in accordance with point 6.2.
- 6.2. Running resistance curve fitting

The running resistance force F shall be calculated as follows:

6.2.1. The following equation shall be fitted to the data set of F_j and v_j obtained in points 6.1. and 4. respectively by linear regression to determine the coefficients f₀ and f₂,

Equation B.5.5.-7

$$F = f_0 + f_2 \times v^2$$

6.2.2. The coefficients f₀ and f₂ thus determined shall be corrected to the standard ambient conditions using the following equations:

Equation B.5.5.-8

$$f_0^* = f_0 [1 + K_0 (T_T - T_0)]$$

Equation B.5.5.-9

$$\mathbf{f^*}_2 = \mathbf{f}_2 \times \frac{\mathbf{T}_T}{\mathbf{T}_0} \times \frac{\mathbf{p}_0}{\mathbf{p}_T}$$

where:

 K_0 shall be determined on the basis of the empirical data for the particular vehicle and tyre tests or shall be assumed as follows, if the information is not available: $K_0 = 6 \cdot 10^{-3} \text{ K}^{-1}$.

6.3. Target running resistance force F* for chassis dynamometer setting

The target running resistance force $F^*(v_0)$ on the chassis dynamometer at the reference vehicle speed v_0 , in Newton, is determined using the following equation:

Equation B.5.5.-10

$$F^*(v_0) = f^*_0 + f^*_2 \times v_0^2$$

B.5.6. Annex: chassis dynamometer system

1. Specification

- 1.1. General requirements
- 1.1.1. The dynamometer shall be capable of simulating road load within one of the following classifications:
 - (a) dynamometer with fixed load curve, i.e. a dynamometer whose physical characteristics provide a fixed load curve shape;
 - (b) dynamometer with adjustable load curve, i.e. a dynamometer with at least two road load parameters that can be adjusted to shape the load curve.
- 1.1.2. Dynamometers with electric inertia simulation shall be demonstrated to be equivalent to mechanical inertia systems. The means by which equivalence is established are described in point 4.
- 1.1.3. Where the total resistance to progress on the road cannot be reproduced on the chassis dynamometer between vehicle speeds of 10 km/h and 120 km/h, it is recommended that a chassis dynamometer with the characteristics defined in point 1.2. should be used.
- 1.1.3.1. The load absorbed by the brake and the chassis dynamometer (internal frictional effects) between the vehicle speeds of 0 and 120 km/h is as follows:

Equation B.5.6.-1:

 $F = (a + b \cdot v^2) \pm 0.1 \cdot F_{80}$ (without being negative)

where:

F = total load absorbed by the chassis dynamometer (N);

a = value equivalent to rolling resistance (N);

b = value equivalent to coefficient of air resistance (N/(km/h)²);

v = vehicle speed (km/h);

 F_{80} = load at 80 km/h (N). Alternatively for vehicles that cannot attain 80 km/h the load at the reference vehicle speeds v_j in table B.5.6.-1 in Annex B.5.5. or B.5.6. as applicable shall be determined.

- 1.2. Specific requirements
- 1.2.1. The setting of the dynamometer shall not be affected by the lapse of time. It shall not produce any vibrations perceptible to the vehicle and likely to impair the vehicle's normal operations.
- 1.2.2. The chassis dynamometer may have one roller or two rollers in the cases of three-wheel vehicles with two front wheels and quadricycles. In such cases, the front roller shall drive, directly or indirectly, the inertial masses and the power-absorption device.
- 1.2.3. It shall be possible to measure and read the indicated load to an accuracy of ± 5

percent.

- 1.2.4. In the case of a dynamometer with a fixed load curve, the accuracy of the load setting at 80 km/h or of the load setting at the reference vehicle speeds (30 km/h, respectively 15 km/h) referred to in point 1.1.3.1. for vehicles that cannot attain 80 km/h, shall be ± 5 percent. In the case of a dynamometer with adjustable load curve, the accuracy of matching dynamometer load to road load shall be ± 5 percent for vehicle speeds > 20 km/h and \pm 10 percent for vehicle speeds \leq 20 km/h. Below this vehicle speed, dynamometer absorption shall be positive.
- 1.2.5. The total inertia of the rotating parts (including the simulated inertia where applicable) shall be known and shall be within \pm 10 kg of the inertia class for the test.
- 1.2.6. The speed of the vehicle shall be measured by the speed of rotation of the roller (the front roller in the case of a two-roller dynamometer from which the actual speed of the vehicle is calculated). It shall be measured with an accuracy of ± 1 km/h at vehicle speeds over 10 km/h. The distance actually driven by the vehicle shall be measured by the movement of rotation of the roller (the front roller in the case of a two-roller dynamometer).

2. Dynamometer calibration procedure

2.1. Introduction

This section describes the method to be used to determine the load absorbed by a dynamometer brake. The load absorbed comprises the load absorbed by frictional effects and the load absorbed by the power-absorption device. The dynamometer is brought into operation beyond the range of test vehicle speeds. The device used for starting up the dynamometer is then disconnected; the rotational speed of the driven roller decreases. The kinetic energy of the rollers is dissipated by the power-absorption unit and by the frictional effects. This method disregards variations in the roller's internal frictional effects caused by rollers with or without the vehicle. The frictional effects of the rear roller shall be disregarded when the roller is free.

2.2. Calibration of the load indicator at 80 km/h or of the load indicator referred to in point 1.1.3.1. for vehicles that cannot attain 80 km/h.

The following procedure shall be used for calibration of the load indicator to 80 km/h or the applicable load indicator referred to in point 1.1.3.1. for vehicles that cannot attain 80 km/h, as a function of the load absorbed (see also Figure B.5.6.-1):

- 2.2.1. Measure the rotational speed of the roller if this has not already been done. A fifth wheel, a revolution counter or some other method may be used.
- 2.2.2. Place the vehicle on the dynamometer or devise some other method for starting up the dynamometer.
- 2.2.3. Use the flywheel or any other system of inertia simulation for the particular inertia class to be used.

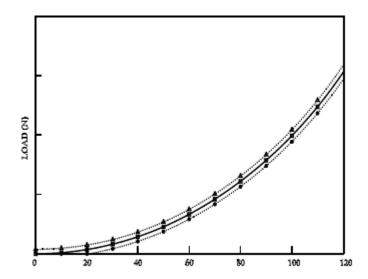


Figure B.5.6.-1: power absorbed by the chassis dynamometer Legend:

$$\Box F = a + b \cdot v^2$$
 $\bullet = (a + b \cdot v^2) - 0.1 \cdot F_{80}$ $\Delta = (a + b \cdot v^2) + 0.1 \cdot F_{80}$

- 2.2.4. Bring the dynamometer to a vehicle speed of 80 km/h or to the reference vehicle speed referred to in point 1.1.3.1. for vehicles that cannot attain 80 km/h.
- 2.2.5. Note the load indicated F_i (N).
- 2.2.6. Bring the dynamometer to a vehicle speed of 90 km/h or to the respective reference vehicle speed referred to in point 1.1.3.1. plus 5 km/h for vehicles that cannot attain 80 km/h
- 2.2.7. Disconnect the device used to start up the dynamometer.
- 2.2.8. Note the time taken by the dynamometer to pass from a vehicle speed of 85 to 75 km/h, or for vehicles that cannot attain 80 km/h referred to in Table B.5.5.1: of annex B.5.5., note the time between $v_i + 5$ km/h to v_{i-} 5 km/h.
- 2.2.9. Set the power-absorption device at a different level.
- 2.2.10. The requirements of points 2.2.4. to 2.2.9. shall be repeated sufficiently often to cover the range of loads used.
- 2.2.11. Calculate the load absorbed using the formula:

Equation B.5.6.-2:

$$F = \frac{m_i \cdot \Delta v}{\Delta t}$$

where:

F = load absorbed (N);

 m_i = equivalent inertia in kg (excluding the inertial effects of the free rear roller);

 Δ v = vehicle speed deviation in m/s (10 km/h = 2.775 m/s);

 Δ t = time taken by the roller to pass from 85 km/h to 75 km/h, or for vehicles that cannot attain 80 km/h from 35 – 25 km/h, respectively from 20 – 10 km/h, referred to in Table B.5.5. of Annex B.5.5.

2.2.12. Figure B.5.6.-2 shows the load indicated at 80 km/h in terms of load absorbed at 80 km/h.

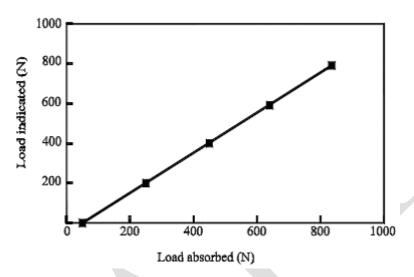


Figure B.5.6.-2: Load indicated at 80 km/h in terms of load absorbed at 80 km/h

- 2.2.13. The requirements laid down in points 2.2.3. to 2.2.12. shall be repeated for all inertia classes to be used.
- 2.3. Calibration of the load indicator at other vehicle speeds

 The procedures described in point 2.2. shall be repeated as often as necessary for the chosen vehicle speeds.
- 2.4. Calibration of force or torqueThe same procedure shall be used for force or torque calibration.

3. Verification of the load curve

3.1. Procedure

The load-absorption curve of the dynamometer from a reference setting at a vehicle speed of 80 km/h or for vehicles that cannot attain 80 km/h at the respective reference vehicle speeds referred to in point 1.1.3.1., shall be verified as follows:

- 3.1.1. Place the vehicle on the dynamometer or devise some other method for starting up the dynamometer.
- 3.1.2. Adjust the dynamometer to the absorbed load (F_{80}) at 80 km/h, or for vehicles that cannot attain 80 km/h to the absorbed load F_{vj} at the respective target vehicle speed v_i referred to in point 1.1.3.1.

- 3.1.3. Note the load absorbed at 120, 100, 80, 60, 40 and 20 km/h or for vehicles that cannot attain 80 km/h absorbed at the target vehicles speeds v_j referred to in point 1.1.3.1.
- 3.1.4. Draw the curve F(v) and verify that it corresponds to the requirements of point 1.1.3.1.
- 3.1.5. Repeat the procedure set out in points 3.1.1. to 3.1.4. for other values of F_{80} and for other values of inertia.

4 Verification of simulated inertia

4.1. Object

The method described in this Annex makes it possible to check that the simulated total inertia of the dynamometer is carried out satisfactorily in the running phase of the operating cycle. The manufacturer of the chassis dynamometer shall specify a method for verifying the specifications according to point 4.3.

4.2. Principle

4.2.1. Drawing-up working equations

Since the dynamometer is subjected to variations in the rotating speed of the roller(s), the force at the surface of the roller(s) can be expressed by:

Equation B.5.6.-3:

$$F = I \cdot \gamma = I_M \cdot \gamma + F_1$$

where:

F is the force at the surface of the roller(s) in N;

I is the total inertia of the dynamometer (equivalent inertia of the vehicle);

I_M is the inertia of the mechanical masses of the dynamometer;

γ is the tangential acceleration at roller surface;

 F_1 is the inertia force.

Note: An explanation of this formula with reference to dynamometers with mechanically simulated inertia is appended.

Thus, total inertia is expressed as follows:

Equation B.5.6.-4:

$$I = I_m + F_1 / \gamma$$

where:

I_m can be calculated or measured by traditional methods;

 F_1 can be measured on the dynamometer;

γ can be calculated from the peripheral rotation speed of the rollers.

The total inertia (I) will be determined during an acceleration or deceleration

test with values no lower than those obtained on an operating cycle.

4.2.2. Specification for the calculation of total inertia

The test and calculation methods shall make it possible to determine the total inertia I with a relative error $(\Delta I/I)$ of less than ± 2 percent.

- 4.3. Specification
- 4.3.1. The mass of the simulated total inertia I shall remain the same as the theoretical value of the equivalent inertia (see Annex B.5.4.) within the following limits:
- ± 5 percent of the theoretical value for each instantaneous value;
- 4.3.1.2. ±2 percent of the theoretical value for the average value calculated for each sequence of the cycle.

The limit specified in point 4.3.1.1. is brought to ± 50 percent for one second when starting and, for vehicles with manual transmission, for two seconds during gear changes.

- 4.4. Verification procedure
- 4.4.1. Verification is carried out during each test throughout the test cycles defined in Annex B.5.14.
- 4.4.2. However, if the requirements laid down in point 4.3. are met, with instantaneous accelerations which are at least three times greater or smaller than the values obtained in the sequences of the theoretical cycle, the verification described in point 4.4.1. will not be necessary.

B.5.7. Annex: exhaust dilution system

1. System specification

1.1. System overview

A full-flow exhaust dilution system shall be used. This requires that the vehicle exhaust be continuously diluted with ambient air under controlled conditions. The total volume of the mixture of exhaust and dilution air shall be measured and a continuously proportional sample of the volume shall be collected for analysis. The quantities of pollutants are determined from the sample concentrations, corrected for the pollutant content of the ambient air and the totalised flow over the test period. The exhaust dilution system shall consist of a transfer tube, a mixing chamber and dilution tunnel, a dilution air conditioning, a suction device and a flow measurement device. Sampling probes shall be fitted in the dilution tunnel as specified in B.2.3.4.3.12. The mixing chamber described in this point shall be a vessel, such as those illustrated in Figures B.5.7.-1 and B.5.7.-2, in which vehicle exhaust gases and the dilution air are combined so as to produce a homogeneous mixture at the chamber outlet.

1.2. General requirements

- 1.2.1. The vehicle exhaust gases shall be diluted with a sufficient amount of ambient air to prevent any water condensation in the sampling and measuring system under any conditions which may occur during a test.
- 1.2.2. The mixture of air and exhaust gases shall be homogeneous at the point where the sampling probe is located (see point 1.3.3.). The sampling probe shall extract a representative sample of the diluted exhaust gas.
- 1.2.3. The system shall enable the total volume of the diluted exhaust gases to be measured.
- 1.2.4. The sampling system shall be gas-tight. The design of the variable dilution sampling system and the materials that go to make it up shall be such that they do not affect the pollutant concentration in the diluted exhaust gases. Should any component in the system (heat exchanger, cyclone separator, blower, etc.) change the concentration of any of the pollutants in the diluted exhaust gases and the fault cannot be corrected, sampling for that pollutant shall be carried out upstream from that component.
- 1.2.5. All parts of the dilution system that are in contact with raw and diluted exhaust gas shall be designed to minimise deposition or alteration of the particulates or particles. All parts shall be made of electrically conductive materials that do not react with exhaust gas components and shall be electrically grounded to prevent electrostatic effects.

- 1.2.6. If the vehicle being tested is equipped with an exhaust pipe comprising several branches, the connecting tubes shall be connected as near as possible to the vehicle without adversely affecting its operation.
- 1.2.7. The variable-dilution system shall be designed so as to enable the exhaust gases to be sampled without appreciably changing the back-pressure at the exhaust pipe outlet.
- 1.2.8. The connecting tube between the vehicle and dilution system shall be so designed as to minimise heat loss.
- 1.3. Specific requirements
- 1.3.1. Connection to vehicle exhaust

The connecting tube between the vehicle exhaust outlets and the dilution system shall be as short as possible and satisfy the following requirements:

- (a) the tube shall be less than 3.6 m long, or less than 6.1 m long if heat insulated. Its internal diameter may not exceed 105 mm;
- (b) it shall not cause the static pressure at the exhaust outlets on the test vehicle to differ by more than ± 0.75 kPa at 50 km/h, or more than ± 1.25 kPa for the whole duration of the test, from the static pressures recorded when nothing is connected to the vehicle exhaust outlets. The pressure shall be measured in the exhaust outlet or in an extension having the same diameter, as near as possible to the end of the pipe. Sampling systems capable of maintaining the static pressure to within ± 0.25 kPa may be used if a written request from a manufacturer to the technical service substantiates the need for the closer tolerance;
- (c) it shall not change the nature of the exhaust gas;
- (d) any elastomeric connectors employed shall be as thermally stable as possible and have minimum exposure to the exhaust gases.

1.3.2. Dilution air conditioning

The dilution air used for the primary dilution of the exhaust in the CVS tunnel shall be passed through a medium capable of reducing particles in the most penetrating particle size of the filter material by \geq 99.95 percent, or through a filter of at least class H13 of EN 1822:1998. This represents the specification of High Efficiency Particulate Air (HEPA) filters. The dilution air may be charcoal scrubbed before being passed to the HEPA filter. It is recommended that an additional coarse particle filter is situated before the HEPA filter and after the charcoal scrubber, if used. At the vehicle manufacturer's request, the dilution air may be sampled according to good engineering practice to determine the tunnel contribution to background particulate mass levels, which can then be subtracted from the values measured in the diluted exhaust.

1.3.3. Dilution tunnel

Provision shall be made for the vehicle exhaust gases and the dilution air to be mixed. A mixing orifice may be used. In order to minimise the effects on the conditions at the exhaust outlet and to limit the drop in pressure inside the dilution-air conditioning device, if any, the pressure at the mixing point shall

not differ by more than ± 0.25 kPa from atmospheric pressure. The homogeneity of the mixture in any cross-section at the location of the sampling probe shall not vary by more than ± 2 percent from the average of the values obtained for at least five points located at equal intervals on the diameter of the gas stream. For particulate and particle emissions sampling, a dilution tunnel shall be used which:

- (a) shall consist of a straight tube of electrically-conductive material, which shall be earthed;
- (b) shall be small enough in diameter to cause turbulent flow (Reynolds number ≥ 4000) and of sufficient length to cause complete mixing of the exhaust and dilution air;
- (c) shall be at least 200 mm in diameter;
- (d) may be insulated.

1.3.4. Suction device

This device may have a range of fixed rotation speeds to ensure sufficient flow to prevent any water condensation. This result is generally obtained if the flow is either:

- (a) twice the maximum flow of exhaust gas produced by accelerations of the driving cycle; or
- (b) sufficient to ensure that the CO₂ concentration in the dilute exhaust sample bag is less than 3 percent by volume for petrol and diesel.

1.3.5. Volume measurement in the primary dilution system

The method for measuring total dilute exhaust volume incorporated in the constant volume sampler shall be such that measurement is accurate to \pm 2 percent under all operating conditions. If the device cannot compensate for variations in the temperature of the mixture of exhaust gases and dilution air at the measuring point, a heat exchanger shall be used to maintain the temperature to within ± 6 °C of the specified operating temperature. If necessary, some form of protection for the volume measuring device may be used, e.g. a cyclone separator, bulk stream filter, etc. A temperature sensor shall be installed immediately before the volume measuring device. This sensor shall have an accuracy and a precision of ± 1 °C and a response time of 0.1 s at 62 percent of a given temperature variation (value measured in silicone oil). The difference from atmospheric pressure shall be measured upstream and, if necessary, downstream from the volume measuring device. The pressure measurements shall have a precision and an accuracy of ± 0.4 kPa during the test.

1.4. Recommended system descriptions

Figure B.5.7.-1 and Figure B.5.7.-2 are schematic drawings of two types of recommended exhaust dilution systems that meet the requirements of this Annex. Since various configurations can produce accurate results, exact conformity with these figures is not essential. Additional components such as

instruments, valves, solenoids and switches may be used to provide additional information and coordinate the functions of the component system.

1.4.1. Full-flow dilution system with positive displacement pump

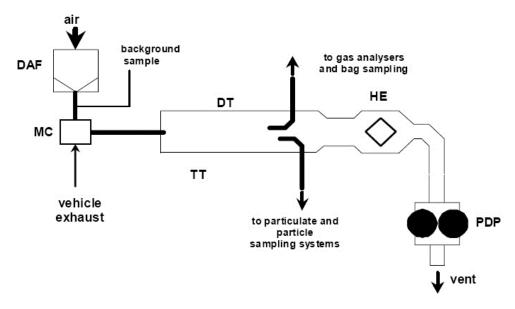


Figure B.5.7.-1: Positive displacement pump dilution system

The positive displacement pump (PDP) full-flow dilution system satisfies the requirements of this Annex by metering the flow of gas through the pump at constant temperature and pressure. The total volume is measured by counting the revolutions of the calibrated positive displacement pump. The proportional sample is achieved by sampling with pump, flow meter and flow control valve at a constant flow rate. The collecting equipment consists of:

- 1.4.1.1. A filter (refer to DAF in Figure B.5.7.-1) for the dilution air shall be installed, which can be preheated if necessary. This filter shall consist of the following filters in sequence: an optional activated charcoal filter (inlet side) and a high efficiency particulate air (HEPA) filter (outlet side). It is recommended that an additional coarse particle filter is situated before the HEPA filter and after the charcoal filter, if used. The purpose of the charcoal filter is to reduce and stabilise the hydrocarbon concentrations of ambient emissions in the dilution air;
- 1.4.1.2. A transfer tube (TT) by which vehicle exhaust is admitted into a dilution tunnel (DT) in which the exhaust gas and dilution air are mixed homogeneously;
- 1.4.1.3. The positive displacement pump (PDP), producing a constant-volume flow of the air/exhaust-gas mixture. The PDP revolutions, together with associated temperature and pressure measurement, are used to determine the flow rate;
- 1.4.1.4. A heat exchanger (HE) of a capacity sufficient to ensure that throughout the test the temperature of the air/exhaust-gas mixture measured at a point immediately upstream of the positive displacement pump is within 6.0 °C of the average operating temperature during the test. This device shall not affect the pollutant concentrations of diluted gases taken off afterwards for analysis.

- 1.4.1.5. A mixing chamber (MC) in which exhaust gas and air are mixed homogeneously and which may be located close to the vehicle so that the length of the transfer tube (TT) is minimised.
- 1.4.2. Full-flow dilution system with critical-flow venturi

Critical-Flow Venturi Dilution System

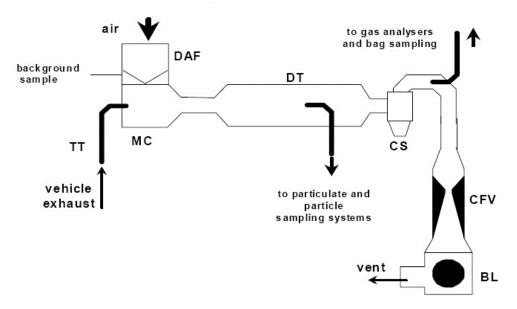


Figure B.5.7.-2: Critical-flow venturi dilution system

The use of a critical-flow venturi (CFV) for the full-flow dilution system is based on the principles of flow mechanics for critical flow. The variable mixture flow rate of dilution and exhaust gas is maintained at sonic velocity which is directly proportional to the square root of the gas temperature. Flow is continually monitored, computed and integrated throughout the test. The use of an additional critical-flow sampling venturi ensures the proportionality of the gas samples taken from the dilution tunnel. As pressure and temperature are both equal at the two venturi inlets, the volume of the gas flow diverted for sampling is proportional to the total volume of diluted exhaust-gas mixture produced, and thus the requirements of this Annex are met. The collecting equipment consists of:

- 1.4.2.1. A filter (DAF) for the dilution air which can be preheated if necessary. This filter shall consist of the following filters in sequence: an optional activated charcoal filter (inlet side) and a high efficiency particulate air (HEPA) filter (outlet side). It is recommended that an additional coarse particle filter is situated before the HEPA filter and after the charcoal filter, if used. The purpose of the charcoal filter is to reduce and stabilise the hydrocarbon concentrations of ambient emissions in the dilution air;
- 1.4.2.2. A mixing chamber (MC) in which exhaust gas and air are mixed homogeneously and which may be located close to the vehicle so that the

length of the transfer tube (TT) is minimised;

- 1.4.2.3. A dilution tunnel (DT) from which particulates and particles are sampled;
- 1.4.2.4. Some form of protection for the measurement system may be used, e.g. a cyclone separator, bulk stream filter, etc.;
- 1.4.2.5. A measuring critical-flow venturi tube (CFV) to measure the flow volume of the diluted exhaust gas;
- 1.4.2.6. A blower (BL) of sufficient capacity to handle the total volume of diluted exhaust gas.

2. CVS calibration procedure

2.1. General requirements

The CVS system shall be calibrated by using an accurate flow-meter and a restricting device. The flow through the system shall be measured at various pressure readings and the control parameters of the system measured and related to the flows. The flow-meter shall be dynamic and suitable for the high flow-rate encountered in CVS testing. The device shall be of certified accuracy traceable to an approved national or international standard.

- 2.1.1. Various types of flow-meter may be used, e.g. calibrated venturi, laminar flow-meter, calibrated turbine-meter, provided that they are dynamic measurement systems and can meet the requirements of point 1.3.5. of this Annex.
- 2.1.2. The following points give details of methods of calibrating PDP and CFV units, using a laminar flow-meter which gives the required accuracy, together with a statistical check on the calibration validity.
- 2.2. Calibration of the positive displacement pump (PDP)
- 2.2.1. The following calibration procedure outlines the equipment, the test configuration and the various parameters that are measured to establish the flow-rate of the CVS pump. All the parameters relating to the pump are simultaneously measured with the parameters relating to the flow-meter which is connected in series with the pump. The calculated flow rate (given in m³/min at pump inlet, absolute pressure and temperature) can then be plotted against a correlation function that is the value of a specific combination of pump parameters. The linear equation that relates the pump flow and the correlation function is then determined. If a CVS has a multiple rotation speed drive, a calibration shall be performed for each range used.
- 2.2.2. This calibration procedure is based on the measurement of the absolute values of the pump and flow-meter parameters that relate to the flow rate at each point. Three conditions shall be maintained to ensure the accuracy and integrity of the calibration curve:
- 2.2.2.1. The pump pressures shall be measured at tappings on the pump rather than at the external piping on the pump inlet and outlet. Pressure taps that are mounted at the top centre and bottom centre of the pump drive head plate are exposed to

the actual pump cavity pressures and therefore reflect the absolute pressure differentials;

- 2.2.2.2. Temperature stability shall be maintained during the calibration. The laminar flow-meter is sensitive to inlet temperature oscillations which cause the data points to be scattered. Gradual changes of ± 1 °C in temperature are acceptable as long as they occur over a period of several minutes;
- 2.2.2.3. All connections between the flow-meter and the CVS pump shall be free of any leakage.
- 2.2.3. During an exhaust emission test, the measurement of these same pump parameters enables the user to calculate the flow rate from the calibration equation.
- 2.2.4. Figure B.5.7.-3 of this Annex shows one possible test set-up. Variations are permissible, provided that the technical service approves them as being of comparable accuracy. If the set-up shown in Figure B.5.7.-3 is used, the following data shall be found within the limits of precision given:

Barometric pressure (corrected) (P_b) ±0.03 kPa

Ambient temperature (T) ± 0.2 °C

Air temperature at LFE (ETI) \pm 0.15 °C

Pressure depression upstream of LFE (EPI) ±0.01 kPa

Pressure drop across the LFE matrix (EDP) ±0.0015 kPa

Air temperature at CVS pump inlet (PTI) ± 0.2 °C

Air temperature at CVS pump outlet (PTO) ± 0.2 °C

Pressure depression at CVS pump inlet (PPI) ±0.22 kPa

Pressure head at CVS pump outlet (PPO) ±0.22 kPa

Pump revolutions during test period (n) $\pm 1 \text{ min}^{-1}$

Elapsed time for period (minimum 250 s) (t) ± 0.1 s

Figure 8
PDP Calibration Configuration

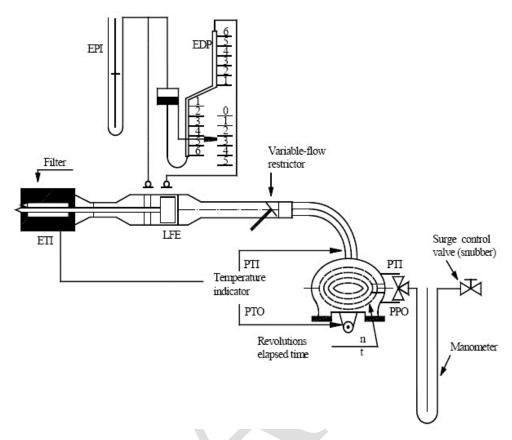


Figure B.5.7.-3 PDP calibration configuration

- 2.2.5. After the system has been connected as shown in Figure B.5.7.-3, set the variable restrictor in the wide-open position and run the CVS pump for 20 minutes before starting the calibration.
- 2.2.6. Reset the restrictor valve to a more restricted condition in an increment of pump inlet depression (about 1 kPa) that will yield a minimum of six data points for the total calibration. Allow the system to stabilise for three minutes and repeat the data acquisition.
- 2.2.7. The air flow rate (Qs) at each test point is calculated in standard m³/min from the flow-meter data using the manufacturer's prescribed method.
- 2.2.8. The air flow-rate is then converted to pump flow (V0) in m³/rev at absolute pump inlet temperature and pressure.

Equation B.5.7.-1:

$$V_0 = \frac{Q_s}{n} \cdot \frac{T_p}{273.2} \cdot \frac{101.33}{P_p}$$

where:

 $V_0 = \text{pump flow rate at } T_p \text{ and } P_p \text{ (m}^3/\text{rev)};$

Qs = air flow at 101.33 kPa and 0 °C in (m 3 /min);

 $T_p = \text{pump inlet temperature } (K);$

 P_p = absolute pump inlet pressure (kPa);

n = pump rotation speed (min-1).

2.2.9.

To compensate for the interaction of pump rotation speed pressure variations at the pump and the pump slip rate, the correlation function (x_0) between the pump rotation speed (n), the pressure differential from pump inlet to pump outlet, and the absolute pump outlet pressure is calculated as follows:

Equation B.5.7.-2:

$$x_0 = \frac{1}{n} \sqrt{\frac{\Delta P_p}{P_p}}$$

where:

 $x_0 = correlation function;$

 ΔP_p = pressure differential from pump inlet to pump outlet (kPa);

 P_e = absolute outlet pressure (PPO + P_b) (kPa).

2.2.9.1. A linear least-square fit is performed to generate the calibration equations which have the formula:

Equation B.5.7.-3:

$$V_0 = D_0 - M(x_0)$$

$$n = A - B (\Delta P_p)$$

D₀, M, A and B are the slope-intercept constants describing the lines.

- 2.2.10. A CVS system that has multiple pump rotation speeds shall be calibrated on each rotation speed used. The calibration curves generated for the ranges shall be approximately parallel and the intercept values (D0) shall increase as the pump flow range decreases.
- 2.2.11 If the calibration has been performed carefully, the calculated values from the equation will be within 0.5 percent of the measured value of V0.Values of M will vary from one pump to another. Calibration is performed at pump start-up and after major maintenance.
- 2.3. Calibration of the critical-flow venturi (CFV)
- 2.3.1. Calibration of the CFV is based on the flow equation for a critical-flow venturi: Equation B.5.7.-4

$$Q_s = \frac{K_{\pi}P}{\sqrt{T}}$$

where:

 $Q_s = flow;$

 K_v = calibration coefficient;

P = absolute pressure (kPa);

T = absolute temperature (K).

Gas flow is a function of inlet pressure and temperature. The calibration procedure described in points 2.3.2. to 2.3.7. shall establish the value of the calibration coefficient at measured values of pressure, temperature and air flow.

- 2.3.2. The manufacturer's recommended procedure shall be followed for calibrating electronic portions of the CFV.
- 2.3.3. Measurements for flow calibration of the critical-flow venturi are required and the following data shall be found within the limits of precision given:

Barometric pressure (corrected) (Pb) ±0.03 kPa

LFE air temperature, flow-meter (ETI) ± 0.15 °C

Pressure depression upstream of LFE (EPI) ±0.01 kPa

Pressure drop across (EDP) LFE matrix ±0.0015 kPa

Air flow (Qs) ± 0.5 percent

CFV inlet depression (PPI) ±0.02 kPa

Temperature at venturi inlet (Tv) ± 0.2 °C.

2.3.4. The equipment shall be set up as shown in Figure B.5.7.-4 and checked for leaks. Any leaks between the flow-measuring device and the critical-flow venturi will seriously affect the accuracy of the calibration.

CFV Calibration Configuration

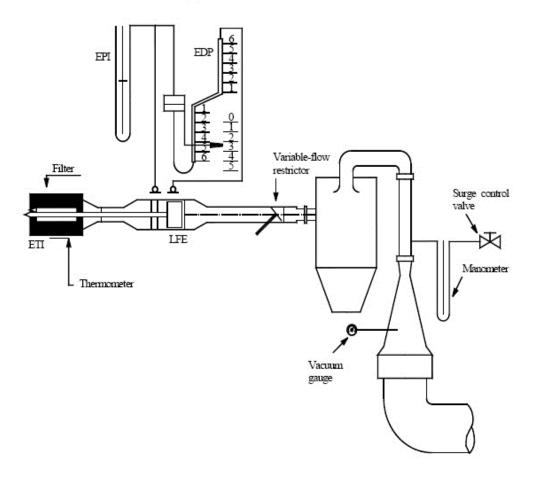


Figure B.5.7.-4 CFV calibration configuration

- 2.3.5. The variable-flow restrictor shall be set to the open position, the blower shall be started and the system stabilised. Data from all instruments shall be recorded.
- 2.3.6. The flow restrictor shall be varied and at least eight readings shall be taken across the critical flow range of the venturi.
- 2.3.7. The data recorded during the calibration shall be used in the following calculations. The air flow-rate (Qs) at each test point is calculated from the flow-meter data using the manufacturer's prescribed method. Calculate values of the calibration coefficient (K_v) for each test point:

Equation B.5.8.-5:

$$K_{\pi} = \frac{Q_{s} \sqrt{T_{\pi}}}{P_{\pi}}$$

where:

 $Q_s = \text{flow-rate in m}^3/\text{min at } 0 \, ^{\circ}\text{C} \text{ and } 101.3 \text{ kPa};$

 T_v = temperature at the venturi inlet (K);

 P_v = absolute pressure at the venturi inlet (kPa).

Plot K_v as a function of venturi inlet pressure. For sonic flow, K_v will have a relatively constant value. As pressure decreases (vacuum increases), the venturi becomes unchoked and K_v decreases. The resultant K_v changes are not permissible. For a minimum of eight points in the critical region, calculate an average K_v and the standard deviation. If the standard deviation exceeds 0.3 percent of the average K_v , take corrective action.

3. System verification procedure

3.1. General requirements

The total accuracy of the CVS sampling system and analytical system shall be determined by introducing a known mass of a pollutant gas into the system while it is being operated as if during a normal test and then analysing and calculating the pollutant mass according to the formula in point 4, except that the density of propane shall be taken as 1.967 grams per litre at standard conditions. The two techniques described in points 3.2. and 3.3. are known to give sufficient accuracy. The maximum permissible deviation between the quantity of gas introduced and the quantity of gas measured is 5 percent.

3.2. CFO method

- 3.2.1. Metering a constant flow of pure gas (CO or C₃H₈) using a critical-flow orifice device
- 3.2.2. A known quantity of pure gas (CO or C₃H₈) is fed into the CVS system through the calibrated critical orifice. If the inlet pressure is high enough, the flow-rate (q), which is adjusted by means of the critical-flow orifice, is independent of orifice outlet pressure (critical flow). If deviations exceeding 5 percent occur, the cause of the malfunction shall be determined and corrected. The CVS system is operated as in an exhaust emission test for about five to ten minutes. The gas collected in the sampling bag is analysed by the usual equipment and the results compared to the concentration of the gas samples which was known beforehand.

3.3. Gravimetric method

- 3.3.1. Metering a limited quantity of pure gas (CO or C₃H₈) by means of a gravimetric technique
- 3.3.2. The following gravimetric procedure may be used to verify the CVS system. The weight of a small cylinder filled with either carbon monoxide or propane is determined with a precision of ± 0.01 g. For about five to ten minutes, the CVS system is operated as in a normal exhaust emission test, while CO or propane is injected into the system. The quantity of pure gas involved is determined by means of differential weighing. The gas accumulated in the bag is analysed using the equipment normally used for exhaust-gas analysis. The results are then compared to the concentration figures computed previously.

B.5.8. <u>Annex: [approval] / [certification] tests of a replacement pollution-control device type as separate technical unit</u>

1. Scope of the annex

This Annex applies to the [approval] / [certification] of pollution control devices as separate technical units to be fitted as replacement parts on one or more types of vehicle.

- 2. Application for environmental performance [approval] / [certification]
- 2.1. Applications for [approval] / [certification] of a type of replacement pollution-control device as a separate technical unit shall be submitted by the manufacturer of the system or by his authorised representative.
- 2.2. A model for the information document is referred to in Annex B.5.11.
- 2.3. For each type of replacement pollution-control device for which [approval] / [certification] is requested, the [approval] / [certification] application shall be accompanied by the following documents in triplicate, and by the following particulars:
- 2.3.1. A description of the types of vehicles for which the device is intended, in terms of its characteristics;
- 2.3.2. The numbers or symbols specific to the propulsion unit and vehicle type;
- 2.3.3. Description of the replacement catalytic converter type stating the relative position of each of its components, together with the fitting instructions;
- 2.3.4. Drawings of each component to facilitate location and identification, and statement of materials used. These drawings shall also indicate the intended location of the mandatory [approval] / [certification] mark.
- 2.4. The following shall be submitted to the technical service responsible for the [approval] / [certification] test:
- 2.4.1. Vehicle(s) of a type [approved] / [certified] in accordance with this annex equipped with a new original equipment pollution-control device type. This (these) vehicles shall be selected by the applicant with the agreement of the technical service to the satisfaction of the [approval authority] / [certification authority]. It (they) shall comply with the requirements of the type I test set out in section B.2.
- 2.4.2 The test vehicles shall be without emission control system defects and be properly maintained and used; any excessively worn out or malfunctioning emission-related original part shall be repaired or replaced. The test vehicles shall be tuned properly and set to the manufacturer's specification prior to emission testing.

2.4.3. One sample of the type of the replacement pollution-control device type. This sample shall be clearly and indelibly marked with the applicant's trade name or mark and its commercial designation.

3. Requirements

3.1. General requirements

The design, construction and mounting of the replacement pollution-control device type shall be such that:

- 3.1.1. the vehicle complies with the requirements of this GTR under normal conditions of use, and in particular regardless of any vibrations to which it may be subjected;
- 3.1.2. the replacement pollution control device displays reasonable resistance to the corrosion phenomena to which it is exposed, with due regard to the normal conditions of use of the vehicle:
- 3.1.3. the ground clearance available with the original equipment pollution-control device type and the angle at which the vehicle can lean over are not reduced;
- 3.1.4. the surface of the device does not reach unduly high temperatures;
- 3.1.5. the outline of the device has no projections or sharp edges;
- 3.1.6. shock absorbers and suspension have adequate clearance;
- 3.1.7. adequate safety clearance is provided for pipes;
- 3.1.8. the replacement pollution-control device is impact-resistant in a way that is compatible with clearly-defined maintenance and installation requirements;
- 3.1.9. if the original equipment pollution-control includes thermal protection, the replacement pollution control device shall include equivalent protection;
- 3.1.10. if (an) oxygen probe(s) and other sensors or actuators are originally installed on the exhaust line, the replacement pollution-control device type shall be installed at exactly the same position as the original equipment pollution-control device and the position on the exhaust line of the oxygen probe(s) and other sensors or actuators shall not be modified.
- 3.2. Requirements regarding emissions
- 3.2.1. The vehicle referred to in point 2.4.1, equipped with a replacement pollution-control device of the type for which [approval] / [certification] is requested, shall undergo the tests laid down in sections B.2., B.3, B.4. and B.4. (depending on the [approval] / [certification] of the vehicle)¹.
- 3.2.1.1. Evaluation of pollutant emissions from vehicles equipped with replacement

¹As provided for in this GTR in the version applicable to the type-approval of that vehicle.

pollution-control devices

Requirements regarding tailpipe or evaporative emissions are deemed to be complied with if the test vehicle equipped with the replacement pollutant-control device complies with the limit values in point 9. of section B.1. (according to the [approval] / [certification] of the vehicle)¹.

- Where the [approval] / [certification] application is for different types of vehicles from the same manufacturer, the type I test may be limited to as few as two vehicles selected after agreement with the technical service to the satisfaction of the [approval authority] / [certification authority], provided that the different types of vehicle are fitted with the same type of original equipment pollution-control device.
- 3.2.2. Requirements regarding permissible sound level
 - The vehicles referred to in point 2.4.1, equipped with a replacement pollution control device type that could allow worse noise emissions than the type for which [approval] / [certification] is requested, shall satisfy the applicable requirements of UN Regulations No 9, 41, 63 or 92. The test result for the vehicle in motion and for the stationary test shall be mentioned in the test report.
- 3.3. Testing of the propulsion unit performance of the vehicle
- 3.3.1. The replacement pollution-control device type shall be such as to ensure that the propulsion unit performance of the vehicle is comparable with that achieved with the original equipment pollution-control device type.
- 3.3.2. The propulsion unit performance of the vehicle equipped with the replacement pollution-control device shall be compared with that of an original equipment pollution-control device, also in new condition, fitted in turn to the vehicle referred to in point 2.4.1.
- 3.3.3. The maximum net power and maximum net torque as well as the maximum design vehicle speed, if applicable, measured with the replacement pollution-control device, shall not deviate by more than + 5% from those measured under the same conditions with the [approved] / [certified] original equipment pollution-control device type.

B.5.9. 1. <u>Annex: vehicle propulsion unit family with regard to environmental performance demonstration tests</u>

1. 2. Introduction

- 1.1. 3. In order to alleviate the test burden on manufacturers when demonstrating the environmental performance of vehicles these may be grouped as a vehicle propulsion unit family. One or more parent vehicles shall be selected from this group of vehicles by the manufacturer to the satisfaction of the [approval authority] / [certification authority] that shall be used to demonstrate environmental performance test types I, II and VII.
- 1.2. 4. A light motor vehicle may continue to be regarded as belonging to the same vehicle propulsion unit family provided that the vehicle variant, version, propulsion unit, pollution-control system listed in table B.5.9.-1 are identical or remain within the prescribed and declared tolerances.
- 1.3. Vehicle and propulsion unit family attribution with regard to environmental tests
 - 6. For the environmental test types I, II and VII a representative parent vehicle shall be selected within the boundaries set by the classification criteria laid down in point 2.

2. Classification criteria

7. ('X' in the following table means 'applicable')

8.	9. Classification criteria description	10. Test type I	11. Test type	12. Test type
1.	Vehicle			
1.1.	category;	X	X	X
1.2.	sub-category;	X	X	X
1.3.	the inertia of a vehicle variant(s) or version(s) within two inertia categories above or below the nominal inertia category;	X		X
1.4.	overall gear ratios (+/- 8%);	X		X
2.	Propulsion family characteristics			
2.3.	number of cylinders of the combustion engine;	X	X	X
2.4.	engine capacity (+/- 2 %) ⁽¹⁾ of the combustion engine;	X	X	X
2.5.	number and control (variable cam phasing or lift) of combustion engine valves;	X	X	X

2.6.	monofuel / bifuel / flex fuel H ₂ NG / multifuel;			X
2.7.	fuel system (carburettor / scavenging port / port fuel injection / direct fuel injection / common rail / pump-injector / other);		X	X
2.8.	fuel storage ⁽²⁾ ;		14.	15.
2.9.	16. type of cooling system of combustion engine;	X	X	X
2.10.	17. combustion cycle (PI / CI / two-stroke / four-stroke / other);	X	X	X
2.11.	18. intake air system (naturally aspirated / charged (turbocharger / super-charger) / intercooler / boost control) and air induction control (mechanical throttle / electronic throttle control / no throttle);	X	X	X
19.	Pollution control system characteristics			
20. .1.	21. propulsion unit exhaust (not) equipped with catalytic converter(s);	X	X	X
3.1.	22. catalytic converter(s) type;	X	X	X
23. .1.1.	24. number and elements of catalytic converters;	X	X	X
25. .1.2.	26. size of catalytic converters (volume of monolith(s) +/-15 %);	X	X	X
27. .1.3.	28. operation principle of catalytic activity (oxidising, three-way, heated, SCR, other.);	X	X	X
29. .1.4.	30. precious metal load (identical or higher);	X	X	X
31.	32. precious metal ratio (+/- 15 %);	X	X	X
33. .1.5.	34. substrate (structure and material);	X	X	X
35. .1.6.	36. cell density;	X	X	X
37. .1.7.	38. type of casing for the catalytic converter(s);	X	X	X
39. .2.	40. propulsion unit exhaust (not) equipped with particulate filter (PF);	X	X	X
3.2.1.	41. PF types;	X	X	X

	3.2.2.	42. number and elements of PF;	X	X	X
	3.2.3.	43. size of PF (volume of filter element +/- 10 %);	X	X	X
	3.2.4.	44. operation principle of PF (partial / wall-flow / other);	X	X	X
	3.2.5.	45. active surface of PF;	X	X	X
	46. .3.	47. Propulsion unit (not) equipped with periodically regenerating system;	X	X	X
	3.3.1.	48. periodically regenerating system type;	X	X	X
	3.3.2.	49. operation principle of periodically regenerating system;	X	X	X
	50. .4.	51. propulsion (not) equipped with selective catalytic converter reduction (SCR) system;	X	X	X
	3.4.1.	52. SCR system type;	X	X	X
	3.4.2.	53. operation principle of periodically regenerating system;	X	X	X
	54. .5.	55. Propulsion unit (not) equipped with lean NOx trap /absorber;	X	X	X
	56. .5.1.	57. lean NOx trap / absorber type;	X	X	X
	58. .5.2.	59. operation principle of lean NOx trap / absorber;	X	X	X
4	60. .6.	Propulsion unit (not) equipped with a cold-start device or starting aid device(s);	X	X	X
	61.	cold-start or starting aid device type;	X	X	X
	62. .6.2.	operation principle of cold start or starting aid device(s);	X	X	X
	63. .6.3.	Activation time of cold-start or starting aid device(s) and /or duty cycle (only limited time activated after cold start / continuous operation);	X	X	X
	64. .7.	propulsion unit (not) equipped with O2 sensor for fuel control;	X	X	X
	65. .7.1.	O ₂ sensor types;	X	X	X
	66. .7.2.	operation principle of O ₂ sensor (binary / wide range / other);	X	X	X
	67. .7.3.	68. O ₂ sensor interaction with closed-loop fuelling system (stoichiometry / lean or rich operation);	X	X	X
	69.	propulsion unit (not) equipped with exhaust gas recirculation	X	X	X

(EGR) system;							
EGR system types;	X	X	X				
operation principle of EGR system (internal / external);	X	X	X				
maximum EGR rate (+/- 5 %);	X	X	X				
72. Explanatory notes: (1) maximum 30% acceptable for test type VIII (2) Only for vehicles equipped with storage for gaseous fuel							
	EGR system types; operation principle of EGR system (internal / external); maximum EGR rate (+/- 5 %); Explanatory notes:	EGR system types; operation principle of EGR system (internal / external); maximum EGR rate (+/- 5 %); Explanatory notes:	EGR system types; operation principle of EGR system (internal / external); x x maximum EGR rate (+/- 5 %); Explanatory notes:				

Table B.5.9.-1: Classification criteria propulsion unit family with regard to test types I, II and VII

B.5.10. Annex: information document containing the essential characteristics of the propulsion units and the pollutant control systems

1. The manufacturer shall complete the applicable item numbers of the list below, and submit it as part of the information folder.

Item No.	(Sub) categories	Detailed information
0.		GENERAL INFORMATION
A.		General information concerning vehicles
0.1.	L1e L7e	Make (trade name of manufacturer):
0.2.	L1e	Type:
0.2.1	Lle L7e	Variant(s):
0.2.2	Lle L7e	Version(s):
0.2.3.	L1e L7e	Commercial name(s) (if available):
0.3.	L1e L7e	Category, subcategory and sub-subcategory of vehicle:
0.4.	L1e L7e	Company name and address of manufacturer:
0.4.1.	L1e L7e	Name(s) and address(es) of assembly plants:
0.4.2.	L1e L7e	Name and address of manufacturer's authorised representative, if any:
0.5.	L1e L7e	Manufacturer's statutory plate(s):
0.5.1.	Lle L7e	Location of the manufacturer's statutory plate:
0.5.2.	Lle L7e	Method of attachment:
0.5.3.	Lle L7e	Photographs and/or drawings of the statutory plate (completed example with dimensions):
0.6.	L1e L7e	Location of the vehicle identification number:
0.6.1.	L1e L7e	Photographs and/or drawings of the locations of the vehicle identification number (completed example with dimensions):
0.6.1.1.	L1e — L7e	The serial number of the type begins with:

General information concerning systems, components or separate technical

B.

units

0.7.	L1e L7e	Make(s) (trade name(s) of manufacturer):				
0.8.	L1e L7e Type:					
0.8.1.	L1e L7e	L1e L7e Commercial name(s) (if available):				
0.8.2.	Lle L7e	Type-approval number(s) (if available):				
0.8.3.	L1e — L7e	Type-approval(s) issued on (date, if available):				
0.9.	Lle — L7e	Company name and address of manufacturer:				
0.9.1.	L1e	Name(s) and address(es) of assembly plants:				
0.9.2.	L1e	Name and address of manufacturer's authorised representative, if any:				
0.10.		Vehicle(s) for which the system/separate technical unit is intended for (21):				
0.10.1.	Lle L7e	Type:				
0.10.2.	L1e L7e	Variant:				
0.10.3.	Lle L7e	Version:				
0.10.4.	Lle L7e	Commercial name(s) (if available):				
0.10.5.	Lle L7e	Category, subcategory and sub-subcategory of vehicle:				
0.11.	L1e — L7e	Type-approval marks for components and separate technical units:				
0.11.1.	L1e L7e	Method of attachment:				
0.11.2.	Lle L7e	Photographs and/or drawings of the location of the type-approval mark (completed example with dimensions):				
С.		General information regarding conformity of production				
0.12.		Conformity of production				
0.12.1.	L1e	Description of overall quality-assurance management systems.				
1.		GENERAL CONSTRUCTION CHARACTERISTICS				
1.1.	L1e L7e	Photographs and/or drawings of a representative vehicle:				
1.2.	L1e L7e	Scale drawing of the whole vehicle:				
1.3.	L1e L7e	Number of axles and wheels:				
1.3.1.	Lle L7e	Axles with twinned wheels:				

1.3.2.	L1e L7e	Powered axles:
1.4.	L1e L7e	Chassis (if any) (overall drawing):
1.5.	L2e, L5e B, L6e B, L7e A2, L7e B2, L7e C	Material used for the bodywork:
1.6.	L1e L7e	Position and arrangement of the propulsion unit(s):
1.7.	L4e, L5e B, L6e- B, L7e A2, L7e B2, L7e C	Hand of drive: left/right/centre ⁽⁴⁾ :
1.7.1.	L1e L7e	Vehicle is equipped to be driven in right/left-hand traffic and in countries that use metric/metric and imperial units. (4):
1.8.		Propulsion unit performance
1.8.1.	L3e, L4e, L5e, L7e A, L7e B2	Declared maximum vehicle speed:km/h
1.8.2.	L1e, L2e, L6e, L7e B1, L7e C	Maximum design vehicle speed (22): km/h and gear in which it is reached:
1.8.3.	L1e L7e	Maximum net power combustion engine: kW at min ⁻¹ at A/F ratio:
1.8.4.	Lle L7e	Maximum net torque combustion engine:Nm atmin ⁻¹ at A/F ratio:
2.		MASSES AND DIMENSIONS
		(in kg and mm.) refer to drawings where applicable
2.1		Range of vehicle mass (overall)
2.1.1.	L1e L7e	Mass in running order: kg
2.1.1.1.	Lle L7e	Distribution of mass in running order between the axles: kg
2.1.2.	Lle L7e	Actual mass: kg
2.1.8.	Lle L7e	Mass of the optional equipment: kg
2.1.9.	Lle L7e	Mass of the superstructure: kg
2.1.10.	Lle L7e	Mass of the propulsion battery: kg
2.1.11.	10 14	Mass of the doors: kg
	L2e, L4e L5e, L6e L7e	<u> </u>

2.1.13.	Lle L7e	Mass of the gaseous fuel system as well as storage tanks for gaseous fuel: kg	
2.1.14.	Lle L7e	Mass of the storage tanks to store compressed air: kg	
2.1.15.	Lle L7e	Reference mass: kg	
2.2.		Range of vehicle dimensions (overall)	
2.2.1.	L1e L7e	Length: mm	
2.2.2.	Lle L7e	Width: mm	
2.2.3.	Lle L7e	Height: mm	
2.2.4.	Lle L7e	Wheelbase: mm	
2.2.4.1.	L/1e	Wheelbase sidecar: mm	
2.2.5.		Track width	
2.2.5.1.	L1e L7e if equipped with twinned wheels L2e, L4e, L5e, L6e, L7e	Track width front: mm.	
2.2.5.2.	L1e L7e if equipped with twinned wheels	Track width rear: mm.	
2.2.5.3.	L2e, L4e, L5e, L6e, L7e	Track width sidecar: mm.	
2.2.6.	L7e B	Front overhang: mm.	
2.2.7.	L7e B	Rear overhang: mm.	
2.2.8.		Load platform dimensions	
2.2.8.1.	L2e U, L5e B, L6e BU, L7e B2, L7e CU	Length of the load platform: mm	
2.2.8.2.	L2e U, L5e B, L6e BU, L7e B2, L7e CU	Width of load platform: mm	
2.2.8.3.	L2e U, L5e- B, L6e BU, L7e B2, L7e-	Height of load platform: mm	

CU 2.2.9.9. Seat height: mm L3e-AxT 2.2.9.10. L3e-AxE, Ground clearance: mm L3e AxT GENERAL POWERTRAIN CHARACTERISTICS 3. 3.1 Manufacturer of the propulsion unit 3.1.1. Combustion engine Lle L7e 3.1.1.1. Manufacturer: Engine code (as marked on the engine or other means of identification): 3.1.1.2. L1e L7e 3.1.1.3. L1e L7e Fuel identification marking (if available): 3.1.1.4. L1e L7e Photographs and/or drawings of the location of the code(s) and/or type-approval numbers (completed example with dimensions)⁽²⁰⁾:.... 3.2. **Combustion engine** 3.2.1. Specific engine information 3.2.1.1. L1e L7e Number of combustion engines: L1e L7e Working principle: internal combustion engine (ICE)/positive ignition/compression 3.2.1.2. ignition /external combustion engine (ECE)/turbine/compressed air⁽⁴⁾: 3.2.1.3. Lle L7e Cycle: four-stroke/two-stroke/rotary/other: Lle L7e 3.2.1.4. Cylinders 3.2.1.4.1. L1e L7e Number: 3.2.1.4.2. Lle L7e Arrangement: 3.2.1.4.3. Lle L7e Bore: mm 3.2.1.4.4. L1e L7e Stroke:.... mm 3.2.1.4.5. Lle L7e Number and configuration of stators in the case of rotary-piston engine: Lle L7e 3.2.1.4.6. Volume of combustion chambers in the case of rotary-piston engine:cm³ 3.2.1.4.7. Lle L7e Firing order: 3.2.1.5. L1e L7e Engine capacity:cm³ L1e L7e 3.2.1.6. Volumetric compression ratio: 3.2.1.7. Number of inlet and exhaust valves L1e L7e * 3.2.1.7.1. Number and minimum cross-sectional areas of inlet and outlet ports: * 3.2.1.7.2. Lle L7e Valve timing or equivalent data:

* 3.2.1.7.3.	L1e L7e	Maximum lift of valves, angles of opening and closing, or timing details of alternative distribution systems, in relation to dead centres. For variable timing system, minimum and maximum timing:		
* 3.2.1.7.4.	L1e L7e	Reference and/or setting ranges:		
3.2.1.8.	L1e L7e	Drawings of combustion chamber, cylinder head, piston, piston rings:		
3.2.1.9.	L1e L7e	Normal warm engine idling speed: min ⁻¹		
3.2.1.10.	L1e L7e	Stop-start system: yes/no		
*3.2.2.		Powertrain/propulsion unit/drive-train management system		
3.2.2.1.	L1e L7e	$\label{eq:pcus} PCUs/ECUs \ \ software \ \ identification \ number(s): \ \ and \ \ calibration \ verification \ number(s):$		
3.2.3.		Fuel		
3.2.3.1.	L1e L7e	Fuel type:		
3.2.3.2	L1e L7e	Vehicle fuel configuration: mono-fuel/bi- fuel/flex fuel		
3.2.3.2.1.	L1e L7e	Maximum amount of bio-fuel acceptable in fuel:% by volume		
3.2.4.		Fuel pressure delivery and control		
3.2.4.1.	L1e L7e	Brief description and schematic drawing of low-and/or high-pressure fuelling wet system(s):		
3.2.4.2.	L1e L7e	Low- and/or high-pressure fuel pump(s): yes/no		
3.2.4.2.1.	L1e L7e	Fuel pump control: mechanical/on/off electric/continuous operation/electronically controlled variable operation:		
3.2.4.2.2.	L1e L7e	For CI combustion engines and dual fuel engines only maximum fuel delivery: g/s or mm ³ /stroke or cycle at an engine speed of:min ⁻¹ or, alternatively, a characteristic diagram:		
		(When boost control is supplied, state the characteristic fuel delivery and boost pressure versus engine speed)		
3.2.4.3.	L1e L7e	Common rail: yes/no		
3.2.4.4.	L1e L7e	Fuel distributor/rail/hoses: yes/no		
3.2.4.5.	L1e L7e	Fuel pressure and/or fuel flow regulator(s): yes/no		
3.2.5.		Fuel mass metering and control		
3.2.5.1.	L1e L7e	By carburettor(s): yes/no		
* 3.2.5.1.1.	L1e L7e	Operating principle and construction:		
* 3.2.5.1.2.	L1e L7e	Maximum fuel-flow rate: g/s at maximum power and torque:		

3.2.5.1.3.	L1e L7e	Carburettor(s) settings:
* 3.2.5.1.4.	L1e L7e	Carburettor diffusers:
* 3.2.5.1.5.	L1e L7e	Carburettor fuel-level in float chamber:
* 3.2.5.1.5.1.	L1e L7e	Carburettor mass of float:
3.2.5.1.6.	L1e L7e	Carburettor cold-starting system: manual/automatic: yes/no
3.2.5.1.6.1.	L1e L7e	Carburettor cold-starting system operating principle(s):
3.2.5.1.7.	L1e L7e	Mixture scavenging port: yes/no
3.2.5.1.7.1.	L1e L7e	Mixture scavenging port dimensions:
3.2.5.2.	Lle L7e	By mechanically/hydraulically controlled fuel injection: yes/no
3.2.5.2.1.	L1e L7e	Operation principle:
3.2.5.2.2.	L1e L7e	Mechanical/electronic adjustment of maximum fuel mass delivery: yes/no
3.2.5.3.	L1e L7e	By electronically controlled fuel injection system: yes/no
3.2.5.3.1.	L1e L7e	Operation principle: port injection/direct injection/pre-chamber/swirl chamber:
3.2.5.3.2.	L1e L7e	Fuel injector(s): single-/multi-point/direct injection/other (specify):
3.2.5.3.3.	Lle L7e	Total and per cylinder amount of fuel injectors:
3.2.5.4.	Lle L7e	Air-assisted fuel injector: yes/no:
3.2.5.4.1.	Lle L7e	Description and operating pressure of air-assist:
3.2.5.5.	Lle L7e	Cold start system: yes/no
3.2.5.5.1.	Lle L7e	Description of cold start system:
3.2.5.6.	Lle L7e	Auxiliary starting aid: yes/no
3.2.5.7.	Lle L7e	CI injection specific: yes/no
3.2.5.7.1.	Lle L7e	Static injection timing:
3.2.5.7.2.	Lle L7e	Injection advance curve:
3.2.6.		Gaseous fuelling system and control
3.2.6.1.	L1e L7e	Brief description and schematic drawing of gaseous fuelling system(s):
3.2.6.2.1.	L1e L7e	Type-approval number according to UN Regulation No 67:
3.2.7.		Air-induction system
3.2.7.1.	L1e L7e	Brief description and schematic drawing of gaseous intake air-flow and induction system:
3.2.7.2.	L1e L7e	Intake manifold description and working principle (e.g. fixed length/variable

		length/swirl valves) ⁽⁴⁾ (include detailed drawings and/or photos):	
* 3.2.7.2.1.	L1e L7e	Description and drawings of inlet pipes and their accessories (plenum chamber, heating device with control strategy, additional air intakes, etc.):	
3.2.7.3.	L1e L7e	Intake air pressure charger: yes/no	
3.2.7.3.1.	L1e L7e	Brief description and schematic drawing of the intake air-pressure charger system:	
3.2.7.3.2.	L1e L7e	Working and control principles:	
3.2.7.3.3.	L1e L7e	Type(s) (turbo or supercharger, other):	
3.2.7.3.4.	L1e L7e	Maximum intake air-charge pressure and flow-rate at maximum torque and power:kPa and g/s or charge pressure and flow-rate map:kPa and g/s	
3.2.7.4.	L1e L7e	Waste gate: yes/no	
3.2.7.5.	L1e L7e	Intercooler: yes/no	
3.2.7.5.1.	L1e L7e	Type: air-air/air-water/other	
* 3.2.7.5.2.	L1e L7e	Intake depression at rated engine speed and at 100% load (compression ignition engines only): kPa	
3.2.7.6.	L1e L7e	Air filter, (drawings, photographs):	
3.2.7.7.	Lle L7e	Intake air-silencer description (drawings, photographs):	
*3.2.7.7.1.	Lle L7e	Working principle:	
3.2.8.		Air-mass metering and control	
3.2.8.1.	L1e L7e	Brief description and schematic drawing of air-mass metering and control system:	
3.2.8.2.	Lle L7e	Mechanical throttle body: yes/no	
3.2.8.3.	Lle L7e	Electronic throttle control (ETC): yes/no	
3.2.8.3.1.	Lle L7e	Schematic drawing of electronic throttle control:	
* 3.2.8.3.1.2.	L1e L7e	Description of ETC hardware redundancies regarding sensors/actuators/electric power/ground/control electronics:	
3.2.9.		Spark delivery system and control	
3.2.9.1.	L1e L7e	Brief description and schematic drawing of spark delivery and control system:	
3.2.9.1.1.	Lle L7e	Working principle:	
* 3.2.9.1.2.	L1e L7e	Ignition advance curve or map at wide open throttle:	
3.2.9.1.3.	L1e L7e	Static ignition timing: degrees before TDC at maximum torque and power	
3.2.9.2.	L1e L7e	Ion sense capability: yes/no	

3.2.9.3.	Lle L7e	Spark plugs:		
3.2.9.3.1.	L1e L7e	Gap setting:mm		
3.2.9.4.	Lle L7e	gnition coil(s):		
* 3.2.9.4.1.	L1e L7e	Vorking principle:		
* 3.2.9.4.2.	Lle L7e	Dwell angle and timing at wide open throttle:		
3.2.10.		Powertrain cooling system and control		
3.2.10.1.	Lle L7e	Brief description and schematic drawing of powertrain cooling and control system:		
3.2.10.2.	Lle L7e	Cooling system: liquid: yes/no		
3.2.10.2.1.	Lle L7e	Maximum temperature at outlet: °C		
3.2.10.2.2.	L1e — L7e	Nominal setting of the engine temperature control mechanism:		
3.2.10.2.3.	L1e L7e	Nature of liquid:		
3.2.10.2.4.	L1e L7e	Circulating pump(s): yes/no		
3.2.10.2.4.1.	L1e L7e	Characteristics:		
3.2.10.2.5.	Lle L7e	Drive ratio(s):		
3.2.10.2.6.	Lle L7e	Description of the fan and its drive mechanism:		
3.2.10.3.	L1e L7e	Air cooling: yes/no		
3.2.10.3.1.	Lle L7e	Reference point:		
3.2.10.3.2.	Lle L7e	Maximum temperature at reference point:°C		
3.2.10.3.3.	L1e L7e	Fan: yes/no		
3.2.10.3.3.1.	Lle L7e	Characteristics:		
3.2.10.3.3.2.	L1e L7e	Drive ratio(s):		
3.2.11.		Powertrain lubrication system and control		
3.2.11.1.	L1e L7e	Brief description and schematic drawing of powertrain lubrication and control system:		
3.2.11.2.	L1e L7e	Lubrication system configuration(s) (wet sump, dry sump, other, pump/injection into induction system/mixed with the fuel, etc.):		
3.2.11.3.	L1e L7e	Location of oil reservoir (if any):		
3.2.11.4.	L1e L7e	Feed system (pump/injection into induction system/mixed with the fuel, etc.):		
3.2.11.5.	L1e L7e	Lubricating pump: yes/no		
3.2.11.6.	L1e L7e	Oil cooler: yes/no		
3.2.11.6.1.	L1e L7e	Drawing		

3.2.11.7.	L1e L7e	Lubricant(s) characteristics:	
3.2.11.8.	L1e L7e	Lubricant mixed with the fuel: yes/no:	
3.2.11.8.1.	L1e L7e	Percentage range of lubricant mixed with the fuel:	
3.2.12.		Exhaust system and control	
3.2.12.1.	L1e L7e	Brief description and schematic drawing of exhaust devices for noise and tailpipe emission control:	
3.2.12.2.	L1e L7e	Description and drawing of the exhaust manifold:	
3.2.12.3.	L1e L7e	Description and detailed drawing of the exhaust device:	
3.2.12.4.	L1e L7e	Maximum permissible exhaust back-pressure at rated engine speed and at 100% load: kPa	
3.2.12.5.	Lle L7e	Type, marking of exhaust noise-abatement device(s):	
* 3.2.12.6.	L1e L7e	Noise-reducing measures in the engine compartment and on the engine where relevant for external noise:	
3.2.12.7.	L1e L7e	Location of the exhaust outlet:	
3.2.12.8.	L1e L7e	Exhaust noise abatement device containing fibrous materials: yes/no:	
3.2.13.		Other electrical systems and control than those intended for the electrical propulsion unit	
3.2.13. 3.2.13.1.	Lle L7e	· ·	
	Lle L7e	propulsion unit	
3.2.13.1.		Propulsion unit Rated voltage: V, positive/negative ground	
3.2.13.1. 3.2.13.2.	L1e L7e	propulsion unit Rated voltage: V, positive/negative ground Generator: yes/no:	
3.2.13.1. 3.2.13.2. 3.2.13.2.1.	Lle L7e	Propulsion unit Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA	
3.2.13.1. 3.2.13.2. 3.2.13.2.1. 3.2.13.3.	Lle L7e Lle L7e Lle L7e	Propulsion unit Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA Battery(ies): yes/no	
3.2.13.1. 3.2.13.2. 3.2.13.2.1. 3.2.13.3. 3.2.13.3.1.	Lle L7e Lle L7e Lle L7e Lle L7e	Propulsion unit Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA Battery(ies): yes/no Capacity and other characteristics (mass,):	
3.2.13.1. 3.2.13.2. 3.2.13.2.1. 3.2.13.3. 3.2.13.3.1. 3.2.13.4.	Lle L7e Lle L7e Lle L7e Lle L7e	Propulsion unit Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA Battery(ies): yes/no Capacity and other characteristics (mass,):	
3.2.13.1. 3.2.13.2. 3.2.13.2.1. 3.2.13.3. 3.2.13.3.1. 3.2.13.4.	Lle L7e Lle L7e Lle L7e Lle L7e	Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA Battery(ies): yes/no Capacity and other characteristics (mass,):	
3.2.13.1. 3.2.13.2. 3.2.13.2.1. 3.2.13.3. 3.2.13.3.1. 3.2.13.4. 3.4.1.	Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e	Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA Battery(ies): yes/no Capacity and other characteristics (mass,):	
3.2.13.1. 3.2.13.2.1 3.2.13.3. 3.2.13.3.1. 3.2.13.4. 3.4.1. 3.4.1.1.	Lle L7e	Rated voltage: V, positive/negative ground Generator: yes/no: Nominal output: VA Battery(ies): yes/no Capacity and other characteristics (mass,):	

3.4.1.2.2.	L1e L7e	Maximum temperature at reference point: °C		
3.4.2.		Lubrication system		
3.4.2.1.	L1e L7e	Description of lubrication system:		
3.4.2.2.	Lle L7e	Location of oil reservoir (if any):		
3.4.2.3.	L1e L7e	Feed system (pump/injection into induction system/mixed with the fuel, etc.):		
3.4.2.4.	L1e - L7e	Lubricant mixed with the fuel:		
3.4.2.4.1.	L1e L7e	Percentage:		
3.4.2.5.	Lle L7e	Oil cooler: yes/no:		
*3.4.2.5.1.	Lle L7e	Drawing(s):		
3.5.		Drive-train and control)		
3.5.1.	L1e L7e	Brief description and schematic drawing of the vehicle drive-train and its control system (gear shift control, clutch control or any other element of drive-train):		
3.5.2.		Clutch		
3.5.2.1.	L1e L7e	Brief description and schematic drawing of the clutch and its control system:		
3.5.3.		Transmission		
3.5.3.1.	L1e L7e	Brief description and schematic drawing of gear shift system(s) and its control:		
3.5.3.2.	L1e L7e	Drawing of the transmission:		
3.5.3.3.	Lle L7e	Type (mechanical, hydraulic, electric, manual/manual automated/automatic/CVT/other (indicate).):		
3.5.3.4.	Lle L7e	A brief description of the electrical/electronic components (if any):		
3.5.3.5.	Lle L7e	Location relative to the engine:		
3.5.3.6.	L1e L7e	Method of control:		
3.5.4.		Gear ratios		
	Lle I7e			

Overview gear ratios

Gear	Internal transmission ratios (ratios of engine to transmission output shaft revolutions)	Final drive ratio(s) (ratio of transmission output shaft to driven wheel revolutions)	Total gear ratios	Ratio (engine speed/vehicle speed) for manual transmission only
Maximum for CVT (*)				

		2
		3
		Minimum for CVT(+)
		Reverse
		(*) Continuously variable transmission
3.5.4.1.	L3e AxE, L3e AxT	Final drive ratio:
3.5.4.2.	L3e AxE, L3e AxT	Overall gear ratio in highest gear:
3.6.		Cycles designed to pedal
3.6.1.	Lle	Ratio manpower/electric power:
3.6.2.	Lle	Maximum assistance factor::
3.6.3.	Lle	Maximum vehicle speed for which the electric motor gives assistance:km/h
3.6.4.	Lle	Switch off distance:km
4.		GENERAL INFORMATION ON ENVIRONMENTAL AND PROPULSION PERFORMANCE
4.0		General information on environmental and propulsion unit performance
4.0 4.0.1.	L1e L7e	General information on environmental and propulsion unit performance Environmental step: Euro
	Lle L7e	
4.0.1.	Lle L7e	Environmental step: Euro (3/4/5)
4.0.1. 4.1.		Environmental step: Euro
4.0.1. 4.1. 4.1.1.		Environmental step: Euro
4.0.1. 4.1. 4.1.1. 4.1.2.	Lle L7e	Environmental step: Euro
4.0.1. 4.1. 4.1.1. 4.1.2. 4.1.2.1.	Lle L7e	Environmental step: Euro
4.0.1. 4.1. 4.1.2. 4.1.2.1.	Lle L7e Lle L7e	Environmental step: Euro
4.0.1. 4.1. 4.1.1. 4.1.2. 4.1.2.1. 4.1.2.2. 4.1.2.3.	Lle L7e Lle L7e Lle L7e Lle L7e	Environmental step: Euro
4.0.1. 4.1. 4.1.1. 4.1.2. 4.1.2.1. 4.1.2.2. 4.1.2.3. * 4.1.2.4.	Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e	Environmental step: Euro
4.0.1. 4.1. 4.1.1. 4.1.2. 4.1.2.1. 4.1.2.2. 4.1.2.3. * 4.1.2.4. * 4.1.2.5.	Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e	Environmental step: Euro

4.1.2.9.	L1e L7e	Location of the catalytic converter(s) (place and reference distance in the exhaust line):
4.1.2.10.	Lle L7e	Catalyst heat-shield: yes/no
4.1.2.11.	L1e L7e	Brief description and schematic drawing of the regeneration system/method of exhaust after-treatment systems and its control system:
*4.1.2.11.1.	Lle L7e	Normal operating temperature range:°C
4.1.2.11.2.	Lle L7e	Consumable reagents: yes/no
4.1.2.11.3.	L1e L7e	Brief description and schematic drawing of the reagent flow (wet) system and its control system:
4.1.2.11.4.	L1e L7e	Type and concentration of reagent needed for catalytic action:
*4.1.2.11.5.	Lle L7e	Normal operational temperature range of reagent:°C
4.1.2.11.6.	Lle L7e	Frequency of reagent refill: continuous/maintenance
4.1.2.12.	Lle L7e	Identifying part number:
4.1.3.		Oxygen sensor(s)
4.1.3.1.	L1e L7e	Oxygen sensor component(s) drawing(s):
4.1.3.2.	L1e—L7e	Drawing of exhaust device with oxygen sensor location(s) (dimensions relative to exhaust valves):
4.1.3.3.	L1e L7e	Control range(s):
4.1.3.3. 4.1.3.4.	Lle L7e	Control range(s): Identifying part number(s):
4.1.3.4.	L1e L7e	Identifying part number(s):
4.1.3.4. 4.1.3.5.	Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy:
4.1.3.4. 4.1.3.5. 4.1.3.6.	Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4.	Lle L7e Lle L7e Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no Secondary air-injection (air-inject in exhaust) Brief description and schematic drawing of the secondary air-injection system and its
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4. 4.1.4.1.	Lle L7e Lle L7e Lle L7e Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no Secondary air-injection (air-inject in exhaust) Brief description and schematic drawing of the secondary air-injection system and its control system:
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4. 4.1.4.1.	Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no Secondary air-injection (air-inject in exhaust) Brief description and schematic drawing of the secondary air-injection system and its control system: Configuration (mechanical, pulse air, air pump etc.):
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4. 4.1.4.1. 4.1.4.2. 4.1.4.3.	Lle L7e Lle L7e Lle L7e Lle L7e Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no Secondary air-injection (air-inject in exhaust) Brief description and schematic drawing of the secondary air-injection system and its control system: Configuration (mechanical, pulse air, air pump etc.): Working principle:
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4. 4.1.4.1. 4.1.4.2. 4.1.4.3. 4.1.5.	Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no Secondary air-injection (air-inject in exhaust) Brief description and schematic drawing of the secondary air-injection system and its control system: Configuration (mechanical, pulse air, air pump etc.): Working principle: External exhaust gas recirculation (EGR) Brief description and schematic drawing of the EGR system (exhaust flow) and its
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4. 4.1.4.1. 4.1.4.2. 4.1.4.3. 4.1.5.	Lle L7e	Identifying part number(s): Description of oxygen sensor heating system and heating strategy: Oxygen sensor heat shield(s): yes/no Secondary air-injection (air-inject in exhaust) Brief description and schematic drawing of the secondary air-injection system and its control system: Configuration (mechanical, pulse air, air pump etc.): Working principle: External exhaust gas recirculation (EGR) Brief description and schematic drawing of the EGR system (exhaust flow) and its control system:
4.1.3.4. 4.1.3.5. 4.1.3.6. 4.1.4. 4.1.4.1. 4.1.4.2. 4.1.4.3. 4.1.5.1. 4.1.5.2.	Lle L7e	Identifying part number(s):

4.1.6.1.	L1e L7e	PT component drawing with dimensions, shape and capacity of the particulate filter:
4.1.6.2.	L1e L7e	Design of the particulate filter:
4.1.6.3.	L1e L7e	Brief description and schematic drawing of the particulate filter and its control system:
4.1.6.4.	Lle L7e	Location (reference distance in the exhaust line):
4.1.6.5.	Lle L7e	Method or system of regeneration, description and drawing::
4.1.6.6.	L1e L7e	Identifying part number:
4.1.7.		Lean NOx trap
4.1.7.1.	L1e L7e	Operation principle of lean NOx trap:
4.1.8.		Additional tailpipe emission-control devices (if any not covered under another heading)
4.1.8.1.	Lle L7e	Working principle:
5.		VEHICLE PROPULSION FAMILY
5.1.	Lle L7e	To define the vehicle propulsion unit family, the manufacturer shall submit the information required for classification criteria set out in point 2 of point B.5.9., if not already provided in the information document.

B.5.11. <u>Annex: test result reporting requirements and information concerning the conduct of tests</u>

- 1. General requirements for the format of test reports
- 1.1. The test reports shall comply with the provisions of Standard EN ISO/IEC 17025:2005. In particular it shall include the information mentioned in point 5.10.2, including footnote (1) of that standard.
- 1.2. The template of the test reports shall be drawn up by the [approval authority] / [certification authority] in accordance with its rules of good practice.
- 1.3. The test report shall be drafted in one of the official languages of the country where [approval] / [certification] is sought.
- 1.3.1. Where a test has been carried out in a country other than the one handling the [approval] / [certification] application, the [approval authority] / [certification authority] may require the applicant to provide a certified translation of the test report.
- 1.4. Only authenticated copies of a test report shall be submitted.
- 1.5. The test reports shall include a description of the vehicle tested including its unambiguous identification. The parts having significant influence role in determining the test results shall be described and their identification number indicated.

Examples of parts include the silencers for noise measurement and the engine management system (ECU) for measuring tailpipe emissions.

Moreover it shall include at least the following information:

- 1.5.1. A detailed description of the characteristics of the vehicle, system, component or separate technical unit characteristics in connection with the regulatory act;
- 1.5.2. Category of vehicle tested;
- 1.5.3. The information shall indicate the variant and/or version to which it applies. One version shall not have more than one test result. However, a combination of several test results per version, indicating the worst case, is permissible. In this case, a note shall state that for items marked (*) only worst-case results are given.
- 1.5.4. When the tests are conducted on a vehicle, system, component or technical unit which combines a number of least favourable features concerning the required performance level (the worst-case), the test report shall include a reference stating how the selection was made by the manufacturer in agreement with the technical service.
- 1.5.5. Condition of the vehicle influencing the test, such as fitted accessories; actual masses; test voltage; tyre sizes; tyre pressures; etc.;
- 1.5.6. <u>Identification of the system, component or separate technical unit tested;</u>

- 1.5.7. Ambient conditions influencing the test: steam pressure (kPa); relative humidity (%); ambient temperature (°C); wind speed and direction on test track (km/h), etc.;
- 1.5.8. The measurement results specified in the relevant regulatory acts and, where required, the limits or thresholds to be met;
- 1.5.9. With regard to each measurement mentioned in point 1.5.5., the relevant decision: passed or failed;
- 1.5.10. A detailed statement of compliance with the various provisions to be met, i.e. provisions for which measurements were not required.
- 1.5.11. When test methods other than those prescribed in the regulatory acts are permitted, the report shall describe the test method used. The same applies when alternative provisions to those in the regulatory acts may be applied;
- 1.5.12. The number of photographs to be taken during testing shall be decided by the [approval authority] / [certification authority]. In the case of virtual testing, screen prints or other suitable evidence may replace photographs;
- 1.5.13. Technical service and persons responsible for carrying out the test and their position in the organisation;
- 1.5.14. Conclusions drawn up;
- 1.5.15. When opinions, assumptions and interpretations have been made, they shall be documented properly and marked as such in the test report.
- 2. Minimum information to be included in the test reports
- 2.1. In addition to the general requirements set out in point 1., the test reports shall contain as a minimum the information set out in point 2.2. This information can be grouped in an executive summary of the test report(s) applicable to the vehicle, system, component and separate technical unit, or be included in the test report(s) itself/themselves.
- 2.2. Minimum information of the test reports by subject as follows:
- 2.2.1. Generic information on environmental performance

The test report shall contain the following generic test data (only needed once per test type):

- 2.2.1.1. Description of propulsion unit, propulsion unit family and drive train of test vehicle(s) Error!

 Bookmark not defined.
- 2.2.1.2. Emission level of test vehicle: Euro 3, Euro 4, Euro 5 Error! Bookmark not defined. Error! Bookmark not defined.
- 2.2.1.3. Description of emission test bench(es), specifications and settings Error! Bookmark not defined.

2.2.1.4.	Chassis/engine dynamometer(s) specifications Error! Bookmark not defined.
2.2.1.5.	Inertia (reference) mass and running resistance settings for single/dual Error! Bookmark not defined chassis dynamometer Error! Bookmark not defined.
2.2.1.6.	Comprehensive report of road test results for the determination of test bench settings, including coast down times for single/dual Error! Bookmark not defined. roll chassis dynamometer Error! Bookmark not defined.
2.2.1.7.	Applicable test type I driving schedule (ECE R40 (with/without EUDC), ECE R47, WMTC stage 1, WMTC stage 2, revised WMTC) Error! Bookmark not defined. Error! Bookmark not defined.
2.2.1.8.	Description gearshift prescriptions for environmental testing Error! Bookmark not defined.
2.2.2.	Test type I: requirements: tailpipe emissions after cold start
	The following items specific to test type I shall be provided Error! Bookmark not defined.
2.2.2.1.	Description of tested vehicle(s) (prototype(s) or series production, hardware and software levels, VIN) Error! Bookmark not defined.
2.2.2.2.	Any deviations by test vehicle(s) from data provided in information document, section B.5.11.: yes/no Error! Bookmark not defined. Error! Bookmark not defined. If yes, please provide list with deviations.
2.2.2.3.	[Approval] / [Certification] number if not parent vehicle Error! Bookmark not defined.
2.2.2.4.	Mileage(s) of test vehicle(s) Error! Bookmark not defined.
2.2.2.5.	Test fuel(s) used Error! Bookmark not defined.
2.2.2.7.	Description of test type I measurement methods for gas fuelled vehicles referred to in section B.2.2. Error! Bookmark not defined.
2.2.2.8.	Description of test type I measurement methods for vehicles equipped with a periodically regenerating system referred to in section B.2.3. Error! Bookmark not defined.
2.2.2.9.	Information on regeneration strategy Error! Bookmark not defined.
	D (number of operating cycles between 2 cycles when regenerative phases occur) Error! Bookmark not defined.
	d (number of operating cycles required for regeneration) Error! Bookmark not defined.
2.2.2.10.	Description of weighting of type I test results as referred to in point 5.1.1.5. of section B.2. including equation number and weighting factors Error! Bookmark not defined.
2.2.2.11.	Number of type I operating cycles between two cycles where regenerative phases occur under the conditions equivalent to type I test (Distance 'D' in Figure B.2.3. 1 in section B.2.3.) Error! Bookmark not defined.
2.2.2.12.	Description of method employed to determine the number of cycles between two cycles where regenerative phases occur Error! Bookmark not defined.
2.2.2.13.	Parameters to determine the level of loading required before regeneration occurs (i.e. temperature, pressure etc.) Error! Bookmark not defined.

- 2.2.2.14. Description of method used to load system in the test procedure described in point 3.1. of section B.2.3. Error! Bookmark not defined.
- 2.2.2.15. Test records according to point 6. of section B.2. Error! Bookmark not defined.
- 2.2.2.16. Type I test results Error! Bookmark not defined.

Test Type I Test Results (TR _{TTIs})	Test No	co	THC	NMHC	NOx	THC + NOx	PM	
	1							
TR _{TTI Measured x} (i) (iv) (mg/km)	2							
	3							
TR _{TTI Measured x Mean} (i) (iv)								
(mg/km) K _i ⁽ⁱ⁾ (v)(vii) (no unit)						(ii)		
TR _{ITIx} (i)(vi)= K _i ··TR _{ITI} Measured x Mean (mg/km) & (% of L _x)						(iii)		
Limit value L _x (viii) (mg/km)								
(ii) (iii) (iv) (v) (vi) (viii)	Where applicable. Not applicable. Mean value calculated by adding mean values (M · K _i) calculated for THC and NOx. Round to 2 decimal places. Round to 4 decimal places. Round to 0 decimal places. (vii) Set K _i = 1 in case: (a) the vehicle is <u>not</u> equipped with a periodically regenerating emission abatement system or; (b) the vehicle is <u>not</u> a hybrid electric vehicle. Test limit x set out in point 9. of section B.1. x = 1 to 4 and refers to the numbering of the pollutant constituents in point 9. of section B.1., e.g. the Euro 5 limit for CO is referred to as L _i , the limit for THC is referred to as L ₂ , the limit for NO _x as L ₂ and the limit for PM as L ₄ .							
			x measuremen					

Table B.5.11. 1: Test type I results

2.2.3. Test type II requirements: Tailpipe emissions at (increased idle)/free acceleration

- 2.2.3.1. Details of test vehicle(s) if different from vehicle used for type I testing Error! Bookmark not defined.; (items 2.2.2.1. to 2.2.2.4. where different):
- 2.2.3.2. Description of propulsion unit idling activation method in case of stop_start system Error! Bookmark not defined.

2.2.3.3. Type II test results Error! Bookmark not defined.

Test	CO (% vol.)	Lambda	Engine speed (min-)	Engine oil temperature (°C)	Measured & corrected value of absorption coefficient (m-1)
------	--	--------	---------------------------	-----------------------------------	--

PI: Low idle					-
PI: High idle test					-
CI Free acceleration test / Smoke opacity test results	-	-	-	-	

Table B.5.11. 2: Test type II results

2.2.5. Test type VII requirements: Measurement of CO₂ emissions and fuel consumption

- 2.2.5.1. Details of test vehicle(s), its powertrain and pollution control devices explicitly documented and listed, emission test laboratory equipment and settings if different from data reported under items 2.2.2.1. to 2.2.2.10. Error! Bookmark not defined.
- 2.2.5.2. Documentation added according to UN Regulation No 101 (OJ L 138, 26.5.2012, p. 1): yes/no Error! Bookmark not defined. Error! Bookmark not defined.
- 2.2.5.3. The vehicle manufacturer has ensured that the CO₂ emissions and fuel consumption data are provided to the buyer of the vehicle at the time of purchase of a new vehicle: yes/no Error! Bookmark not defined. Error! Bookmark not defined.
- 2.2.5.4. A completed specimen of the test type VII result format used to inform the buyer of the new vehicle is added to the information document: yes/no Error! Bookmark not defined. Error! Bookmark not defined.
- 2.2.5.5. Type VII test results, where applicable and for each reference fuel tested Error! Bookmark not defined.
- 2.2.5.6. CO₂ emissions and fuel consumption Error! Bookmark not defined.

CO ₂ clinisations and fact consumption								
Test Type VII Test Results (TR _{TTVII})	Test No	CO ₂ (g/km)	Fuel consumption (1/100km) or (kg/100 km)					
	4							
TR _{TTI Measured x} (i)(ii)	2							
	3							
TRTH Measured Mean (i) (ii)								
K _i ^{(t) (iii) (v)} (no unit)								
$\frac{TR_{TTVIIx}^{(i)}(iv)}{K_i \cdot TR_{TTI Measured \times Mean}}$								
(iii) Round to 4 (iv) Round to 0 (v) Set K _i =1 i	decimal places. decimal places decimal places n case:	with a periodically reger	nerating emission abatement system or;					
	ele is <u>not</u> a hybrid e							

Table B.5.11. 6: Test Type VII result table for propulsion unit(s) equipped with a combustion engine only or equipped with not externally chargeable (NOVC) hybrid electric propulsion unit(s)

- 2.2.5.7. CO₂-emissions/fuel consumption (manufacturer's declared values) Error! Bookmark not defined.
- 2.2.5.7.1. For light motor vehicles equipped with a passenger compartment, the maximum electrical consumption owing to auxiliary heating such as heating systems for the passenger compartment/seats/other error! Bookmark not defined. Error! Bookmark not defined.

B.5.12. Annex: template form to record coast down times

Trade name:	Production number (Bo	ody):	
Date: / /	Place of the test:	Name of recorder	
Climate:	Atmospheric pressure: kPa	Atmospheric temperature:	:°C
Wind speed (parallel/perpen	dicular):/m/s		

Rider height: ___m

Test Vehicle speed km/h	coast down time(s)			Statistical accuracy in percent	Average coast down time in s	Running resistance in N	Target running resistance in N	Note	
	First								
	Second								
	First								
	Second								
	First								
	Second								
	First								
	Second						•		
	First								
	Second								
	First								
	Second								

Curve fitting: F*=__+_v²

B.5.13. Annex: template form to record chassis dynamometer settings

Trade name:	Production number (Body):	
Date: / /	Place of the test:	Name of recorder

Test Vehicle	(Coast dow	vn time(s)	Running res		Setting	Note
	Test 1	Test 2	Test 3	Average	Setting value	Target value		

Curve fitting: $F^*= + v2$

B.5.14. Annex: driving cycles for the type I test

1. World Harmonised Motorcycle Test Cycle (WMTC), description of the test cycle

The WMTC to be used on the chassis dynamometer shall be as depicted in the following graph and as specified in the following points:

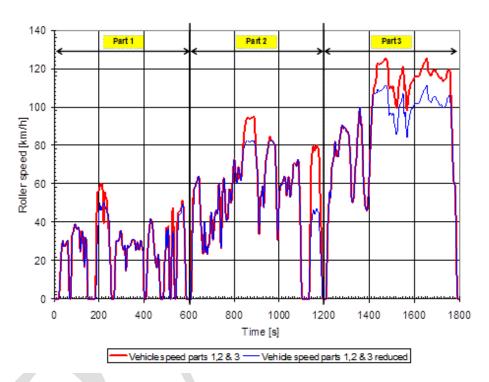


Figure B.5.14.-1: WMTC drive cycle

1.1. The WMTC lasts 1800 seconds and consists of three parts to be carried out without interruption. The characteristic driving conditions (idling, acceleration, steady vehicle speed, deceleration, etc.). are set out in the following points and tables.

1.2. WMTC, cycle part 1

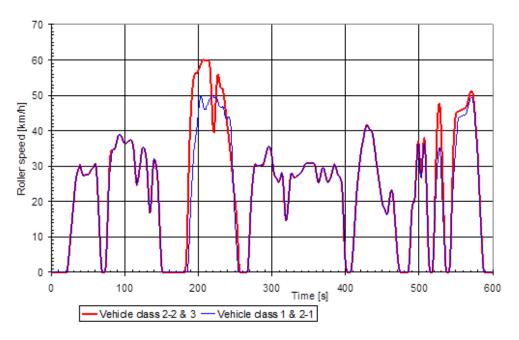


Figure B.5.14.-2: WMTC, part 1

1.2.1 The characteristic desired vehicle speed versus test time of WMTC, cycle part 1 is set out in the following tables.

1.2.2.1

	roller speed	ph	ase i	ndicate	(TS)	a -	roller speed	ph	asei	indicate)(TSi		rollerspeed	ph	ase i	ndicate	OF5
time in s	in km/h			cruise		time in s	in km/h	-		cruise	_	time in s	in km/h			cruise	$\overline{}$
0	0.0	X	200	with the second	SURE SU	81	29.6	зтор	200	oralise.	X	121	31,2	Stop	200	X	- Care
1	0.0	x	\vdash			62	26.9				x	122	33.0			x	\vdash
2	0,0	x				63	23,0				x	123	34,4			x	\vdash
3	0.0	x				84	18.6				x	124	35,2			x	\vdash
4	0.0	x	-			65	14.1				ж	125	35,4			200	ж
5	0.0	x				88	9,3				x	128	35,2				30
6	0,0	x	-			67	4,8				ж	127	34.7				ж
7	0,0	x				68	1,9				x	128	33,9				x
8	0,0	x				89	0,0	ж			othic	129	32,4				ж
9	0.0	x				70	0,0	x				130	29.8				ж
10	0.0	x				71	0,0	x				131	28,1				20
11	0.0	x				72	0,0	x				132	22,1				20
12	0.0	x				73	0,0	X.				133	18,6				.30
13	0.0	x				74	1.7		ж			134	16,8		ж		
14	0.0	X.				75	5,8		x			135	17.7		x		Г
15	0.0	x				76	11.8		ж			136	21.1		ж		Г
16	0,0	X.				88	17,3		x			137	25,4		ж		Г
17	0,0	ж.				78	22,0		ж			138	29,2		ж		
18	0,0	ж				79	26,2		ж			139	31,6		ж		
19	0,0	ж				80	29,4		ж			140	32,1				ж
20	0,0	х				81	31,1		ж			141	31,6				ж
21	0,0	x				82	32,9		x			142	30,7				ж
22	1.0		ж			83	34,7		X		,	143	29,7				ж
23	2,6		x			84	34,8		X			144	28,1				ж
24	4,8		x			85	34,8		x			145	25,0				х
25	7,2		ж			86	34,9		x			146	20,3				ж
28	9,6		26.			27	35,4		x			147	15,0				ж
27	12,0		ж			88	36,2		x			148	9,7				ж
28	14,3		ж			89	37.1		26.			149	5,0				ж
29	16,6		ж			90	38,0		X			150	1,6				ж
30	18,9		ж			91	38,7			X.		151	0,0	ж			┖
31	21,2		x			92	38,9			X		152	0,0	ж			╙
32	23,5		ж			93	38,9			X.		153	0,0	X.			╙
33	25,8		ж			94	38,8			x		154	0,0	ж			╙
34	27,1		ж			95	38,5			X.		155	0,0	ж			╙
35	28,0		x			96	38,1			x		156	0,0	x			╙
38	28,7		ж			97	37,5			X.		157	0,0	ж			╙
37	29,2		ж			98	37,0			X.		158	0,0	ж			╙
38	29,8		х			99	38,7			X.		159	0,0	x			⊢
39	30,3			X		100	36,5		_	X		160	0,0	ж			⊢
40	29,6			X		101	38,5		_	x		181	0,0	ж			⊢
41	28,7	\vdash		X.		102	38,8			x	\vdash	182	0,0	X.	\vdash		\vdash
42	27,9		\vdash	х		103	38,8			x	\vdash	183	0,0	X.	\vdash		\vdash
43	27.4			X.		104	37,0		\vdash	ж	\vdash	184	0,0	X.			\vdash
44	27,3			X.		105	37,1	1	\vdash	X.	\vdash	185	0,0	X.			\vdash
45	27,3			X		106	37.3	\vdash		X	\vdash	188	0,0	26.	\vdash		\vdash
48	27,4	\vdash		X.		107	37,4	\vdash		X.	\vdash	187	0,0	ж	\vdash		\vdash
48	27,5			X		108	37,5	\vdash		X.	\vdash	188	0,0	x	\vdash		\vdash
48	27,8			X		109	37,4			ж	7-	169	0,0	x			\vdash
49 50	27,8			x		110 111	36,9 36,0				x	170	0,0 0,0	x			\vdash
51	27,6 27,8			x		112	34,8				x	171 172	0,0	X			\vdash
52	28,1			x		113	31.9				x	173	0,0	X.			\vdash
53	28,5			x		1114	29,0	\vdash			x	174	0,0	x	\vdash		\vdash
54	28,9	\vdash		x	-	115	26,9				x	175	0,0	x			\vdash
55	29,2	\vdash		x		116	24,7			- 1	A	176	0,0	x			\vdash
56	29,4	\vdash		x		117	25,4			X.		177	0,0	x			\vdash
57	29.7	\vdash		x		118	26,4			x		178	0,0	x	\vdash		\vdash
58	30.0			x		119	27.7			x		179	0,0	x			\vdash
59	30,5			x		120	29,4			x		180	0,0	X.			\vdash
60	30,6		\vdash		ж								-0m				\vdash

Table B.5.14.-1: WMTC, cycle part 1, reduced vehicle speed for vehicle classes 1 and 2-1, 0 to $180 \ s$.

fime	ins	roller speed	ph	ase i	ndicate	0.05	time in s	roller speed	ph	ase i	indicato	(FS	time in s	roller speed	ph	ase i	ndicato	NTS
		in km∂h	stop	acc	cruise	dec		în km/h	stop	acc	cruise	dec	LINE IN 2	in km/h	stop	acc	cruise	dec
	81	0,0	x				241	43,9			x		301	30,6			x	
-	82	0,0	X.			_	242	43,8				X.	302	29,0			x	_
_	83	0,0	X.			_	243	43,0				X.	303	27,8			x	
_	84	0,0	X.			_	244	40,9				x	304	27,2		_	x	_
_	85	0,4		x		_	245	36,9				x	305	26,9			x	
_	86	1,8		x		_	248	32,1				ж	306	28,5			X	_
-	87	5,4		x		-	247	28,8	\vdash			X.	307	28,1		_	X	<u> </u>
-	88	11,1		x		_	248	21,8	\vdash			ж	308	25,7			X	_
-	89	16,7		x		_	249	17,2				x	309	25,5			X	
$\overline{}$	90	21,3		x		-	250	13,7				x	310	25,7			X.	
	91	24,8		x			251	10,3				x	311	28,4			x	
	92 93	28,4 31,8		X.		\vdash	252 253	7,0 3,5	\vdash			x	312 313	27,3 28,1		\vdash	x	\vdash
_	94	34,8		x		\vdash	254	0,0	x			200	314	27,9			26.	x
_	95	38,3		x			255	0,0	x				315	26,0				x
-	96	37,8		x			258	0,0	x				316	22,7				x
-	97	39,6		x		\vdash	257	0,0	x				317	19,0				x
-	98	41,3		x		\vdash	258	0,0	x				318	16,0				X.
-	99	43,3		x			259	0,0	x				319	14,6		ж		
I	00	45.1		x			280	0.0	x				320	15,2		ж		
$\overline{}$	01	47.5		X.			281	0,0	x				321	16,9		ж		
	02	49,0		x			282	0,0	x				322	19,3		ж		
20	03	50,0			X.		263	0,0	x				323	22,0		ж		
20	04	49,5			X.		284	0,0	x				324	24,6		ж		
20	05	48,8			X.		285	0,0	X.				325	26,8		ж		
20	06	47,6			X.		288	0,0	X.				328	27,9		ж		
20	07	48,5			X.		267	0,5		ж			327	28,0			x	
20	08	48,1			X.		268	2,9		ж			328	27,7			X.	
	09	48,1			X.		269	8,2		ж			329	27,1			x	
-	10	48,8			x	_	270	13,2		ж			330	26,8			x	
	11	46,9			X.	_	271	17,8	\Box	x			331	28,6			x	_
-	12	47,2			x	_	272	21,4		ж			332	26,8			x	_
-	13	47,8			ж	_	273	24,1		ж			333	27,0			X	_
-	14	48,4			x	_	274	28,4		x			334	27,2			X.	
-	15	48,9 49.2			X		275	28,4		x			335 338	27,4			X	
-	16 17	49,6			x	\vdash	278 277	29,9 30,5	\vdash	ж			337	27,5 27,7			X.	\vdash
-	18	49,9			x	-	278	30,5			x		338	27,9			x	
-	19	50,0			X.		279	30,3			X.		339	28,1				
	20	49,8	\vdash		x	\vdash	280	30,2	\vdash		x		340	28,3		\vdash	x	\vdash
	21	49,5			x		281	30,1	Н		x		341	28,6			x	
	22	49.2			x		282	30,1			X.		342	29,1			x	
23	23	49,3			X.		283	30,1			x.		343	29,6			x	
2	24	49,4			X.		284	30,2			X.		344	30,1			x	
23	25	49,4			X.		285	30,2			X.		345	30,6			x	
2	26	48,6			X.		286	30,2			X.		346	30,8			X.	
2	27	47,8			X.		287	30,2			ж.		347	30,8			X.	
2	28	47,0			X.		288	30,5			x.		348	30,8			x	
2	29	46,9			X.		289	31,0			ж		349	30,8			ж	
$\overline{}$	30	46,6	Ш		ж		290	31,9	\sqcup		ж		350	30,8		_	ж	
	31	48,8			х		291	32,8	\sqcup		х		351	30,8		\vdash	х	
-	32	48,8	Ш		x		292	33,7	ш		ж		352	30,8		\vdash	ж	
-	33	46,9			x		293	34,5	\sqcup		x		353	30,8		_	x	
-	34	48,4	\vdash		х	<u> </u>	294	35,1	\sqcup		x		354	30,9		\vdash	x	<u> </u>
-	35	45,6	\vdash		X	<u> </u>	295	35,5	\vdash		x		355	30,9	_	\vdash	X	<u> </u>
-	38	44,4			X.	<u> </u>	298	35,6	\vdash		X		358	30,9		\vdash	X	<u> </u>
	37	43,5	\vdash		x	\vdash	297	35,4	$\vdash\vdash$		X.		357	30,8		\vdash	X	\vdash
	38 39	43,2 43.3			X.	-	298 299	35,0 34.0	\vdash		X.		358 359	30,4 29.6		\vdash	X.	\vdash
1 6	J (2)	ಇವವ	, ,		30.		233	34.0	ı I	1	30.		J00		1		36.	

Table B.5.14.-2: WMTC, cycle part 1, reduced vehicle speed for vehicle classes 1 and 2-1, 181 to 360 s

34,0 32,4

29,6 28,4

359 380

299 300

239

43,3

1.2.2.3

	rollar speed	nh	a se i	indicate	ers.		roller speed	nh	a se i	indicate	VES.		roller speed	nh	ace i	indicate	ars.
time in s	roller speed in km/h			oruise	dec	time in s	roller speed in km/h	stop		oruise	dec	time in s	in km/h	stop		oruise	_
381	27.1	stop	ave		ueu	421	34,0	Stop	_	cruise	uec	481	0,0	_	acc	cruise	uec
362	26,0	\vdash	\vdash	X		422	35,4		x			482	0,0	X.			\vdash
363	25,4	\vdash	\vdash	X.	-	423	38,5		X		_	483	0,0	x			\vdash
384	25,5	_	\vdash			424	37,5		x			484	0,0	x			\vdash
		\vdash	\vdash	X.	_	425			-		_			_			⊢
385	28,3	_	\vdash	ж.			38,6		x			485	0,0	ж			\vdash
388	27,3	_	_	x	_	428	39,6		ж			486	1,4		x		├
367	28,3		_	X.		427	40,7		ж			487	4,5		X.		<u> </u>
388	29,2		_	X.		428	41,4		ж			488	8,8		ж		<u> </u>
389	29,5			X.		429	41,7			X.		489	13,4		X.		_
370	29,4		_	x		430	41,4		_	X		490	17,3		ж		_
371	28,9			x		431	40,9			x		491	19,2		x		
372	28,1			X.		432	40,5			x.		492	19,7		x		
373	27,1			X.		433	40,2			x.		493	19,8		x		
374	26,3			X.		434	40,1			X.		494	20,7		x		
375	25,7			X.		435	40,1			x.		495	23,7		ж		
376	25,5			x		438	39,8				x	498	27,9		x		
377	25,6			X.		437	38,9				X.	497	31,9		x		
378	25,9			x		438	37,4				X	498	35,4		x		\vdash
379	26,3	\vdash	\vdash	X.	\vdash	439	35,8	\vdash	\vdash		X	499	36,2	\vdash	- 0%		ж
		_	\vdash			440			\vdash		_						_
380	26,9		-	X.			34,1		\vdash		ж	500	34,2				ж
381	27,6	_	-	x		441	32,5		-		x	501	30,2				ж
382	28,4	 	-	X.		442	30,9				x	502	27,1		_		ж
383	29,3		_	X.	_	443	29,4				X.	503	26,6		X.		├
384	30,1		_	X.		444	27,9		_		х	504	28,6		x		_
385	30,4			X.		445	28,5				X.	505	32,6		X.		
386	30,2			X.		448	25,0				x	508	35,5		X		
387	29,5			26.		447	23,4				X.	507	38,6				20.
388	28,6			X.		448	21,8				X.	508	34,6				x
389	27,9			X.		449	20,3				ж	509	30,0				ж
390	27,5			X.		450	19,3				x	510	23,1				ж
391	27,2			x.		451	18,7				x	511	16,7				x
392	26,9			offic	x	452	18,3				x	512	10,7				x
393	26,4	\vdash	\vdash		x	453	17,8		\vdash		x	513	4.7				x
394	25,7	\vdash	\vdash			454	17,4		\vdash		x	514	1,2				x
		_	\vdash		X.				\vdash								- 24
395	24,9	_	-		X.	455	16,8		-		X.	515	0,0	X	_		├
396	21,4	_	_	_	X.	458	16,3			X		518	0,0	ж			-
397	15,9		_		x	457	16,5			X		517	0,0	x	_		—
398	9,9		_		X.	458	17,8			X		518	0,0	X.			
399	4,9				X.	459	19,2			X		519	3,0		X		
400	2,1				X.	480	20,8			x		520	8,2		x		
401	0,9				ж	481	22,2			x		521	14,3		x		
402	0,0	ж				482	23,0			x.		522	19,3		x		
403	0,0	х	L			483	23,0		L		X.	523	23,5		X.		L
404	0,0	X				484	22,0				x	524	27,3		X.		
405	0,0	X				485	20,1	1			X.	525	30,8		ж.		
408	0.0	х				488	17.7				x	528	33,7		x		
407	0,0	x				487	15,0				x	527	35,2		x		
408	1,2		х			488	12,1		\vdash		x	528	35,2				ж
409	3,2		x			489	9,1		\vdash		x	529	32,5				x
410						470	6,2		\vdash			530					
	5,9		X					_	\vdash	\vdash	x		27,9		\vdash	-	x
411	8,8		X			471	3,8	-	\vdash	\vdash	ж.	531	23,2	\vdash	\vdash		x
412	12,0		x			472	1,8	_	\vdash	\vdash	x	532	18,5	\vdash	<u> </u>		ж
413	15,4		X.		-//	473	0,8	_	<u> </u>	\vdash	X.	533	13,8	_	_		ж
414	18,9		X.			474	0,0	X.	<u> </u>	\vdash		534	9,1				ж
415	22,1		X.			475	0,0	X.				535	4,5				x
416	24,7		ж.			478	0,0	ж				538	2,3				ж
417	28,8		X.			477	0,0	X.				537	0,0	ж	L		
418	28,7		X.			478	0,0	ж.				538	0,0	X.			
419	30,6		ж			479	0,0	ж				539	0,0	ж			
420	32,4		x			480	0,0	x				540	0,0	x			
			00'00	1			-0-						-0-	- OF-10	ı	ı	1

Table B.5.14.-3: WMTC, cycle part 1, reduced vehicle speed for vehicle classes 1 and 2-1, 361 to 540 s

1.2.2.4.

time in s	roller speed	ph	ase i	ndicate	WS.
time in s	in km/h	stop	acc	cruise	dec
541	0.0	ж			
542	2.8		ж		
543	8,1		ж		
544	14,3		ж		
545	19,2		ж		
548	23,5		x		
547	27,2		ж		
548	30,5		x		
549	33,1		x		
550	35,7		х		
551	38,3		ж		
552	41,0		ж		
553	43.6			x.	
554	43,7			X.	
555	43.8			x.	
558	43.9			x	
557	44,0			X.	
558	44.1			x.	
559	44,2			x	
580	44,3			X.	
561	44,4			x.	
562	44,5			x.	
583	44,6			X.	
584	44,9			x.	
565	45,5			X.	
588	48.3			x.	
567	47.1			X.	
588	48,0			x.	
589	48.7			x.	
570	49,2			x.	
571	49,4			X.	
572	49,3			x.	
573	48,7				X.
574	47,3				ж
575	45,0				ж
576	42,3				ж
588	39,5				X.
578	36,6				X.
579	33,7				X.
580	30,1				ж
581	26.0				ж
582	21,8				ж
583	17,7				ж
584	13,5				ж
585	9,4				ж
588	5,8				X.
587	2.1				ж.
588	0,0	x			
589	0,0	ж			
590	0,0	ж			
591	0,0	X.			
592	0,0	x			
593	0,0	х			
594	0,0	ж			
595	0,0	ж			
598	0,0	x			
597	0,0	x			
598	0,0	x			
599	0,0	X.			
600	0,0	ж			

Table B.5.14.-4: WMTC, cycle part 1, reduced vehicle speed for vehicle classes 1 and 2-1, 541 to $600\ \mathrm{s}$

1.2.2.5.

	roller speed in	ph	iase i	indicato)TS		roller speed	ph	ase	indicato	DTS		roller speed	ph	asei	ndicato	ITS
time in s	km/h	stop	acc	cruise	dec	time in s	in km/h	stop	acc	cruise	dec	time in s	in km/h	stop	acc	cruise	de
0	0,0	ж	$\overline{}$			81	29,7	\vdash	$\overline{}$		ж	121	31.0			ж	Т
1	0,0	х				62	27,0				X.	122	32,8			ж	Г
2	0,0	ж.				63	23,0				X.	123	34,3			x.	Г
3	0,0	X.				84	18,7				X.	124	35,1			x	Г
4	0,0	x				85	14,2				ж	125	35,3				2
5	0,0	x				88	9,4				X.	128	35,1]
8	0,0	x				67	4,9				ж	127	34,6				1
8	0,0	x				88	2,0				ж	128	33,7				1
8	0,0	X.				89	0,0	ж				129	32,2				1
9	0,0	ж				70	0,0	X.				130	29,6				L
10	0,0	x				71	0,0	x				131	26,0				₽
11	0,0	X.				72	0,0	X.			_	132	22,0				Ŀ
12	0,0	X.	_			73	0,0	X.				133	18,5				Ŀ
13	0,0	x				74	1,7	_	X.			134	16,6		ж		╄
14	0,0	X.	_			75	5,8	├	X.			135	17,6		ж		╀
15	0,0	x	_			78	11,8	-	X.			138	21,0		ж		╄
16	0,0	X.	<u> </u>			88	18,3	-	ж.			137	25,2		ж		\vdash
17	0,0	X.				78	24,5	 	36.			138	29,1		ж		\vdash
18	0,0	X.	<u> </u>		_	79	29,4	-	X.			139	31,4		ж		+
19	0,0	ж.	\vdash			80	32,5	_	x			140	31,9				╀
20	0,0	X.	-			81	34,2		X.			141	31,4				ŀ
21	0,0	X.	-			82	34,4		X			142	30,6				ŀ
22	1,0	_	ж.			83	34,5	-	x	_		143	29,5				ŀ
23	2,8	\vdash	x			84	34,8	-	X.			144	28.0				H
24 25	4,8	 	X.			85 86	34,7	 	X			145 148	24,9				_
28	7,2 9.6		x			87	34,8 35,2		x			147	14.8				╀
27	12,0	\vdash	X			88	38,0		X			148	9,5				H
28	14,3	_	x			89	37,0		X.		Ť	149	4.8				H
29	18.8		x			90	37.9		x			150	1.4				Ħ
30	18,9		x			91	38,6		x			151	0.0	x.			H
31	21,2		x			92	38,8	 	200	x		152	0.0	x			H
32	23,5	\vdash	x			93	38,8	-	\vdash	x		153	0.0	x			H
33	25,6		x			94	38,7			x		154	0.0	x			t
34	27,1		X.			95	38.5			x		155	0.0	x			t
35	28,0		x			98	38,0			X.		158	0,0	x			H
36	28,7		X.			97	37,4			ж		157	0,0	x			T
37	29,2		26.			98	38,9			x		158	0.0	x			T
38	29,8		X.			99	38.8			x.		159	0.0	ж			Г
39	30,4		-	X.		100	38,4		_	X.		180	0,0	x			T
40	29/8			x		101	38,4			x.		181	0,0	X.			Γ
41	28,7			x		102	38,5			ж		162	0,0	x.			Г
42	27,9			x		103	36,7			х		163	0,0	ж			Γ
43	27,5			x		104	38,9			x		184	0,0	ж			Γ
44	27,3			x		105	37,0			х		105	0,0	ж			ſ
45	27,4			х		108	37,2			ж		188	0,0	X.			ſ
46	27,5			x		107	37,3			х		167	0,0	x			Ĺ
47	27,6			x		108	37,4			х		168	0,0	ж			Ĺ
48	27,6			ж		109	37,3			х		189	0,0	X.			L
49	27,6			ж		110	36,8			х		170	0,0	X.			L
50	27.7			x		111	35,8				ж	171	0,0	ж			L
51	27,8			ж		112	34,7				ж	172	0,0	X.			Ĺ
52	28,1			x		113	31,8	—	<u> </u>		ж	173	0,0	X.	$oxed{}$		L
53	28,6	<u> </u>		x		114	28,9	<u> </u>	<u> </u>		ж	174	0,0	ж	$ldsymbol{ldsymbol{ldsymbol{eta}}}$		L
54	29,0			ж		115	26,7				X.	175	0,0	X.			L
55	29,2			x		116	24,6	<u> </u>		х		178	0,0	ж			L
58	29,5			x		117	25,2	<u> </u>	<u> </u>	x		177	0,0	ж	$ldsymbol{ldsymbol{ldsymbol{eta}}}$		L
57	29,7			x		118	26,2	Ь—		x		178	0,0	ж			L
58	30,1			x		119	27,6			х		179	0,0	X.			L
59	30,5			x		120	29,2			х		180	0,0	ж			L
80	30,7	I		X.		l .	Ι	Ι -		I							Г

Table B.5.14.-5: WMTC, cycle part 1 for vehicle classes 2-2 and 3, 0 to $180\ s$

1.2.2.6.

40 0	roller speed in	ph	iase i	indicato	NTS	4* *	roller speed	ph	ase i	indicate	015	42	roller speed	ph	asei	indicato)TS
time in s	km/h	stop	acc	cruise	dec	time in s	in km/h	stop	acc	oruise	dec	time in s	in km/h	stop	acc	oruise	dec
181	0,0	x				241	38.3				ж	301	30.6			ж	\vdash
182	0.0	ж				242	38,4				х	302	28.9			x.	Г
183	2.0		ж			243	34,6				ж	303	27,8			x	\vdash
184	6.0		x			244	32.7				ж	304	27.2			x	\vdash
185	12.4		x			245	30.6				x	305	26.9			x	\vdash
186	21,4		x			248	28,1				x	308	26,5			x	\vdash
			_					\vdash			_	307					\vdash
187	30,0		ж.			247	25,5	_			ж		28,1			х	⊢
188	37,1		X.			248	23,1	_	\vdash		ж	308	25,7	_	_	X.	⊢
189	42,5		x			249	21,2	_			x	309	25,5	_	_	x	⊢
190	48,8		x			250	19,5				x	310	25,7			X.	⊢
191	49,8		X.			251	17,8				ж	311	28,4			x	_
192	52,4		X.			252	15,3				ж	312	27,3			X.	┖
193	54,4		ж.			253	11,5				x	313	28,1			x	
194	55,6		26.			254	7,2				ж	314	27,9				ж
195	56,1			x		255	2,5				ж	315	26,0				20
198	56,2			x		258	0,0	X.				316	22,7				ж
197	58,2			x.		257	0,0	x				317	19,0				20
198	58,2			x		258	0.0	x	М			318	16.0				×
199	56,7	-		x	\vdash	259	0.0	x	\Box			319	14.8	\vdash	ж		- 200
200	57,2			x		280	0.0	x				320	15,2		x		\vdash
201						281		_			\vdash	321			_		⊢
	57,7			ж			0,0	X.			_		16,9	_	ж		⊢
202	58,2			x		262	0,0	X.			_	322	19,3	_	x		⊢
203	58,7			x		263	0,0	X.			_	323	22,0		x		⊢
204	59,3			x		284	0,0	X.				324	24,8		x		_
205	59,8			X.		285	0,0	X.				325	26,8		x		
208	80,0			x		288	0,0	X.				328	27,9		x		
207	80,0			ж		267	0,5		X.			327	28,1			x	
208	59,9			X.		288	2,9		x.			328	27,7			x.	
209	59,9			x		289	8,2		ж			329	27,2			x	
210	59,9			x		270	13,2		x			330	26,8			x	Г
211	59,9			ж		271	17,8		х			331	28,8			x.	\vdash
212	59.9			х		272	21.4		x			332	26,8			x	\vdash
213	59,8			x		273	24.1		x		\vdash	333	27,0			x	\vdash
214	59,6			- A	х	274	28,4		x		\vdash	334	27,2	\vdash	\vdash		\vdash
	-				-			-	_		_			\vdash		X.	⊢
215	59,1				ж	275	28,4	_	ж		_	335	27,4	_	_	X.	⊢
216	57,1				ж	278	29,9	_	X.		_	338	27,6	_	_	X.	⊢
217	53,2				ж	277	30,5	_	x			337	27,7	_	_	X.	⊢
218	48,3				ж	278	30,5			X.		338	27,9			X.	
219	43,9				ж	279	30,3			X.		339	28,1			x	
220	40,3				X.	280	30,2			X.		340	28,3			X.	
221	39,5				ж	281	30,1			X.		341	28,6			ж	
222	41,3		ж			282	30,1			x.		342	29,0			x	L
223	45,2		X.			283	30,1			36.		343	29,6			x.	
224	50,1		ж			284	30,1			x.		344	30,1			ж	
225	53,7		X.			285	30,1			x		345	30,5			X.	
228	55,8	$\overline{}$	X.		\vdash	286	30.1	\vdash	М	x		348	30.7			x	
227	55.8	$\overline{}$	- 000		х	287	30.2	\vdash	\Box	x		347	30.8	\vdash		x	\vdash
228	54,7	\vdash	\vdash			288	30,4	\vdash	\vdash		\vdash	348	30,8	\vdash	\vdash		\vdash
		\vdash	\vdash		X			\vdash	\vdash	x	\vdash			\vdash	\vdash	X	\vdash
229	53,3	-	\vdash		x	289	31,0	\vdash	\vdash	X.	 	349	30,8	\vdash	\vdash	X.	\vdash
230	52,3	-	_	_	ж	290	31,8		\vdash	X.	<u> </u>	350	30,8	—	<u> </u>	X.	\vdash
231	52,0	-	-	_	ж	291	32,7	\vdash	\vdash	X.	\vdash	351	30,8	\vdash		x	\vdash
232	52,1	_	_		ж	292	33,6		\vdash	X.	_	352	30,8	_	_	X.	⊢
233	51,8		_		ж	293	34,4		\sqcup	X.		353	30,8			X.	\vdash
234	50,8				ж	294	35,0			X.		354	30,9			x	
235	49,2				ж	295	35,4			X.		355	30,9			ж	
236	47,5				ж.	296	35,5			36.		358	30,9		L	x.	L
237	45,7				ж	297	35,3			X.		357	30,8			x.	
238	43,9				ж	298	34,9			x		358	30,4			x	
239	42,0	\vdash	\vdash		x	299	33,9	\vdash	\Box	x	\vdash	359	29,6	\vdash	\vdash	x	\vdash
																	\vdash
240	40,2				X.	300	32,4			X.		380	28,4			X.	Ĺ

Table B.5.14.-6: WMTC, cycle part 1 for vehicle classes 2-2 and 3, 181 to $360\ s$

1.2.2. 7.

	roller speed in	пħ	ase i	indicate	rs.		roller speed	nh	35e i	indicate	NES.		rollerspeed	nh	asei	ndicate	ars.
time in s	km/h	- 0.	_	cruise	_	time in s	in km/h			oruise	_	time in s	in km/h	-	_	cruise	_
381	27.1	-1-6		ж		421	34,0		x			481	0.0	x			
382	28,0			X.		422	35,4	\vdash	X.			482	0,0	26.			\vdash
383	25,4			X.		423	38,5		ж.			483	0,0	X.			Т
384	25,5			ж		424	37,5		x.			484	0.0	ж			Г
385	28,3			ж.		425	38,6		x.			485	0.0	ж			Г
388	27,3			x		428	39,7		X.			486	1.4		x		Г
387	28,4			x		427	40,7		X.			487	4,5		x		Г
388	29,2			X.		428	41,5		26.			488	8,8		x		
389	29,5			X.		429	41.7			ж		489	13,4		x		
370	29,5			x		430	41,5			x		490	17,3		ж		
371	29,0			X.		431	41,0			ж		491	19,2		ж		$oxed{oxed}$
372	28,1			x		432	40,6			х		492	19,7		x		╙
373	27,2			X.		433	40,3			ж		493	19,8		x		╙
374	28,3			X.		434	40,2			ж	_	494	20,7		x		╙
375	25,7		_	x		435	40,1			x		495	23,6		x		╙
376	25,5		_	x		438	39,8				X	498	28,1		ж		\vdash
377	25,6		_	x		437	38,9	<u> </u>			х	497	32,8		x		\vdash
378	26,0		_	ж		438	37,5	<u> </u>			X	498	36,3		x		\vdash
379	28,4	_	_	ж	_	439	35,8	 			X.	499	37,1		<u> </u>		20
380	27,0	_	_	x	_	440	34,2	 		-	ж	500	35,1		<u> </u>		ж
381	27.7			x		441	32,5				X.	501	31,1				ж
382	28,5			x		442	30,9				X.	502	28,0		_		30
383	29,4			x	_	443	29,4			-	X.	503	27,5		x		⊢
384	30,2			X		444	28,0	-			ж.	504	29,5		x		⊢
385	30,5			ж	_	445	28,5	_			X.	505	34,0	P	X.		⊢
386	30,3			ж	_	448	25,0				ж.	508	37,0		ж		H
387	29,5	_		ж	_	447	23,5				ж	507	38,0		\vdash		x
388 389	28,7 27,9	_		x	_	448 449	21,9 20,4				x	508 509	38,1 31,5				X.
390	27,5			x		450	19,4				X.	510	24,5				x
391	27,3			x	\vdash	451	18.8	\vdash			x	511	17,5		\vdash		X
392	27,0			- 26	x	452	18.4	\vdash			x	512	10,5		\vdash		X
393	28.5				x	453	18.0	-			X	513	4,5				x
394	25,8				x	454	17,5	\vdash			26	514	1,0				X
395	25,0				x	455	18.9				x	515	0,0	ж			376
396	21,5				ж	458	18,4			_x		518	0,0	ж			\vdash
397	16.0				x	457	16.6			X	\vdash	517	0.0	ж			\vdash
398	10,0				ж	458	17.7	\vdash		x.		518	0,0	х			Т
399	5.0				ж	459	19,4			x		519	2.9		ж		Г
400	2,2				ж	460	20,9			x.		520	8,0		ж		Г
401	1.0				ж	481	22,3			x		521	16,0		ж		Г
402	0,0	X				462	23,2			ж		522	24,0		ж		
403	0,0	X.				463	23,2				ж	523	32,0		ж		
404	0,0	ж				484	22,2				X.	524	38,8		ж		
405	0,0	X.				485	20,3				X.	525	43,1		ж		
408	0,0	x				488	17,9				ж	528	46,0		ж		
407	0,0	x				487	15,2				X.	527	47,5				ж
408	1,2		X.			468	12,3				X.	528	47,5				20
409	3,2		x			469	9,3				ж.	529	44,8				ж
410	5,9		26.			470	8,4				ж.	530	40,1				20
411	8,8		26.			471	3,8				X.	531	33,8				20
412	12,0		26.			472	2,0				X.	532	27,2				20
413	15,4		26.			473	0,9				X.	533	20,0				20
414	18,9	<u> </u>	26.			474	0,0	X.		<u> </u>		534	12,8				20
415	22.1		x			475	0,0	x			<u> </u>	535	7,0		<u> </u>		ж
416	24,8		x			478	0,0	x			<u> </u>	538	2,2		<u> </u>		ж
417	26,8		x			477	0,0	X.			<u> </u>	537	0,0	ж	<u> </u>		\vdash
418	28,7		x			478	0,0	X.			<u> </u>	538	0,0	ж	<u> </u>		⊢
419	30,8		ж			479	0,0	X.			<u> </u>	539	0,0	ж	<u> </u>		\vdash
420	32,4		x			480	0,0	x				540	0,0	ж			\bot

Table B.5.14.-7: WMTC, cycle part 1 for vehicle classes 2-2 and 3, 361 to $540 \ s$

1.2.2.8.

			_	- F 4	
time in s	roller speed in km/h			ndicate	
541	0,0	_	acc	cruise	dec
542	2,7	ж	ж		
543	8,0		x		
544	16,0		x		
545	24,8		x		
546	32.0				
547	37,2		X		
548	40.4		X		
549	43,1		X		
550	44,6		x		
551	45,2		-^-	х	
552	45,3			x	
553	45.4			x	
554	45.5			x	
555	45.6			X	
556	45,7				
557	45,8			X	
558	45,9			X	
559	46.0			x	
	46,1				
560 561	46,2			X	
				X	
562	46,3			X	
563	46,4			X	
564	46,7		_	Х	
565	47,2 48,0			X	
566 567	48,9			X	
				X	
568 569	49,8 En E			X	
570	50,5 51,0			X	
571	51,1			x	
	51,0				
572 573	50,4			ж	197
574	49,0				X
575	46,7				X
576	44,0				X
577	41,1				x
578	38,3				X
579	35,4				
580	31,8				X
581	27,3				X
582	22,4				X
583	17.7				
584	13.4				X
585	~				X
	9,3				X
586	5,5				X
56/	2,0				ж
588	0,0	Х			
589 580	0,0	X	\vdash		_
590	0,0	X	\vdash		_
591	0,0	X			
592	0,0	X	\vdash		_
593	0,0	Х	\vdash		<u> </u>
594	0,0	Х	\vdash		<u> </u>
595 500	0,0	X	\vdash		_
596	0,0	Х	<u> </u>		
597	0,0	Х	\vdash		_
598	0,0	X	_		
599	0,0	Х	—		_
600	0,0	ж			

Table B.5.14.-8: WMTC, cycle part 1 for vehicle classes 2-2 and 3, 541 to $600 \ \mathrm{s}$

1.3. WMTC, part 2

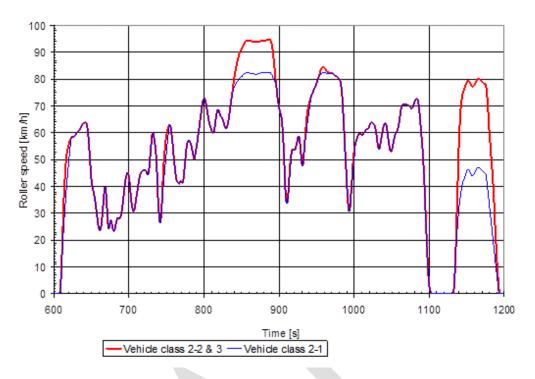


Figure B.5.14.-3: WMTC, part 2

3.1. The characteristic desired vehicle speed versus test time of WMTC, part 2 is set out in the following tables.

1.3.1.1.

	rellerensed	nh	area i	indicate	vec		collegeness	mh	aca i	ndicate	vec.		eelles en ee d	nh	nen i	indicato	vec.
time in s	roller speed in km/h	stop	_	cruise		time in s	roller speed in km/h	-	_	cruise	_	time in s	roller speed in km/h	_		cruise	
0	0,0	_	acc	cruise	uec	81	23,7	stop		cruise	uec	121	48.2	stop	acc		uec
		x	\vdash						ж						\vdash	x	\vdash
2	0,0	x	\vdash			63	23,8 25,0		X			122 123	48,1 45.7		\vdash	x	\vdash
3	0,0	ж.	\vdash		_	64			X			124	45,0		\vdash	X.	\vdash
4		ж	 		_		27,3		x					_	 	x	\vdash
	0,0	ж	_		_	85	30,4		ж			125	44,3	_		ж	\vdash
5	0,0	х	_			66	33,9		ж			128	44,7	_	X.		-
- 6	0,0	ж	_			67	37,3		X.			127	46,8		X.		<u> </u>
8	0,0	х	_		_	68	39,8				x	128	49,9	_	X.		\vdash
8	0,0	ж				69	39,5				x	129	52,8	_	x		<u> </u>
9	2,3		x		_	70	36,3				x	130	55,6		x		_
10	7,3	_	X.			71	31,4				x	131	58,2	_	X.		<u> </u>
11	13,6		x			72	28,5				x	132	80,2				х
12	18,9		X.			73	24,2				x	133	59,3				X.
13	23,6		X.			74	24,8				X.	134	57,5				X.
14	27,8		X.			75	26,6				ж.	135	55,4				X.
15	31,8		X.			76	27,5				36.	138	52,5				ж.
16	35,6		X.			77	26,8				ж	137	47,9				X.
17	39,3		X.			78	25,3				x	138	41,4				X.
18	42.7		X.			79	24,0				X.	139	34,4				ж
19	46,0		x.			80	23,3			x		140	30,0				ж
20	49.1		ж			81	23,7			x		141	27,0				ж
21	52.1		x			82	24,9			x		142	28,5		x		
22	54.9		x			83	28,4			x		143	28,7		x		
23	57,5		x			84	27.7			x		144	32,7		x		-
24	58,4		anc.	ж		85	28,3			x		145	38,5		x		-
25	58,5			x		86	28,3			x		148	40,0		x		\vdash
28	58,5			x		87	28,1			x		147	43,5		x		
27	58,6		\vdash	x		88	28,1		х			148	48.7	\vdash	x		\vdash
28	58,9		 			89			-			149	49,8		-		\vdash
			\vdash	X.	_		28,6		ж		\vdash			\vdash	x		\vdash
29	59,3		_	X		90	29,8		ж			150	52,7		ж		_
30	59,8		\vdash	x	_	91	31,6		X.			151	55,5		x		\vdash
31	80,2		_	x		92	33,9		ж			152	58,1		ж.		_
32	60,5		<u> </u>	X.	_	93	36,5		ж		\vdash	153	80,8	_	X.		\vdash
33	60,8	_	<u> </u>	X.	_	94	39,1		X.			154	62,9	_	X.		<u> </u>
34	81,1		<u> </u>	X.	_	95	41,5		ж		_	155	62,9	_	<u> </u>		ж
35	81,5		_	X.	_	96	43,3		ж			158	61,7	_	<u> </u>		ж
38	62,0			x		97	44,5		ж		_	157	59,4				X.
37	62,5		_	X.		98	45,1				Ж.	158	56,6		_		X.
38	63,0	\vdash		ж		99	45,1		$oxed{\Box}$		x	159	53,7	_			х
39	63,4		<u> </u>	ж		100	43,9		\vdash		х	160	50,7		<u> </u>		ж
40	63,7		<u> </u>	х		101	41,4		$oxed{oxed}$		x	181	47.7	<u> </u>	<u> </u>		ж
41	63,8		<u> </u>	x		102	38,4		$oxed{oxed}$		x	182	45,0		<u> </u>		ж
42	63,9			ж		103	35,5		$ldsymbol{ldsymbol{ldsymbol{eta}}}$		x	163	43,1		<u> </u>		ж
43	63,8			X.		104	32,9				x	184	41,9			X.	
44	63,2				X.	105	31,3				x	185	41,6			x	
45	81,7				x	108	30,7				x	188	41,3			x	
48	58,9				X.	107	31,0			ж		187	40,9			x	
47	55,2				X.	108	32,2			ж		168	41,8			x	
48	51,0				x	109	34,0			x		189	42,1			x	
49	46,7				X.	110	36,0			x		170	41,8			x	
50	42,8				ж	111	37,9			x		171	41,3			x.	
51	40,2				X.	112	39,9			x		172	41,5		ж		
52	38,8				X.	113	41,8			x		173	43,5		X.		
53	37,9				x	114	43,1			x	Г	174	46,5		x		
54	36,7				x	115	44,3			x	Г	175	49,7		x		
55	35,1		\vdash		x	116	45,0			x	\vdash	178	52,6	\vdash	x		$\overline{}$
58	32,9		\vdash		x	117	45,5			x	\vdash	177	55,0		x		\vdash
57	30,4	\vdash	\vdash		x	118	45,8		\vdash		\vdash	178	58,5	\vdash	x		\vdash
58	28,0		\vdash		x	119	46,0		\vdash	X	\vdash	179	57,1	\vdash	x		\vdash
			\vdash					\vdash	\vdash	x	\vdash						
59	25,9		\vdash	\vdash	X	120	46,1		\vdash	x	\vdash	180	57,3		\vdash		x
80	24,4	ı	I	ı	X.	I		I		I	ı			ı	I	1	1

Table B.5.14.-9: WMTC, cycle part 2, reduced vehicle speed for vehicle class 2-1, 0 to 180 s

1.3.1.2.

	roller speed	рħ	ase i	indicato	(FS	_	roller speed	рh	ase i	indicato	OFS		rollerspeed	вh	a se i	ndicato	DES.
time in s	in km/h	-	_	oruise	dec	time in s	in km/h	_		cruise	_	time in s	in km/h	-		oruise	_
181	57.0	2100	200	DI LILLE	x	241	77.5	2150	x	UI GISE		301	68,3	2100	200	DI GILLE	ж
182	58,3				x	242	78,1		- 200	x		302	67,3				x
183	55.2				x	243	78,6			x		303	88,1				20
184	53.9				x	244	79.0			x		304	63,9				20
185	52.6				x	245	79.4			x		305	80.2				20
186	51.4				x	248	79,7			x		308	54.9				20
187	50.1		x		376	247	80.1			x		307	48.1				2
188	51.5		x			248	80.7		\vdash	x		308	40.9				2
189	53.1		x			249	80.8			x		309	36.0				2
190	54.8		x			250	81.0			x		310	33,9				2
191	58,6		x			251	81.2			x		311	33.9		х		ď
192	58.5		x			252	81.6			x		312	36.5		x		\vdash
193	60.6		x			253	81,9		\vdash	x		313	40,1		x		\vdash
194	62.8		x			254	82.1			x		314	43.5		x		Н
195	64.9		x			255	82.1			x		315	46.8		x		\vdash
196	67,0		x			258	82,3			x		318	49,8		x		\vdash
197	69,1		x			257	82.4		\vdash	x		317	52.8		x		\vdash
198	70,9		x			258	82.4		\vdash	x		318	53,9	\vdash	x		\vdash
199	72,2		x			259	82,3		\vdash	X.		319	53,9		x		\vdash
200	72,8		- 24		x	280	82,3					320	53,7				\vdash
201	72.8					281	82,2			x		321	53.7		x		\vdash
202	71.9		\vdash		x	282	82.2			X		322	54.3		x		\vdash
203	70,5		\vdash		x	263	82,1			x		323	55,4	\vdash	x		\vdash
203	68,8		\vdash		x	284	82,1			x		324	56,8	\vdash	x		\vdash
205	67,1		\vdash		x	285	82.0	1	\vdash	. x		325	58,1		x		\vdash
206	85,4		\vdash		x	288	82.0		\vdash			328	58,9				Η,
207	63.9		_		x	287	81.9		_	x		327	58.2				2
208	62.8				x	288	81.9					328	55,8				2
209	81.8		\vdash			289				X		329	52,6	\vdash			_
210	81.0		\vdash		х	270	81,9			X.		330	49.2				2
211	80.4		\vdash		x		81,9 81.9			X		331	47.8				2
					Х	271		 		26	\vdash		48.4		x		\vdash
212 213	80,0		x	\vdash		272	82,0 82,0	_		X.		332 333	51.4		x		⊢
214	80,2 81.4		x			273	82.1	-	\vdash	X.		334	54,2		x		⊢
215			x				82.2		\vdash	X		335	56,9	\vdash	x		⊢
	63,3		ж.			275			\vdash	X.			59,4		x		⊢
216	85,5		x			278	82,3			X		338			x		⊢
217	67,4		x			277	82,4			X		337	81,8		х		\vdash
218	88,5		X			278	82,5	-		X		338	84,1		ж		⊢
219	88,7		-		х	279	82,5	-		X		339	88,2		x		⊢
220	88,1				х	280	82,5	-	\vdash	X	\vdash	340	88,2	\vdash	ж		⊢
221	67,3		\vdash		x	281	82,5	-	\vdash	X.		341	70,2		x		⊢
222	88,5		_		x	282	82,4	-	_	X.	\vdash	342	72,0		x		⊢
223	85,9				Х	283	82,4	-	-	X		343	73,7		х		⊢
224	85,5				X	284	82,4	-	-	X.	\vdash	344	74,4	\vdash	ж		⊢
225	64,9				X	285	82,5	-	-	x		345	75,1		ж		⊢
226	84,1				ж	288	82,5	-	_	ж		348	75,8		ж		⊢
227	63,0				X.	287	82,5	-	_	x		347	76,5		ж		⊢
228	62,1		_		X	288	82,4	_	_	X.		348	77.2		ж		⊢
229	81,8		x			289	82,3	-	_	X		349	77,8		ж		⊢
230	01,7		х			290	81,6	-	_	X		350	78,5		x		⊢
231	62,3		26.			291	81,3	-	_	x		351	79,2		x		⊢
232	63,5		X.		~	292	80,3	-	<u> </u>	ж		352	80,0	<u> </u>	ж		\vdash
233	65,3	_	x	\vdash		293	79,9	-	<u> </u>	X.	<u> </u>	353	81,0	\vdash		x	\vdash
234	67,3	_	X.			294	79,2	_	├	ж		354	81,2	\vdash	_	X	\vdash
235	89,2	<u> </u>	X.			295	79,2		<u> </u>	ж		355	81,8			x	\vdash
238	71,1		x			298	78,4		<u> </u>		x	358	82,2	\sqcup		Х	\vdash
237	73,0		ж			297	75,7				x	357	82,2	\sqcup		ж	\perp
238	74,8		x			298	73,2				x	358	82,4	\sqcup		ж	\perp
239	75,7		x			299	71,1				x	359	82,5			X	L
240	76,7		ж.			300	69,5				X.	380	82,5			x	

Table B.5.14.-10: WMTC, cycle part 2, reduced vehicle speed for vehicle class 2-1, 181 to $360 \ \mathrm{s}$

1.3.1.3.

		n/h	nen i	n dinata	vee			n h		ndicato	vee			nh	nen i	ndicato	
time in s	roller speed in km/h	-		ndicato cruise		time in s	roller speed in km/h			cruise		time in s	roller speed in km/h			cruise	_
381	82.5	stop	acc		oec	421	83.1	stop	acc		aec	481	72.0	stop	acc		dec
362	82.5		\vdash	x	_	422	63,6			x	\vdash	482	72,6		\vdash	X.	\vdash
363	82,3		_	x		423	63,9			x		483	72,0 72,8			X	\vdash
384	82,1		\vdash	x	_	424	63.8				\vdash	484	72,7		\vdash	x x	\vdash
385	82,1					425	63,6			X		485	72,0			A	
388				X		428	83.3			X		486					x
	82,1		-	X	_						ж		70,4		\vdash		X.
367	82,1		_	ж	_	427	62,8				X.	487	67.7		\vdash		X.
388	82,1		_	X	_	428	81,9				ж	488	84,4		\vdash		X.
389	82,1		-	Х	_	429	80,5				ж	489	61,0		<u> </u>		ж
370	82,1		-	x	_	430	58,6				ж	490	57,6		\vdash		ж
371	82,1		_	x	_	431	56,5				ж	491	54,0		_		X.
372	82,1		_	x	_	432	54,8				ж	492	49,7		_		X.
373	81,9			x		433	53,8			x		493	44,4				X.
374	81,6			X		434	54,5			x		494	38,2				X.
375	81,3			x		435	56,1			x		495	31,2				x
376	81,1			ж		438	57,9			ж		498	24,0				ж.
377	80,8			x		437	59,7			x		497	16,8				ж.
378	80,6			X.		438	81,2			ж		498	10,4				ж.
379	80,4			X.		439	62,3			x		499	5,7				X.
380	80,1			х		440	63,1			х		500	2,8				X.
381	79,7				x	441	63,6				ж	501	1,6				26.
382	78,6				x	442	63,5				ж	502	0,3				ж.
383	76,8				ж	443	62.7				ж	503	0,0	ж			
384	73,7				ж	444	60,9				ж	504	0,0	ж			
385	69,4				x	445	58,7				ж	505	0,0	x			-
386	84.0		\vdash		x	448	58,4				x	508	0.0	x	\vdash		\vdash
387	58,6				x	447	54,5				x	507	0,0	X.			\vdash
388	53,2		\vdash		x	448	53,3				x	508	0,0	X.	\vdash		\vdash
389	47,8		\vdash			449	53,0				- 20	509	0,0		\vdash		\vdash
	42.4		\vdash		x	450	53,5			X	_	510	0,0	ж.	\vdash		\vdash
390					x					x	_			X.	\vdash		\vdash
391	37,0				x	451	54,8			x		511	0,0	X.			_
392	33,0		\vdash		x	452	58,1			X	\vdash	512	0,0	X.	\vdash		\vdash
393	30,9		_		x	453	57,6			X	_	513	0,0	X.	\vdash		├
394	30,9		X.		_	454	58,9			X	_	514	0,0	X.	\vdash		├
395	33,5		X.			455	59,8	_		X	_	515	0,0	X.	_		├
398	37,2		ж		_	458	60,3			X	_	516	0,0	ж	_		├
397	40,8		x			457	60,7			x		517	0,0	x			
398	44,2		X.			458	61,3	<u> </u>		X		518	0,0	X.	<u> </u>		Ь—
399	47.4		X.			459	62,4	\vdash	\vdash	X		519	0,0	X.			
400	50,4		x			480	84,1	<u> </u>		x		520	0,0	х			Ь
401	53,3		ж			481	88,2	<u> </u>		x		521	0,0	х			<u> </u>
402	56,1		ж			482	88,1	<u> </u>	\vdash	x	<u> </u>	522	0,0	ж			
403	57,3		ж.			483	69,7	$ldsymbol{ldsymbol{ldsymbol{eta}}}$		ж		523	0,0	X.	$oxed{oxed}$		
404	58,1		X.			484	70,4			X		524	0,0	X.			
405	58,8		x			485	70,7			x		525	0,0	X.			
406	59,4		X.			488	70,7			х		528	0,0	ж			
407	59,8			x		487	70,7			x		527	0,0	ж			
408	59,7			x		488	70,7			x		528	0,0	ж			
409	59,4			X.		489	70,6			x		529	0,0	X.			
410	59,2			x		470	70,5			x		530	0,0	X.			
411	59,2			x		471	70,4			x		531	0,0	X.			
412	59.6			x		472	70,2			x		532	0,0	x			
413	80,0			x		473	70,1			x		533	2,3		ж		
414	80.5			x		474	69,8			x		534	7,2		x		\vdash
415	81,0		\vdash	x	\vdash	475	69,5	\vdash		x	\vdash	535	13,5		x		\vdash
416	81,2		\vdash		\vdash	478	69,1				\vdash	538	18,7	<u> </u>	x		\vdash
			\vdash	x	\vdash			\vdash	\vdash	x	\vdash						\vdash
417	81,3		\vdash	X	<u> </u>	477	89,1	\vdash		X	\vdash	537	22,9		x		\vdash
418	81,4		\vdash	X	-	478	89,5	\vdash		x	\vdash	538	28,7		x		\vdash
419	81,7	 	\vdash	X		479	70,3	\vdash	\vdash	X	\vdash	539	30,0	_	x		\vdash
420	62,3	ı	I	30.		480	71,2	1		30.		540	32,8	ı	20.	I	1

Table B.5.14.-11: WMTC, cycle part 2, reduced vehicle speed for vehicle class 2-1, 361 to $540 \ \mathrm{s}$

1.3.1.4.

	roller speed	ph	ase i	indicate	(15)
time in s	in km/h			cruise	
541	35.2	2000	X	Guise	uec
					_
542	37,3		Х		_
543	39,1		Х		
544	40,8		Х		
545	41,8		х		
546	42,5		х		
547	43,3		х		
548	44.1		х		
549	45.0				
			X		_
550	45,7		Х		_
551	46,2	_		Х	_
552	46,3			X	_
553	46,1			х	
554	45,6			X	
555	44.9			х	
556	44.4			ж	
557	44.0				
				X	
558	44,0			X	
559	44,3			X	
560	44,8			X	
561	45,3			X	
562	45,9			X	
563	46.5			х	
564	46.8			х	
565	47.1			×X	
566	47.1			X	_
567	47.0			X	
568	46,7			X	
569	46,3			х	
570	45,9			х	
571	45,6			X	
572	45,4			X	
573	45,2			Х	
574	45,1			X	
				_^	-
575	44,8				X
576	43,5				X
577	40,9				X
578	38,2				X
579	35,6				X
580	33,0				ж
581	38.4				X
	0				
582	27.7	P			ж
583	25,1				Х
584	22,5				Х
985	19,8				X
586	17,2				X
587	14,6				ж
588	12,0				ж
589	9,3				X
590	6,7	\vdash	\vdash		X
591	4,1	_	\vdash		ж
592	1,5		\vdash		Х
593	0,0	Х	\vdash		
594	0,0	ж			
595	0,0	ж			
596	0,0	x			
597	0,0				
		X			\vdash
598	0,0	ж	\vdash		\vdash
599	0,0	X	\vdash		_
600	0,0	x			L

Table B.5.14.-12: WMTC, cycle part 2, reduced vehicle speed for vehicle class 2-1, 541 to $600 \ s$

1.3.1.5.

time in s							TT T			P2 6				-7-		T* 4	
contract of the same	roller speed in km/h			indicate		time in s	roller speed in km/h			ndicate		time in s	roller speed in km/h			indicate	
		_	acc	cruise	oe c	04		stop		cruise	dec	4004		stop	acc	cruise	dec
0	0,0	X.	\vdash			81	23,7		ж		\vdash	121	46,2			X	\vdash
2	0,0	x.				62 63	23,8 25,0		x			122 123	48,1 45,7			X	_
3	0,0	x	\vdash			84	27,3		x			124	45.0			x	\vdash
4	0,0	x	\vdash			85	30,4		x		\vdash	125	44.3			X	\vdash
5	0,0	x	\vdash			88	33,9		x			128	44.7		ж	- ^	\vdash
6	0,0	x				67	37,3		x			127	46.8		x		\vdash
7	0,0	x	\vdash			68	39,8		x		\vdash	128	50,1		x		\vdash
8	0,0	x	\vdash			69	39,5		26.		ж	129	53,6		x		\vdash
9	2.3	20.	х			70	38,3				x	130	56.9		x		\vdash
10	7.3		x			71	31.4				x	131	59.4		x		\vdash
11	15.2		x			72	28.5				x	132	80.2				ж
12	23,9		X.			73	24,2				x	133	59,3				x
13	32.5		x			74	24,8				x	134	57,5				ж
14	39,2		x			75	28,8				x	135	55,4				x
15	44.1		X.			76	27.5				x	138	52,5				ж
18	48,1		x			77	28,8				x	137	47,9				ж
17	51,2		x			78	25,3		\vdash		x	138	41.4	\vdash			x
18	53,3		x			79	24.0				x	139	34.4				x
19	54,5		x			80	23,3			X.	SP30	140	30,0				x
20	55.7		x			81	23,7			x		141	27.0				x
21	58,9		-	x		82	24.9			x		142	26.5		x		
22	57,5			x		83	26,4			x		143	28,7		x		
23	58,0			x		84	27.7			x		144	33.8		x		-
24	58,4			x.		85	28,3			X.		145	40,3		x		
25	58,5			x		86	28,3			ж		148	46,6		x		\vdash
28	58.5			x		87	28.1			x		147	50.4		ж		\vdash
27	58,6			x.		88	28,1			X.		148	54.0		x		П
28	58,9			x		89	28,6			х		149	56,9		ж		\vdash
29	59.3			x		90	29.8			x		150	59.1		x		\vdash
30	59,8			x		91	31.6			x		151	60,6		x		
31	80,2			X.		92	33,9			ж.		152	81,7		ж		\Box
32	60,5			x		93	36,5			X.		153	62,6		ж		
33	80,8			x		94	39,1			X.		154	83,1				ж
34	81,1			x		95	41.5			X.		155	62,9				ж
35	81,5			x		96	43,3			x		158	81,7				ж
36	62,0			x		97	44,5			X.		157	59,4				ж
37	62,5			x		98	45,1				x	158	56,6				ж
38	63,0			х		99	45,1				X.	159	53,7				ж
39	63,4			x		100	43,9				x	160	50,7				ж
40	63,7			x		101	41,4				x	181	47.7				ж
41	63,8			x.		102	38,4				x	182	45,0				ж
42	63,9			x		103	35,5				x	183	43,1				ж
43	63,8			x		104	32,9				x	164	41,9			х	
44	63,2				ж	105	31,3				x	185	41,6			ж	
45	61,7				ж	108	30,7				X.	188	41,3			х	
46	58,9				ж	107	31,0			x		167	40,9			х	
47	55,2				ж	108	32,2			x		188	41,8			ж	
48	51,0				ж	109	34,0			x		169	42,1			х	
49	46,7				x	110	36,0			x		170	41,8			х	
50	42,8	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	$ldsymbol{ldsymbol{eta}}$		х	111	37,9		$oxed{oxed}$	x	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	171	41,3	$ldsymbol{ldsymbol{ldsymbol{eta}}}$		х	
51	40,2				ж.	112	39,9			x		172	41,5		ж		
52	38,8				ж	113	41,6			X.		173	43,5		ж		_
53	37,9		$ldsymbol{ldsymbol{eta}}$		x	114	43,1			х	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	174	46,5	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	ж		
54	36,7				ж	115	44,3			X.		175	49,7		ж		
55	35,1	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	\vdash		ж	116	45,0		$oxed{oxed}$	X.	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	178	52,6	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	ж		_
58	32,9				ж	117	45,5			х		177	55,0		ж		
57	30,4				ж	118	45,8			X.		178	58,5		ж		
58	28,0		$ldsymbol{ldsymbol{eta}}$		ж	119	46,0		ldot	x	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	179	57,1	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	ж		
59	25,9				ж	120	46,1			х		180	57,3				ж
80	24.4			<u> </u>	ж												

Table B.5.14.-13: WMTC, cycle part 2 for vehicle classes 2-2 and 3, 0 to $180\ s$

1.3.1.6.

				. 100 4						- n= 4						TP 4	
time in s	roller speed		_	indicato		time in s	roller speed		_	indicato	_	time in s	roller speed	-		ndicato	_
	in km/h	stop	acc	cruise	dec		in km/h	stop		cruise	dec		in km/h	stop	acc	cruise	_
181	57,0		_		x	241	81,5		x			301	68,3				X
182 183	56,3 55,2		\vdash		x	242 243	83,1 84,6		x			302 303	67,3 66,1				X.
184	53.9		\vdash	_	x	244	86.0		x			304	63.9	\vdash			x
			\vdash		X				X				80.2				_
185	52,8		 		ж	245	87.4		x			305					.X.
186	51,4				ж	248	88,7		x			306	54,9				ж
187	50,1		ж.			247	89,6		x			307	48,1				.30
188	51,5		X.			248	90,2		x			308	40,9				.30
189	53,1		X.			249	90,7		x			309	38,0				.30
190	54,8		x			250	91,2		x			310	33,9				.30
191	58,6		x			251	91,8		x			311	33,9		x		\vdash
192 193	58,5 60,6		X.			252 253	92,4 93,0		x			312 313	38,5 41.0		X		\vdash
194			x			254			ж			314	45,3		ж		⊢
195	62,8 64,9		x			255	93,6 94,1		х	-		315	49,2		X		\vdash
198	67,0		x			256	94,3			X		316	51.5		x		⊢
			-							X					-		⊢
197	89,1	\vdash	x		-	257	94,4 94.4	\vdash	\vdash	X		317	53,2 53.9	\vdash	X		\vdash
198 199	70,9 72,2	\vdash	x			258 259	94,4	\vdash	\vdash	X		318 319	53,9		x		\vdash
200	72.8		X.			280	94.3			X		320	53.7		x		\vdash
			\vdash		x					X					ж		\vdash
201	72,8		\vdash		ж	281	94,2			X		321 322	53,7		ж		\vdash
202 203	71,9		\vdash		X	262 263	94,2 94.2			X		323	54,3		x		\vdash
203	70,5		\vdash	_	ж	284				X		324	55,4 56,8	\vdash	ж		⊢
	68,8		 		x		94,1	-		x				\vdash	x		\vdash
205 208	67,1 65.4		 		x	285 288	94,0 94.0			X		325	58,1 58.9		ж		
			 		ж					X		328					.00
207	63,9		 		x	287	93,9			X		327	58,2				
208	62,8		_		ж	288	93,9			X		328	55,8				.30
209	81,8		 		ж	289	93,9			ж		329	52,6				.30
210	81,0		\vdash		x	270	93,9			Х		330	49,2				.30
211	80,4		\vdash		x	271	93,9			X		331	47,6	\vdash	ж		⊢
212	80,0		 		ж	272	94,0			X		332	48,4	\vdash	x		\vdash
213	80,2		_	X		273	94,0			X.		333	51,8		ж		\vdash
214	81,4	_	 	x		274	94,1		_	X		334	55,7		ж		⊢
215	63,3		 	X.		275	94,2			x		335	59,6		ж		⊢
216	85,5	_	 	X.		278	94,3			X		338	63,0	_	ж		⊢
217	67,4	_	_	X.		277	94,4			X		337	65,9		ж		⊢
218	88,5			х		278	94,5			X		338	68,1	_	ж		⊢
219	88,7		-		ж	279	94,5			x		339	69,8	_	ж		⊢
220	88,1	_			X	280	94,5			x		340	71,1		ж		⊢
221	87,3		 		X	281	94,5			X		341	72,1	_	ж		⊢
222	88,5		 		ж	282	94.4			X.		342	72,9		ж		⊢
223	85,9				X	283	94,5			x		343	73,7	_	ж		⊢
224	85,5				X	284	94,8	\vdash	\vdash	X	\vdash	344	74,4	\vdash	ж		\vdash
225	84,9				X	285	94,7	-	\vdash	x	\vdash	345	75,1	\vdash	ж		\vdash
228	84,1	_			ж	286	94,8	-	\vdash	x		346	75,8	<u> </u>	ж		\vdash
227	63,0		<u> </u>		ж	287	94,9	-	\vdash	X.		347	76,5	\vdash	ж		\vdash
228	82,1		_		X	288	94,8	_	\vdash	ж		348	77,2	<u> </u>	ж		\vdash
229	81,8		X.			289	94,3	-	_		ж	349	77,8	\vdash	ж		\vdash
230	61,7		X.			290	93,3	-	\vdash		x	350	78,5	\vdash	ж		\vdash
231	62,3		x	_		291	91,8	-	\vdash		x	351	79,2	<u> </u>	X		\vdash
232	83,5		X.	_	~	292	89,6	-	\vdash		ж	352	80,0	—	ж		\vdash
233	85,3	_	X.			293	87.0	-	\vdash		ж	353	81,0	<u> </u>	ж		\vdash
234	67,3	_	X.			294	84,1		\vdash		ж	354	82,0	<u> </u>	ж		\vdash
235	69,3		X.			295	81,2	_	<u> </u>		ж	355	83,0	<u> </u>	ж		⊢
238	71,4		X.			298	78,4		<u> </u>		ж	358	83,7		ж		Щ.
237	73,5		ж.			297	75,7		\vdash		ж	357	84,2	<u> </u>	\vdash	X	╙
238	75,8		X.			298	73,2		\vdash		ж	358	84,4	\vdash	\vdash	X	<u> </u>
239	77.7		ж			299	71,1		<u> </u>		х	359	84,5	<u> </u>	<u> </u>	x	<u> </u>
240	79,7		X.			300	89,5				X.	380	84,4			X.	1

Table B.5.14.-14: WMTC, cycle part 2 for vehicle classes 2-2 and 3, 181 to $360\ s$

1.3.1.7.

		_10		- 12 - 4						- PP - 4						- P2 - 40	
time in s	roller speed	_	_	indicato		time in s	roller speed	-		ndicato		time in s	roller speed			ndicato	_
	in km/h	stop	acc	oruise	de c		in km/h	stop	300	cruise	dec		in km/h	stop	acc	cruise	dec
381	84,1		\vdash	ж		421	83,1			X	_	481	72,0	_	\vdash	X.	
382	83,7		\vdash	X		422	83,8			X	 	482	72,6	_	\vdash	x	
383	83,2		_	x		423	63,9		_	х	-	483	72,8	_	_	x	₩
384	82,8		_	X.		424	63,8			X	-	484	72.7	_		x	₩
385	82,6			X.		425	63,6			Х	_	485	72,0				ж
388	82,5			X.		428	63,3				x	488	70,4				X.
367	82,4		$ldsymbol{ldsymbol{ldsymbol{eta}}}$	X.		427	62,8				X.	487	67.7				X.
388	82,3			X.		428	61,9				x	488	84,4				X.
389	82,2			X.		429	89,5				ж	489	81,0				X.
370	82,2			X.		430	58,6				х	490	57,6				ж
371	82,2			X.		431	56,5				ж	491	54,0				26.
372	82,1			26.		432	54,8				ж.	492	49,7				ж.
373	81,9			X.		433	53,8			x		493	44,4				26.
374	81.6			X.		434	54,5			x		494	38,2				ж
375	81,3			X.		435	56,1			X.		495	31,2				X.
378	81,1			x		438	57,9			x		498	24,0				ж.
377	80,8			x		437	59,7			x		497	16,8				x
378	80,6		\vdash	x	\vdash	438	81,2	\vdash		x	\vdash	498	10,4	\vdash	\vdash		x
379	80,4		\vdash	_	<u> </u>	439	62,3		\vdash		\vdash	499		 	\vdash		_
			\vdash	X.	 			\vdash		x	\vdash		5,7	\vdash	\vdash		x
380	80,1		\vdash	X.		440	83,1	\vdash		x	-	500	2,8	\vdash	\vdash		x
381	79,7	_	\vdash		ж	441	63,6	\vdash			ж	501	1,6	 	\vdash		ж
382	78,6		_		X.	442	63,5				ж	502	0,3	<u> </u>	_		ж
383	76,8		_		X.	443	62,7				ж	503	0,0	x	_		—
384	73,7				X.	444	60,9				x	504	0,0	x			_
385	89,4				X.	445	58,7				X.	505	0,0	x			
386	84,0				X.	448	58,4				ж	508	0,0	ж			
387	58,6				26.	447	54,5				x	507	0,0	ж			
388	53,2				26.	448	53,3				X.	508	0,0	X.			
389	47,8				ж.	449	53,0			X.		509	0,0	x			
390	42,4				26.	450	53,5			x		510	0,0	ж			
391	37,0				x.	451	54,6			x		511	0.0	ж			
392	33.0				ж	452	56,1			x		512	0.0	ж			
393	30,9				X.	453	57,6			X.		513	0,0	ж			
394	30.9		x			454	58.9			x		514	0,0	x			\vdash
395	33.5		x			455	59,8			x		515	0.0	x			\vdash
398	38.0		x			458	60.3			x		518	0.0	x			\vdash
397	42,5		x			457	80,7			x	-	517	0,0	x			\vdash
398						458					_		0.0	_			\vdash
	47,0 54.0		x		\vdash		81,3	\vdash		x	\vdash	518		ж.	\vdash		\vdash
399	51,0		ж		-	459	82,4	\vdash		x	\vdash	519	0,0	ж.	\vdash		\vdash
400	53,5		x		<u> </u>	480	84,1	\vdash		x	\vdash	520	0,0	x	\vdash		\vdash
401	55,1		x		<u> </u>	481	88,2	\vdash	-	X	\vdash	521	0,0	x	\vdash		\vdash
402	58,4	—	ж		<u> </u>	482	88,1	\vdash	<u> </u>	x	\vdash	522	0,0	x	\vdash		\vdash
403	57,3		ж		_	483	69,7	<u> </u>		ж		523	0,0	X.	\vdash		—
404	58,1	_	ж		<u> </u>	484	70,4	\vdash		X	<u> </u>	524	0,0	ж	\vdash		—
405	58,8		ж			485	70,7			x		525	0,0	x	\vdash		_
406	59,4		х			488	70,7	$ldsymbol{ldsymbol{eta}}$	$ldsymbol{ldsymbol{ldsymbol{eta}}}$	x		528	0,0	x	$ldsymbol{ldsymbol{eta}}$		
407	59,8			ж		487	70,7			ж		527	0,0	ж			
408	59,7			X.		488	70,7			х		528	0,0	х			
409	59,4			X.		489	70,6			ж		529	0,0	ж			
410	59,2			X.		470	70,5			x		530	0,0	х			
411	59,2			ж.		471	70,4			ж		531	0,0	х			
412	59,6			X.		472	70,2			x		532	0,0	ж			
413	80,0			X.		473	70,1			X.		533	2,3		ж		
414	80.5			x		474	69,8			x		534	7,2		x		
415	81,0		\vdash	x		475	69,5			x	\vdash	535	14,6		x		\Box
416	81,2			x		478	69,1			x		538	23,5		x		\vdash
417	81,3		\vdash	X.		477	69,1			x	\vdash	537	33,0	\vdash	x		-
418	81,4		\vdash			478	69,5				\vdash	538	42,7	\vdash	x		\vdash
			\vdash	X.	\vdash			\vdash		X	\vdash			\vdash			\vdash
419 420	81,7		\vdash	X.	\vdash	479 480	70,3	\vdash	\vdash	x	\vdash	539	51,8 50.4	\vdash	x		\vdash
720	62,3			36.	ı	1000	71,2			30.	1	540	59,4	ı	30.		1

Table B.5.14.-15: WMTC, cycle part 2 for vehicle classes 2-2 and 3, 361 to 540 \ensuremath{s}

1.3.1.8.

	roller speed	ph	ase i	indicato	175
time in s	in km/h	stop			dec
541	65.3		х		
542	69,6		х		
543	72,3		ж		
544	73,9		х		
545	75,0		х		
546	75,7		X		
547	76,5	\vdash	X		
548	77,3		X		
549	78,2		X		
550	78,9	\vdash	x		_
			^	- 9	
551	79,4			X	
552	79,6			X	_
553	79,3	\vdash	_	Х	_
554	78,8			Х	_
555	78,1			X	
556	77,5	_		ж	
557	77.2	<u> </u>	<u> </u>	Х	
558	77,2	<u> </u>	_	Х	
559	77,5			X	
560	77,9			X	
561	78,5			X	
562	79,1			X	
563	79,6		/	X	
564	80,0			X	
565	80,2			X	
566	80,3			X	
567	88.1			x	
568	79.8			Х	
569	79,5			X	
570	79.1				
571	78,8	\vdash		X	
				X	
572	78,6			X	
573	78,4			X	
574	78,3			Х	
575	78,0			_	X
576	76,7				X
577	73,7				Х
578	69,5				Х
579	64,8				X
580	69,3				х
581	56,2				х
582	52,5				X
583	49,0				X
584	45.2				х
585	40.8				х
586	35,4				Х
587	29.4				X
588	23,4				X
589	17,7				X
	12,6				
590 591			_		X
591 592	8,0				X
	4,1		-		X
593	1,3	-			Х
594	0,0	Х	<u> </u>		_
595	0,0	ж	<u> </u>		_
596	0,0	х	<u> </u>		_
597	0,0	х			
598	0,0	х			
599	0,0	х			
	0,0	ж			

Table B.5.14.-16: WMTC, cycle part 2 for vehicle classes 2-2 and 3, 541 to 600 s

1.4. WMTC, part 3

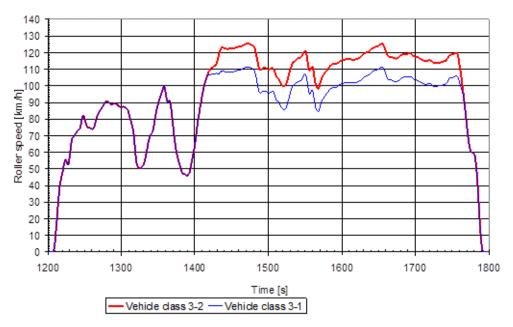


Figure B.5.14.-4: WMTC, part 3.

1.4.1 The characteristic desired vehicle speed versus test time of WMTC, part 3 is set out in the following tables.

1.4.1.1.

	rollerspeed	ph	a se i	ndicato	15		rollerspeed	ph	a se i	ndicato	15		rollerspeed	ph	ase i	indicato	DES
time in s	in km/h			oruise		time in s	in km/h	-		oruise	dec	time in s	in km/h	_	_	oruise	_
0	0.0	X				81	73.9				ж	121	53.0				ж
1	0.0	x				62	74.1		ж			122	51.8				26.
2	0,0	X.				63	75,1		X.			123	50,9				ж.
3	0,0	ж				64	76,8		x.			124	50,5				X.
4	0,0	ж				65	78,7		X.			125	50,2				X.
5	0,0	ж				88	80,4		х			128	50,3		x		П
6	0,0	ж				67	81,7		ж			127	50,6		x.		П
8	0,0	ж				68	82,6		ж			128	51,2		X.		П
8	0,9		ж			69	83,5		ж			129	51,8		X.		
9	3,2		X.			70	84,4		x			130	52,5		X.		
10	7,3		ж			71	85,1		x			131	53,4		X.		
11	12.4		ж			72	85,7		ж			132	54,9		X.		
12	17,9		ж			73	86,3		X.			133	57,0		x.		
13	23,5		X.			74	87,0		X.			134	59,4		X.		
14	29,1		ж			75	87,9		X.			135	61,9		X.		
15	34,3		ж			76	88,8		ж			138	64,3		X.		
16	38,6		X.			88	89,7		X.			137	66,4		X.		Г
17	41,8		ж			78	90,3			X,		138	68,1		ж.		
18	43,9		x			79	90,6			X		139	69,6		X.		\Box
19	45,9		X.			80	90,6			X.		140	70,7		26.		
20	48,1		26.			81	90,5			x		141	71,4		ж.		
21	50.3		X.			82	90.4			×		142	71,8		x		
22	52,6		X.			83	90,1			х		143	72,8		X.		Г
23	54.8		X.			84	89,7			x		144	75,0		x.		\Box
24	55,8		x.			85	89,3			x		145	77.8		x.		\Box
25	55,2		ж			86	89,0			x		148	80,7		x		\Box
28	53,9		X.			87	88,8			36		147	83,3		X.		\vdash
27	52,7		ж.			88	88,9			36		148	85,4		X.		\vdash
28	52,8		26.			89	89,1			x		149	87.3		X.		\vdash
29	55,0		26.			90	89,3			x		150	89,1		x		\vdash
30	58,5		x			91	89,4			x		151	90,6		x		\vdash
31	62,3		x			92	89,4			x		152	91,9		x		-
32	05,7		x			93	89,2			x		153	93,2		x		-
33	88,1		ж			94	88,9			x		154	94,6		x		\vdash
34	89,1		x			95	88.5			x		155	96,0		ж.		\vdash
35	69,5		26.			96	88.0			x		158	97,5		x		\vdash
38	69,9		x			97	87,5			X		157	99,0		x		\vdash
37	70,6		x			98	87.2			x		158	99,8				X.
38	71,3		x			99	87.1			x		159	99,0		\vdash		x
39	72,2		ж			100	87.2			x		180	98,7		\vdash		x
40	72.8		ж.			101	87.3			x		181	93,7		\vdash		x
41	73.2		ж.			102	87.4			x		182	91.3				x
42	73,4		x			103	87,5			x		183	90,4				x
43	73,8		ж			104	87.4			x		184	90,6				x
44	74,8		X			105	87.1			x		185	91,1				x
45	76.7		X			108	86.8			x		188	90.9				x
48	79,1		X		\vdash	107	86,4	\vdash		x		167	89,0		\vdash		x
47	81,1		x			108	85,9			x		188	85,6				ж.
48	82,1				26	109	85,2				ж	189	81,6				ж.
49	81.7			1	x	110	84.0				x	170	77,6		\vdash		X
50	80,3				x	111	82,2				x	171	73,6				x
51	78,8	1			X	112	80,3				x	172	89,7				x
52	77,3				x	113	78,6				x	173	66,0				x
53	75,9				x	114	77,2	\vdash			x	174	62,7		\vdash		x
54	75,0				x	115	75,9				x	175	80,0		\vdash		x
55	74.7				x	116	73,8				x	176	58,0				x
56	74.7				x	117	70,4				x	177	58,4		\vdash		x
57	74.7				x	118	85.7	\vdash	\vdash		x	178	54,8		\vdash		x
	74.6				x	119	80,5	\vdash	\vdash		x	179	53,3		\vdash		x
馬原	12 TABLE	ı			A.	11112	- ಇತ್ತಿಪ				A.	110	ಆವೈವ				_
58 59	74.4				ж	120	55,9				x	180	51,7			l	36.

Table B.5.14.-17: WMTC, cycle part 3, reduced vehicle speed for vehicle class 3-1, 1 to $180\ \mathrm{s}$

1.4.1.2.

	rollerspeed	ph	ase i	indicato	rs.		rollerspeed	рħ	ase i	indicato	ors		rollerspeed	ph	a se i	ndicato	NTS.
time in s	in km/h	-	_	oruise	dec	time in s	in km/h	stop	_	oruise		time in s	in km/h	_		oruise	_
181	50.2				x	241	108.4			x		301	95.8			x	
182	48,7				x	242	108,3			x		302	95,9			x	
183	47,2			x.	ORTEO	243	108,2			X.		303	98,2			x	$\overline{}$
184	47,1			X.		244	108,2			x.		304	98,4			x	
185	47.0			x		245	108,2			x		305	98,7			x	\vdash
186	48,9			x		248	108,2			x		308	96,7			x	$\overline{}$
187	48,6			x		247	108,3			x	\vdash	307	96,3			x	\vdash
188	48,3			x		248	108,4			x		308	95,3			200	x
189	48,1			x		249	108,5			x		309	94,0				X.
190	48,1		x	276		250	108,5			x		310	92.5				X.
191	48.5		x			251	108.5			x		311	91.4				x
192	47.1		x			252	108,5			x		312	90,9				x
193	48,1		x			253	108,5			x		313	90,7				x
194	49,8		x			254	108,7			x		314	90,3				x
195	52.2		x			255	108,8			x		315	89.6				x
198	54,8		x			258	109,0			x		316	88,6				x
197	57,3		x			257	109,2	\vdash	\vdash	X.	\vdash	317	87,7				X.
198	59,5		x			258	109,2	\vdash	\vdash	x	\vdash	318	86,8				X
199	81,7		x			259	109,4	\vdash	\vdash	x		319	86,2				X
$\overline{}$			-														_
200 201	84,4 87.7		x			280 281	109,5 109,5	\vdash	\vdash	x	\vdash	320 321	85,8 85,7				x
			x							x							x
202 203	71,4 74.0		x			282 283	109,6			X.		322 323	85,7				ж
203	74,9		x				109,8	_		X.			86,0		_	ж.	\vdash
	78,2		x			284	110,0			X.		324	86,7			X	\vdash
205	81,1	\vdash	ж			285	110,2	\vdash	_	X.	\vdash	325	87,8		_	x	\vdash
208	83,9		x			288	110,5	-		X.	-	328	89,2			X.	\vdash
207	86,6		x			287	110,7			X	_	327	90,9			x	\vdash
208	89,1	_	x			288	111,0	_		ж	_	328	92,6			X	\vdash
209	91,6		ж			289	111,1	_		X.	_	329	94,3			X	\vdash
210	94,0		ж			270	111,2			X		330	95,9			x	\vdash
211	96,3		ж			271	111,3	_		X.	-	331	97.4			x	\vdash
212	98,4		X.			272	111,3	_		X.	_	332	98,7			X	\vdash
213	100,4		x			273	111,3			X		333	99,7			x	\vdash
214	102,1	_	ж			274	111,2	_		х	-	334	100,3			x	\vdash
215	103,6		x			275	111,0	_		X.	_	335	100,6			x	\vdash
216	104,9		x			276	110,8	_		X.	_	336	101,0			x	\vdash
217	108,2			X		277	110,6			X.		337	101,4			X	\vdash
218	108,5			x		278	110,4			X.		338	101,8			x	\vdash
219	108,5		_	X.		279	110,3			X.		339	102,2			x	\vdash
220	108,8			X.		280	109,9	_		X.	_	340	102,5			x	\vdash
221	108,8	_	_	X.		281	109,3	_			ж	341	102,8		_	x	\vdash
222	107,0	_		X.		282	108,1	_			X.	342	102,7			X	\vdash
223	107,3			X.		283	108,3				ж	343	102,8			x	\vdash
224	107,3	<u> </u>	<u> </u>	X.		284	104,0	-			X.	344	103,0			x	\vdash
225	107,2	_	<u> </u>	X.		285	101,5	<u> </u>	_		X.	345	103,5	\vdash		X.	\vdash
228	107,2	<u> </u>	<u> </u>	X.		286	99,2	<u> </u>	_		ж	346	104,3	<u> </u>		x	\vdash
227	107,2	<u> </u>	<u> </u>	X.		287	97,2	<u> </u>	<u> </u>		ж	347	105,2	—		X.	\vdash
228	107,3		<u> </u>	X.		288	96,1	<u> </u>	<u> </u>		ж	348	106,1	\vdash		X.	\vdash
229	107,5	<u> </u>	<u> </u>	x		289	95,7	<u> </u>	<u> </u>	x	<u> </u>	349	106,8			x	\vdash
230	107,3	<u> </u>	<u> </u>	х		290	95,8	<u> </u>	<u> </u>	X.	<u> </u>	350	107,1	\vdash			х
231	107,3	<u> </u>	<u> </u>	x		291	98,1	<u> </u>	<u> </u>	X.	├	351	108,7	\vdash			ж
232	107,3		<u> </u>	X.		292	96,4	<u> </u>		X.	<u> </u>	352	105,0	<u> </u>			ж
233	107,3		<u> </u>	X.		293	96,7			X.		353	102,3				х
234	108,0			X.		294	96,9	<u> </u>		X.		354	99,1	\vdash			ж
235	108,2			X.		295	96,9	<u> </u>		X.		355	96,3				ж
236	108,9			X.		298	96,8			X.		356	95,0				ж
237	109,0			X.		297	96,7			X.		357	95,4				ж
238	108,9			X.		298	96,4			х		358	96,4				ж
239	108,8			x		299	98,1			х		359	97,3				ж
240	108,6			X.		300	95,9	I		X.		380	97,5				20.

Table B.5.14.-18: WMTC, cycle part 3, reduced vehicle speed for vehicle class 3-1, 181 to 360 s

1.4.1.3.

	roller speed	ph	ase	ndicato	rs -		roller speed	ph	asel	ndloato)rs	4	roller speed	ph	asel	n dioafo	rs
time in s	In km/h	stop	800	oruise	deo	time in s	In km/h	stop	800	oruise	deo	time in s	In km/h	stop	800	oruise	dec
361	96.1				X	421	102.2			X		481	104.5		\Box	X	Г
362	93.4		$\overline{}$		X	422	102.4			X		482	104.8	-	\vdash	X	т
363	90.4	-	-		X	423	102.6			X	\vdash	483	104.9	-	-	X	\vdash
364	87.8	-	-		X	424	102.8			X		484	105.1	-	-	X	\vdash
365	86.0	-	\vdash		X	425	103.1			X		485	105.1	-	\vdash	X	┰
366	85.1	-	\vdash		X	426	103.4	\vdash	_	X	\vdash	486	105.2	-	\vdash	X	⊢
367	84.7		\vdash		X	427	103,9		_	X	\vdash	487	105,2	-	\vdash	X	⊢
368	84.2	-	\vdash	X	٨	428	104.4	\vdash	_	X	\vdash	488	105,2	-	\vdash	X	⊢
369	85.0	-	\vdash		_	429	104,4	\vdash	_		\vdash	489	105,2	-	⊢	_	⊢
		_		X				\vdash	_	X	\vdash			├	⊢	X	⊢
370 371	86,5 88.3	-	\vdash	X		430 431	105,2 105,5	\vdash	_	X	\vdash	490 491	105,3 105.4	-	\vdash	X	⊢
		_	<u> </u>	X					_	X	\vdash			├	├	X	⊢
372	89,9	_	<u> </u>	X		432	105,7	_		X	\vdash	492	105,5	├	Ь	X	╙
373	91,0	_	<u> </u>	X	_	433	105,9	_	_	X	\vdash	493	105,5	├	┝	X	⊢
374	91,8	_	_	X		434	106,1	\vdash		X	\vdash	494	105,3	┞	<u> </u>	X	╙
375	92,5			X		435	106,3			X		495	105,1	_		X	┖
376	93,1	lacksquare		X		436	106,5			X		496	104,7	_		X	╙
377	93,7			X		437	106,8			X		497	104,2			X	
378	94,4			X		438	107,1			X		498	103,9			X	
379	95,0			X		439	107,5			X		499	103,6	Г	Г	X	Г
380	95,6			X		440	108.0			X		500	103,5		${}^{-}$	X	Г
381	96.3	$\overline{}$	$\overline{}$	X		441	108.3			X		501	103.5		${}^{-}$	X	г
382	96.9	-	-	X		442	108.6			X		502	103.4	-	-	X	Н
383	97.5	-	\vdash	X		443	108.9			X		503	103.3	-	\vdash	X	\vdash
384	98.0	-	\vdash	X		444	109.1			X	\vdash	504	103.0	-	\vdash	X	\vdash
385	98.3	-	\vdash	X		445	109.2	\vdash	_	X	\vdash	505	102.7	-	\vdash	X	⊢
386	98.6	-	\vdash	X		4 46	109,4	-	_	X	\vdash	506	102,7	-	\vdash	X	⊢
		-	\vdash		-			\vdash	_		\vdash			-	\vdash		⊢
387	98,9	_		X	_	447	109,5	\vdash	_	X	\vdash	507	102,1	├	⊢	X	⊢
388	99,1	_	<u> </u>	X		448	109,7	_	_	X	\vdash	508	101,9	├	├	X	⊢
389	99,3	_	<u> </u>	X		4 49	109,9		_	X	\vdash	509	101,7	├	<u> </u>	X	╙
390	99,3	_	<u> </u>	X		450	110,2			X	\vdash	510	101,5	├	<u> </u>	X	╙
391	99,2			X		451	110,5			X		511	101,3	_		X	┖
392	99,2			X		452	110,8			X		512	101,2			X	L
393	99,3			X		453	111,0			X		513	101,0			X	┖
394	99,5			X		454	111,2			X		514	100,9			X	
395	99,9			X		455	111,3			X		515	100,9			X	Г
396	100,3			X		456	111,1			X		516	101,0			X	Г
397	100.6			X		457	110.4			X		517	101.2		П	X	Г
398	100.9		-	X		458	109.3			X		518	101.3	-	${}$	X	Н
399	101.1		\vdash	X		459	108,1		-	X		519	101.4	-	-	X	\vdash
400	101.3		\vdash	X		460	106.8		-	X	\vdash	520	101.4	-	\vdash	X	⊢
401	101.4	-	\vdash	X		461	105.5		_	X	\vdash	521	101.2	-	\vdash	X	\vdash
402	101,4		\vdash	X	\vdash	462	104.4		\vdash	X	\vdash	522	101,2	\vdash	\vdash	X	\vdash
403	101,5		\vdash	X	\vdash	463	103,8		\vdash	X	\vdash	523	100,6	-	\vdash	_	\vdash
		\vdash	\vdash		\vdash				\vdash		\vdash			\vdash	\vdash	X	\vdash
404	101,8	\vdash	\vdash	X	\vdash	464	103,6	\vdash	\vdash	X	\vdash	524	99,9	-	\vdash	X	\vdash
405	101,9	\vdash		X	\vdash	465	103,5	\vdash	<u> </u>	X	\vdash	525	99,6			X	⊢
406	102,0	_	<u> </u>	X		466	103,5			X	\vdash	526	99,5	—	—	X	⊢
407	102,0	_	<u> </u>	X	\vdash	467	103,4	\vdash	_	X	\vdash	527	99,5	₩	—	X	⊢
408	102,0		<u> </u>	X		468	103,3	lacksquare		X	$ldsymbol{ldsymbol{\sqcup}}$	528	99,6		<u> </u>	X	_
409	102,0			X		469	103,1			X		529	99,7			X	
410	101,9			X		470	102,9			X		530	99,8			X	
411	101,9			X		471	102,6			X		531	99,9			X	
412	101,9			X		472	102,5			X		532	100,0			X	Г
413	101,8			X		473	102,4			X		533	100,0			X	Г
414	101,8			X		474	102,4			X		534	100.1		\Box	X	Г
415	101,8		\vdash	X		475	102,5		\vdash	X	\Box	535	100.2	-	\vdash	X	т
416	101,8		\vdash	X		476	102,7		\vdash	X	\vdash	536	100,4	-	\vdash	X	\vdash
417	101,8		\vdash			477	103,0		\vdash		\vdash	537	100,4	-	\vdash	_	\vdash
417		\vdash	\vdash	X	\vdash	477	103,0	\vdash	_	X	\vdash	538	100,5	\vdash	\vdash	X	\vdash
	101,8	_		X				\vdash	—	X	\vdash			-		X	⊢
419	101,9	_	<u> </u>	X		479	103,7	\vdash	<u> </u>	X	\vdash	539	100,7	—	—	X	╙
420	102,0	l		X		480	104,1			X		540	100,8			X	ı

Table B.5.14.-19: WMTC, cycle part 3, reduced vehicle speed for vehicle class 3-1, 361 to $540 \ \mathrm{s}$

1.4.1.4.

		I -			
time in s	roller speed	_		ndicate	
	in km/h	stop	acc	cruise	dec
541	101,0	_	_	Х	_
542	101,3			x	
543	102,0			X	
544	102,7			X	
545	103,5			X	
546	184,2			X	
547	104,6			X	
548	104,7 104.8			X	
549	104,8			Х	
550			\vdash	X	_
551 552	104,9 105.1			X	
553	185,4		\vdash	x	
554	185,7		\vdash	X	
555	185,9			x	
556	106.0			X	
557	105,7			_^	х
558	105,7				X
559	103,4				X
560	103,3	\vdash			X
561	188,5				X
562	99,2				X
563	98,0				х
564	96.4				х
565	94,8				ж
566	92,8				ж
567	88,9				ж
568	84,9				ж
569	80,6				ж
570	76,3				ж
571	72,3				ж
572	68,7				ж
573	65,5				х
574	63,0				х
575	61,2				х
576	60,5				ж
577	60,0				ж
578	59,7				х
579	59,4				х
580	59,4				ж
581	58,0	_	_		х
582	55,0	_	_		х
583	51,0	<u> </u>			х
584	46,0				х
585	38,8	\vdash			X
586	31,6	_	\vdash		Х
587	24,4				ж
588	17,2	\vdash	\vdash		х
589	10,0				X
590	5,0	\vdash			X
591 582	2,0	19			Х
593	0,0	X			\vdash
594	0,0	X			
595	0.0				
596	0,0	X			
597	0,0	x			
598	0,0	X			
599	0,0	x			
600	0,0	x			
		270			

Table B.5.14.-20: WMTC, cycle part 3, reduced vehicle speed for vehicle class 3-1, 541 to $600 \ \mathrm{s}$

1.4.1.5.

	roller speed	ph	ase i	ndicate	05		rollerspeed	ph	ase i	ndicate	(FS		rollerspeed	рh	a se i	indicate)T5
time in s	in km/h	stop		cruise	_	time in s	in km/h	stop		oruise	dec	time in s	in km/h	stop		_	dec
0	0,0	х				61	73,9				ж	121	53,0				х
1	0,0	x				62	74.1		ж			122	51.6				ж
2	0,0	X.				63	75,1		ж			123	50,9				X.
3	0,0	X.				64	76,8		ж.			124	50,5				X.
4	0,0	x				85	78,7		x.			125	50,2				x
5	0,0	х				88	80.4		х			126	50.3		ж		
- 6	0,0	ж				67	81,7		x.			127	50,6		ж		
8	0,0	X.				68	82,6		X.			128	51.2		X.		
8	0,9		x			69	83,5		X.			129	51,8		X.		
9	3.2		x			70	84.4		x			130	52.5		ж		
10	7.3		x			71	85,1		ж			131	53.4		ж		
11	12.4		x			72	85.7		X.			132	54.9		26.		
12	17,9		x			73	86,3		x			133	57.0		x		$\overline{}$
13	23,5		ж			74	87.0		ж			134	59.4		ж		Т
14	29,1		x			75	87,9		x			135	61,9		x		\vdash
15	34.3		x			76	88.8		x			138	64,3		x		\vdash
16	38,6		x			77	89.7		x			137	88,4		x		\vdash
17	41,8		X			78	90,3			x		138	88,1		X		\vdash
18	43.9		x			79	90.6			X		139	69.6		x		\vdash
19	45.9		x			80	90,6	\vdash		x		140	70,7		x		\vdash
20	48.1		x			81	90,5					141	71.4		x		\vdash
21	50,3		x			82	90,4			x	\vdash	142	71,8		x		\vdash
22	52,8		x		_	83	90,1			x	\vdash	143	72,8		x		\vdash
23	54,8		x			84	89,7					144	75.0		x		\vdash
24	55,8		x			85	89.3			X		145	77.8		x		\vdash
25					_	86				X	\vdash		80.7				\vdash
	55,2		x				89,0			x		148			ж		\vdash
28	53,9		x			87	88,8			X		147	83,3		ж		\vdash
27	52,7		x			88	88,9			x	_	148	85,4		ж		\vdash
28	52,8		ж			89	89,1			x	\vdash	149	87,3		ж		\vdash
29	55,0		x		-1	90	89,3			X		150	89,1		x		\vdash
30	58,5		X.			91	89,4			X		151	90,6		ж		\vdash
31	62,3		x			92	89,4			X		152	91,9		ж		\vdash
32	65,7		ж			93	89,2	_		X		153	93,2		ж		├
33	88,1		ж			94	88,9			х		154	94,6		ж		\vdash
34	69,1		ж			95	88,5			X		155	96,0		ж		<u> </u>
35	69,5		ж			98	88,0			- M.		158	97,5		ж		_
36	69,9		X			97	87,5			X		157	99,0		ж		_
37	70,8		X			98	87,2			ж		158	99,8				X.
38	71,3		Х			99	87,1			X.		159	99,0				ж
39	72,2		x			100	87,2	_		x		160	96,7		_		X.
40	728		ж			101	87.3	_		x		181	93,7				X
41	73,2		ж			102	87.4	<u> </u>		ж	\vdash	182	91,3		_		х
42	73,4		ж			103	87,5	<u> </u>		X.		163	90,4		_		Х
43	73,8		X			104	87.4			х		184	90,6		_		ж
44	74,8		X			105	87.1			x	\sqcup	185	91,1				ж
45	78,7		х			108	86,8	\vdash		x	ш	188	90,9		\vdash		х
48	79,1		ж			107	86,4	$ldsymbol{ldsymbol{eta}}$		x	$oxed{oxed}$	167	89,0				х
47	81,1		ж			108	85,9	$ldsymbol{ldsymbol{ldsymbol{eta}}}$		x	igsquare	168	85,6				ж
48	82,1				x	109	85,2	lacksquare			ж	169	81,6				ж
49	81,7				x	110	84,0				ж	170	77,6				ж
50	80,3			1	x	111	82,2				ж	171	73,6				ж
51	78,8				ж	112	80,3				ж	172	69,7				ж
52	77,3				ж	113	78,6				ж	173	66,0				ж
53	75,9				ж	114	77.2				ж	174	62,7				х
54	75,0				x	115	75,9				X.	175	80,0				30
55	74.7				ж	116	73,8				ж	178	58,0				ж
56	74.7				х	117	70,4				x	177	56,4				ж
57	74.7				x	118	05,7				ж	178	54,8				30
58	74,6				x	119	80,5				X.	179	53,3				x
59	74.4				x	120	55,9				x	180	51,7		\vdash		x
80	74,1				x						a/6:		−wrdgn0r				- 200

Table B.5.14.-21: WMTC, cycle part 3 for vehicle class 3-2, 0 to $180\ s$

1.4.1.6.

	roller speed	nh	aca i	indicato	(FE		roller speed	nh	alea i	indicato	NE STE		roller speed	mh	aca i	indicato	NE S
time in s	in km/h	_		cruise	dec	time in s	in km/h	-		cruise	dec	time in s	in km/h	-		cruise	_
181	50.2	atop	auc	GIUISE	X	241	122.4	зтор	auc	X	uec	301	109.8	2100	alut	X	uec
182	48.7				X	242	122.3			x		302	109,9			x	\vdash
183	47.2			x	- //-	243	122.2			x		303	110.2	_		x	\vdash
184	47,1			x		244	122.2			x		304	110.4			x	\vdash
185	47.0			x		245	122,2			x		305	110.7			x	\vdash
186	46,9			x		248	122.2			x		308	110,7	_		x	\vdash
187	46.6			x		247	122.3			x		307	110.3			x	\vdash
188	46,3			x		248	122,4			x		308	109,3				ж
189	46.1			x		249	122.5			x		309	108.0				x
190	46,1		ж	orto.		250	122.5			x		310	108,5				x
191	48.5		x			251	122.5			x		311	105.4				x
192	47.1		ж			252	122.5			x		312	104,9				X.
193	48,1		x			253	122.5			x		313	104.7				x
194	49,8		ж			254	122.7			x		314	104,3				x.
195	52.2		ж			255	122.8			X.		315	103,6				ж
198	54.8		ж			258	123,0			x.		316	102,6				x
197	57,3		x			257	123,2			X.		317	101,7				X.
198	59,5		x			258	123,3			ж.		318	100,8				ж.
199	81.7		x			259	123,4			x		319	100,2				X.
200	84,4		x			280	123,5			x		320	99,8				X.
201	67.7		x			281	123,5			x		321	99,7				X.
202	71,4		x			282	123,6			x		322	99,7				X.
203	74,9		ж			283	123,8			X.		323	100,0			x	
204	78,2		ж			284	124,0			x.		324	100,7			x	
205	81,1		ж			285	124,2			x		325	101,8			x	
208	83,9		ж			288	124,5			x.		326	103,2			x	
207	86,6		ж			287	124,7			X.		327	104,9			x	
208	89,1		ж			288	125,0			x		328	108,6			x	
209	91,6		ж			289	125,1			X.		329	108,3			x	
210	94,0		ж			270	125,2			x		330	109,9			x	
211	96,3		ж			271	125,3			x		331	111,4			x	
212	98,4		ж			272	125,3			x.		332	112,7			x	
213	100,4		ж			273	125,3			x		333	113,7			x	
214	102,1		ж			274	125,2			X.		334	114,3			x	
215	103,6		ж			275	125,0			x		335	114,6			x	
218	104,9		ж			276	124,8			x		338	115,0			х	
217	108,2		ж			277	124,6			X.		337	115,4			x	
218	107,5		ж			278	124,4			ж		338	115,8			ж	
219	108,5		ж			279	124,3			X.		339	116,2	<u> </u>		х	
220	109,3		ж			280	123,9		_	x		340	116,5		_	x	₩
221	109,9		ж			281	123,3	_	_		x	341	118,8	<u> </u>		X	—
222	110,5	_	ж			282	122,1	_	<u> </u>		X.	342	116,7	<u> </u>	_	X	
223	110,9		ж			283	120,3		<u> </u>		X.	343	116,8	<u> </u>	<u> </u>	X	
224	111,2		ж			284	118,0		_		X.	344	117,0	_	_	ж	
225	111,4		ж			285	115,5		_		X.	345	117,5		-	X	₩
226	111,7		ж			286	113,2		_		X.	346	118,3	<u> </u>		X	₩
227	111,9		ж			287	111,2		_		X.	347	119,2	_	_	ж	₩
228	112,3		x			288	110,1		_		X.	348	120,1		-	X	₩
229	113,0	_	ж			289	109,7	\vdash	\vdash	ж	\vdash	349	120,8	\vdash	\vdash	X	\vdash
230	114.1		ж			290	109,8		\vdash	x	\vdash	350	121,1	\vdash	\vdash		X.
231	115,7		x			291	110,1		\vdash	ж.	\vdash	351	120,7	\vdash	\vdash		ж.
232	117,5		X			292	110,4		\vdash	X	\vdash	352	119,0	\vdash	\vdash		x
233	119,3		x			293	110,7		_	X	\vdash	353	116,3	\vdash	_		x
234	121,0		ж			294	110,9 110.9		\vdash	X	\vdash	354 355	113,1	\vdash	\vdash		X
235	122,2		\vdash	X		295			\vdash	X	\vdash	355 258	110,3	\vdash	\vdash		X
238	122,9		\vdash	x		298	110,8		_	X	\vdash	356	109,0	\vdash			X.
237	123,0		\vdash	X		297	110,7		_	X	\vdash	357	109,4	-	\vdash		X
238	122,9		\vdash	X.		298	110,4		_	X	\vdash	358	110,4	-	_		X
239	122,8		\vdash	X		299	110,1		\vdash	X	\vdash	359	111,3	\vdash	\vdash		X
240	122,8	ı	ı	ж.		300	109,9		l	26.	I	380	111,5	l			3K.

Table B.5.14.-22: WMTC, cycle part 3 for vehicle class 3-2, 181 to $360\ s$

1.4.1.7

	roller speed	ph	asel	ndicato	rs		roller speed	ph	asel	nd loaf o	rs.		roller speed	ph	asel	n dioafo	rs
time in s	In km/h	-	_	oruise		time in s	In km/h	_	_	oruise	-	time in s	In km/h	_	_	oruise	_
361	110.1				X	421	116.2			X		481	118.5			X	
362	107.4	-	\vdash		X	422	116.4			X		482	118.8	-	-	X	\vdash
363	104.4	-	\vdash		X	423	116.6		-	X	\vdash	483	118.9	-	\vdash	X	\vdash
364	101.8	-	\vdash		X	424	116.8			X	Н	484	119.1		-	X	\vdash
365	100.0	\vdash	\vdash		X	425	117.1			x	\vdash	485	119.1	-	\vdash	X	\vdash
366	99.1	-	\vdash	\vdash	X	426	117.4		\vdash	X	Н	486	119.2	-	\vdash	X	\vdash
367	98.7		-		X	427	117.9			X	Н	487	119.2		-	X	\vdash
368	98.2	-	\vdash	X	^	428	118.4		-	X	\vdash	488	119.2	-	-	X	\vdash
369	99.0	-	\vdash	X	\vdash	429	118.9		-	X	Н	489	119,3	-	\vdash	X	\vdash
370	100.5	-	\vdash	X	\vdash	430	119.2			X	Н	490	119.3		\vdash	X	⊢
371	102.3	-	\vdash	X	\vdash	431	119,5			X		491	119,4	-	-	X	\vdash
372	103.9	-	\vdash	X	\vdash	432	119.7			X	\vdash	492	119.5	-	\vdash	X	\vdash
373	105.0	-	\vdash	X	\vdash	433	119,9		-	X	Н	493	119,5	-	\vdash	X	\vdash
374	105.8	\vdash	\vdash	X	\vdash	434	120,1			X		494	119.3	-	\vdash	X	\vdash
375	106.5	-	\vdash	X	\vdash	435	120.3		-	X	Н	495	119.1	-	-	X	\vdash
376	107.1	-	\vdash	X	\vdash	436	120.5		\vdash	X	Н	496	118.7	-	\vdash	X	\vdash
377	107.7	-	\vdash	X	\vdash	437	120.8			X	Н	497	118.2	-	\vdash	X	\vdash
378	108.4		\vdash	X	\vdash	438	121.1		\vdash	X	Н	498	117.9	-	\vdash	X	\vdash
379	109.0	-	\vdash	X	\vdash	439	121.5			X	Н	499	117.6		\vdash	X	⊢
380	109.6	-	\vdash	X	\vdash	440	122.0		-	X	\vdash	500	117.5	-	\vdash	X	⊢
381	110.3	-	\vdash	X	\vdash	441	122,3		\vdash	X	Н	501	117.5	-	\vdash	X	\vdash
382	110.9	-	\vdash	X	\vdash	442	122,6			X	Н	502	117,4	-	\vdash	X	\vdash
383	111.5	-	\vdash	X	\vdash	443	122.9			X	Н	503	117.3	_	\vdash	X	⊢
384	112.0	-	\vdash	X	\vdash	444	123.1		\vdash	X	Н	504	117.0	-	\vdash	X	\vdash
385	112.3	\vdash	\vdash	X	\vdash	445	123,1			X	Н	505	116,7	-	\vdash	X	⊢
386	112,6	\vdash	\vdash	X	\vdash	4 46	123.4		\vdash	X	\vdash	506	116.4	-	\vdash	X	⊢
387	112.9	-	\vdash	X	\vdash	447	123.5		-	X	Н	507	116.1	-	\vdash	X	\vdash
388	113,1	-	\vdash	X	\vdash	448	123,7			X	Н	508	115.9		\vdash	X	⊢
389	113.3	\vdash	\vdash	X	\vdash	449	123.9		\vdash	X	\vdash	509	115.7	-	\vdash	X	⊢
390	113.3	-	\vdash	X	\vdash	450	124.2	-	_	X	Н	510	115.5	_	\vdash	X	⊢
391	113,2	\vdash	\vdash	X	\vdash	451	124.5			X	\vdash	511	115,3	-	\vdash	X	\vdash
392	113,2	\vdash	\vdash	X	\vdash	452	124.8	\vdash	\vdash	X	Н	512	115.2	-	\vdash	X	⊢
393	113,3	\vdash	\vdash	X	\vdash	453	125.0	\vdash	_	X	\vdash	513	115.0	-	\vdash	X	⊢
394	113,5	\vdash	\vdash	X	\vdash	454	125,0		-	X	\vdash	514	114.9	-	\vdash	X	\vdash
395	113,5	-	\vdash	X	\vdash	455	125,2	-	_	X	Н	515	114,9	_	\vdash	X	⊢
396	114,3	-	\vdash	X	\vdash	456	125,1		_	X	Н	516	115,0	-	\vdash	X	⊢
397	114,5	\vdash	\vdash	X	\vdash	457	124.4	\vdash	\vdash		Н	517	115,0	-	\vdash		⊢
398	114,0	\vdash	\vdash	X	\vdash	458	123.3	\vdash	\vdash	X	Н	518	115,2	-	\vdash	X	⊢
399	115.1	\vdash	\vdash	X	\vdash	459	122,1		_	X	\vdash	519	115,4	-	\vdash		\vdash
400	115,3	-	⊢		\vdash	460	120.8	\vdash	<u> </u>	-	Н		115,4	-	\vdash	X	⊢
		-	\vdash	X	\vdash			-	_	X	Н	520		-	\vdash	X	⊢
401 402	115,4 115,5	\vdash	\vdash	X	\vdash	461 462	119,5 118,4	\vdash	_	X	\vdash	521 522	115,2 114.8	\vdash	\vdash	X	\vdash
402	_	\vdash	\vdash	_	\vdash		117,8	\vdash	_	_	$\vdash\vdash$		114,0	\vdash	\vdash		\vdash
	115,6	\vdash	\vdash	X	\vdash	463		\vdash		X	$\vdash\vdash$	523	113.9	\vdash	\vdash	X	\vdash
404	115,8 115,9	\vdash	\vdash	X	\vdash	464 465	117,6 117,5	\vdash	\vdash	X	$\vdash\vdash$	524 525	113,9	\vdash	\vdash	X	\vdash
		\vdash	\vdash	X	\vdash			\vdash		X	$\vdash\vdash$			\vdash	\vdash	X	\vdash
406	116,0	\vdash	\vdash	X	\vdash	466	117,5	\vdash	<u> </u>	X	$\vdash\vdash$	526	113,5	\vdash	\vdash	X	\vdash
407	116,0	\vdash	\vdash	X	\vdash	467	117,4	\vdash	_	X	$\vdash\vdash$	527	113,5	\vdash	\vdash	X	\vdash
408	116,0	\vdash	\vdash	X	\vdash	468	117,3	\vdash		X	$\vdash\vdash$	528	113,6	\vdash	\vdash	X	⊢
409	116,0	\vdash		X	\vdash	469	117,1	\vdash	_	X	$\vdash\vdash$	529	113,7	\vdash	\vdash	X	\vdash
410	115,9	\vdash	\vdash	X	\vdash	470	116,9	\vdash	\vdash	X	$\vdash\vdash$	530	113,8	\vdash	\vdash	X	\vdash
411	115,9	\vdash		X		471	116,6			X	\vdash	531	113,9	<u> </u>	\vdash	X	⊢
412	115,9	\vdash		X	\vdash	472	116,5	\vdash	<u> </u>	X	$\vdash\vdash$	532	114,0		\vdash	X	\vdash
413	115,8	\vdash	\vdash	X	\vdash	473	116,4	\vdash	\vdash	X	$\vdash\vdash$	533	114,0	\vdash	\vdash	X	\vdash
414	115,8	\vdash	—	X	\vdash	474	116,4	\vdash	<u> </u>	X	\vdash	534	114,1		\vdash	X	\vdash
415	115,8	\vdash		X	\vdash	475	116,5	\vdash	<u> </u>	X	$\vdash\vdash$	535	114,2		\vdash	X	\vdash
416	115,8	\vdash	\vdash	X	\vdash	476	116,7	\vdash	<u> </u>	X	$\vdash\vdash$	536	114,4	\vdash	\vdash	X	\vdash
417	115,8	\vdash		X		477	117,0			X	\vdash	537	114,5	<u> </u>	\vdash	X	₩
418	115,8	—	—	X	\vdash	478	117,3	\vdash	_	X	$\vdash \vdash$	538	114,6	—	_	X	—
419	115,9	<u> </u>	<u> </u>	X	\vdash	479	117,7	\vdash	_	X	ш	539	114,7	<u> </u>	_	X	₩
420	116,0	ı	I	X	ı	480	118,1	1	1	X	ıl	540	114,8	I	ı	X	1

Table B.5.14.-23: WMTC, cycle part 3 for vehicle class 3-2, 361 to 540 s

1.4.1.8

time in s	roller speed	_		ndicato	
Line in a	in km/h	stop	acc	oruise	dec
541	115,0			X.	
542	115,3			26.	
543	116,0			X.	
544	116,7			x.	
545	117,5			ж.	
548	118,2			ж.	
547	118,6			X.	
548	118,7			36.	
549	118,8			26.	
550	118,8			26.	
551	118,9			26.	
552	119,1			36.	
553	119,4			26.	
554	119,7			X.	
555	119,9			X.	
558	120,0			X.	
557	119,7				ж
558	118,4				26.
559	115,9				X.
580	113,2				ж
581	110,5				x
582	107,2				x
563	104,0				ж
584	100,4				ж
585	96,8				ж
588	92,8				ж
587	88,9				x
588	84,9				X.
589	80,6				ж
570	76,3				ж
571	72,3				х
572	68,7				ж
573	65,5				ж
574	63,0				ж
575	61,2				ж
578	60,5				ж
577	60,0				ж
578	59,7				x
579	59,4				ж
580	59.4				ж
581	58.0				ж
582	55.0				ж
583	51.0				x
584	48,0				x
585	38,8				ж
586	31,6				X.
587	24.4				x
588	17,2				x
589	10,0				x
590	5,0				ж
591	2,0	\vdash			X.
592	0,0	x			ami
593	0,0	x			
594	0,0	x			
595	0,0	x	\vdash		
596			\vdash		\vdash
	0,0	x	\vdash		
597	0,0	X	\vdash		_
598	0,0	X	\vdash		_
599	0,0	x	\vdash		_

Table B.5.14.-24: WMTC, cycle part 3 for vehicle class 3-2, 541 to 600 s

- 2. World Harmonised Motorcycle Test Cycle (WMTC) for two-wheeled vehicles with an engine displacement < 50 cm³ and with a maximum design vehicle speed of 25 km/h, 45 km/h respectively.
- 2.1. The WMTC to be used on the chassis dynamometer is depicted in the following graph for vehicles equipped with an engine displacement < 50 cm³ or with a maximum net power or maximum continuous rated power ≤ 4 kW and with a maximum design vehicle speed (25 km/h, 45 km/h, respectively), which consists of one cold phase 1 of the WMTC and one warm phase 1 of the WMTC.

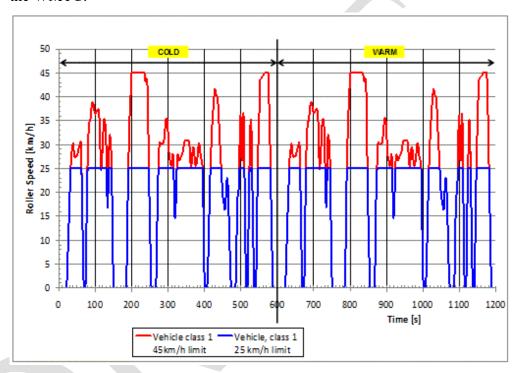


Figure B.5.14.-5: WMTC for vehicles with a maximum design vehicle speed of 45km/h and low engine displacement or maximum net or continuous rated power. The truncated desired vehicle speed trace limited to 25 km/h is applicable for vehicles with a limited maximum design vehicle speed of 25 km/h. In case of vehicle with maximum design speed of 50km/h, the vehicle shall be driven on WMTC upto maximum speed of 50km/h.

2.2 The cold and warm vehicle speed phases are identical.

2.3. Description of the WMTC for vehicles with a maximum design vehicle speed (25 km/h, 45 km/h, respectively) and a low engine displacement (< 50 cm³) or maximum net or continuous rated power (≤ 4 kW)

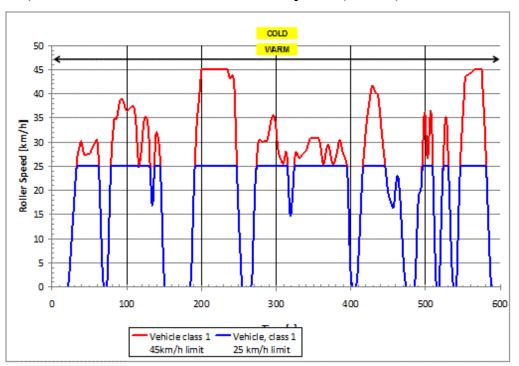


Figure B.5.14.-6: WMTC for vehicles with a maximum design vehicle speed of 45km/h and low engine displacement or maximum net or continuous rated power. The truncated desired vehicle speed trace limited to 25 km/h is applicable for vehicles with a limited maximum design vehicle speed of 25 km/h. In case of vehicle with maximum design speed of 50km/h, the vehicle shall be driven on WMTC upto maximum speed of 50km/h.

- 2.3.1. The desired vehicle speed trace WMTC shown in Figure Ap 6-10 is applicable for vehicles with a maximum design vehicle speed (if applicable at 25 km/h, at 45 km/h or 50 km/h) and a low engine displacement (< 50 cm³) or a low maximum net or continuous rated power (≤ 4 kW) and consists of the desired vehicle speed trace WMTC stage 1, part 1 for class 1 vehicles, driven once cold followed by the same desired vehicle speed trace driven with a warm propulsion unit. The WMTC for vehicles with a low maximum design vehicle speed and low engine displacement or maximum net or continuous rated power lasts 1200 seconds and consists of two equivalent parts to be carried out without interruption.
- 2.3.2. The characteristic driving conditions (idling, acceleration, steady vehicle speed, deceleration, etc.) of the WMTC for vehicles with a maximum design vehicle speed (if applicable at 25 km/h, at 45 km/h, or at 50 km/h) and low engine displacement (< 50 cm³) or maximum net or continuous rated power (≤ 4 kW) are set out in the following points and tables.

2.3.2.1.

	roller		phase ir	ndicators		I	roller		phase in	dicators		I	roller		phase in	ndicators	
time in s	speed in	stop	acc	cruise	dec	time in s	speed in	stop	acc	cruise	dec	time in s	speed in	stop	acc	cruise	dec
	km/h	•	ucc	Cluise	ucc		km/h	зюр	ucc	Cruisc	ucc	404	km/h	зюр	ucc		ucc
1	0	X				61 62	25 25					121 122	25 25			X	
2	0	X				63	23				Х	123	25			X	
3	0	X				64	18,6				X	124	25			X	
4	0	X				65	14,1				Х	125	25				
5	0	X				66	9,3				Х	126	25				
6	0	X				67	4,8				Х	127	25				
7	0	X				68	1,9				Х	128	25				
- 8 9	0	X				69 70	0	X				129 130	25 25				
10	0	X				71	0	X X				131	25				
11	0	X				72	0	X				132	22,1				Х
12	0	X				73	0	X				133	18,6				Х
13	0	Х				74	1,7		Х			134	16,8		х		
14	0	X				75	5,8		X			135	17,7		Х		
15	0	X				76	11,8		X			136	21,1		Х		
16	0	X				77	17,3		X			137	25				
17	0	X				78	22		X			138	25				
18 19	0	X				79 80	25 25					139 140	25 25				
20	0	X				81	25					141	25				
21	0	X				82	25					142	25				
22	1		Х			83	25					143	25				
23	2,6		X			84	25					144	25				
24	4,8		X			85	25					145	25				
25	7,2		X			86	25					146	20,3				Х
26	9,6		Х			87	25					147	15				Х
27	12		X			88	25					148	9,7				X
28 29	14,3 16,6		X			89 90	25 25					149 150	5 1,6				X
30	18,9		X			91	25			Х		151	0	Х			_^
31	21,2		X			92	25			X		152	0	X			
32	23,5		х			93	25			Х		153	0	Х			
33	25					94	25			X		154	0	X			
34	25					95	25			X		155	0	X			
35	25					96	25			X		156	0	Х			
36 37	25 25					97 98	25 25			X		157 158	0	X			
38	25					99	25			X		159	0	X			
39	25			Х		100	25			X		160	0	X			
40	25			Х		101	25			X		161	0	X			
41	25			Х		102	25			Х		162	0	Х			
42	25			X		103	25			X		163	0	X			
43	25			X		104	25			X		164	0	X			
44	25			X		105	25			X		165	0	X			
45 46	25 25		-	X X		106 107	25 25			X X		166 167	0	X X			
47	25			X		108	25			X		168	0	X			
48	25			X		109	25			X		169	0	X			
49	25			X		110	25					170	0	Х			
50	25			Х		111	25					171	0	Х			
51	25			X		112	25					172	0	X			
52	25			X		113	25					173	0	X			
53	25 25			X		114	25					174 175	0	X			
54 55	25		-	X X		115 116	25 24,7			Х		175	0	X X	-		
56	25			X		117	25			X		177	0	X			
57	25			X		118	25			X		178	0	X			
58	25			X		119	25			X		179	0	X			
59	25			Х		120	25			Х		180	0	Х			
60	25				X						1				1		

Table B.5.14.-25: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (25 km/h) and a low engine displacement ($< 50 \text{ cm}^3$) or maximum net or continuous rated power ($\le 4 \text{ kW}$), cold or warm, 0 to 180 s

2.3.2.2.

	roller		phase ir	ndicators			roller		phase ir	dicators		l	roller		phase ir	dicators	
time in s	speed in km/h	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec
181	0	Х				241	25			Х		301	25			Х	
182	0	Х				242	25					302	25			Х	
183	0	X				243	25					303	25			X	
184	0	X				244	25					304	25			X	
185	0,4		Х			245	25					305	25			X	
186	1,8		X			246	25					306	25			X	
187	5,4		Х			247	25					307	25			X	
188	11,1		Х			248	21,8				X	308	25			X	
189	16,7		X			249	17,2				X	309	25			X	
190	21,3		X			250	13,7				X	310	25			X	
191	24,8		X			251	10,3				X	311	25			Х	
192	25					252	7				X	312	25			X	
193	25					253	3,5				X	313	25			X	
194	25					254	0	Х				314	25				
195	25					255	0	X				315	25				
196	25					256	0	Х				316	22,7		<u> </u>		Х
197	25			-		257	0	Х				317	19		-		Х
198	25				<u> </u>	258	0	X				318	16				Х
199	25		-	-	 	259	0	X				319	14,6		X		
200	25 25					260 261	0	X				320 321	15,2 16,9		X		
202	25			-		262	0	X				322	19,3		X		
202	25			v		263	0	X				323	22		X X		
204	25			X		264	0	X X				324	24,6		X		
205	25			X		265	0	X				325	25		^		
206	25			X		266	0	X				326	25				
207	25			X		267	0,5	^	X			327	25			Х	
208	25			X		268	2,9		X			328	25			X	
209	25			X		269	8,2		X			329	25			X	
210	25			X		270	13,2		X			330	25			X	
211	25			X		271	17,8		X			331	25			X	
212	25			X		272	21,4		X			332	25			X	
213	25			Х		273	24,1		X			333	25			Х	
214	25			Х		274	25					334	25			Х	
215	25			Х		275	25					335	25			Х	
216	25			Х		276	25					336	25			Х	
217	25			Х		277	25			Х		337	25			Х	
218	25			Х		278	25			Х		338	25			X	
219	25			Х		279	25			Х		339	25			Х	
220	25			X		280	25			Х		340	25			X	
221	25			Х		281	25			Х		341	25			X	
222	25			Х		282	25			Х		342	25			Х	
223	25			X		283	25			Х		343	25			Х	
224	25			Х		284	25			Х		344	25			X	
225	25			Х	<u> </u>	285	25			Х		345	25			Х	
226	25			Х		286	25			Х		346	25			Х	
227	25			X	<u> </u>	287	25			Х		347	25		-	X	
228	25			X		288	25			X		348	25			X	
229	25			Х	<u> </u>	289	25			X		349	25			X	
230	25 25		-	X	<u> </u>	290 291	25			X		350 351	25 25			X	
231	-		-	X	 	291	25 25			X		351			-	X	
232	25 25		-	X	 	292	25			X		353	25 25		 	X	
234	25		-	X	 	293	25			X		353	25		-	X X	
235	25		-	X X	 	295	25			X X		355	25		-	X	
236	25		 	X	 	296	25			X		356	25		 	X	
237	25			X	 	297	25			X		357	25			X	
238	25			X	 	298	25			X		358	25			X	
239	25			X	 	299	25			X		359	25			X	
240	25				 	300	25					360	25		 		
240	40		1	X		300	40		l	Х	1	200	20			X	

Table B.5.14.-26: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (25 km/h) and a low engine displacement (< 50 cm3) or maximum net or continuous rated power (≤ 4 kW), cold or warm, 181 to 360 s

2.3.2.3.

	roller		phase ir	ndicators		l	roller		phase ir	ndicators		l	roller		phase in	ndicators	
time in s	speed in km/h	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec
361	25			X		421	25		Х			481	0	х			
362	25			X		422	25		X			482	0	х			
363	25			X		423	25		X			483	0	X			
364	25			X		424	25		Х			484	0	X			ļ
365	25			X		425	25		Х			485	0	Х			
366	25			X		426	25		Х			486	1,4		Х		<u> </u>
367	25			X		427	25		X			487	4,5		X		
368 369	25 25			X X		428 429	25 25		Х	Х		488 489	8,8 13,4		X X		
370	25			X		430	25			X		490	17,3		X		
371	25			X		431	25			X		491	19,2		X		
372	25			X		432	25			X		492	19,7		X		
373	25			Х		433	25			х		493	19,8		х		
374	25			X		434	25			Х		494	20,7		Х		
375	25			X		435	25			Х		495	23,7		Х		
376	25			X		436	25					496	25				
377	25			X		437	25					497	25				<u> </u>
378	25			X		438	25					498	25				<u> </u>
379	25			X		439	25					499	25				<u> </u>
380	25 25			X		440	25 25					500 501	25 25				
381 382	25			X		441 442	25					501	25				—
383	25			X X		443	25					503	25				
384	25			X		444	25					504	25				
385	25			X		445	25					505	25				
386	25			X		446	25					506	25				
387	25			Х		447	23,4				X	507	25				
388	25			X		448	21,8				X	508	25				
389	25			X		449	20,3				X	509	25				
390	25			X		450	19,3				X	510	23,1				Х
391	25			X		451	18,7				X	511	16,7				Х
392	25					452	18,3				X	512	10,7				Х
393	25					453	17,8				X	513	4,7				Х
394 395	25 24,9					454 455	17,4 16,8				X	514 515	1,2 0				Х
396	21,4				X X	456	16,3			Х	X	516	0	X			
397	15,9				X	457	16,5			X		517	0	X			
398	9,9				X	458	17,6			X		518	0	X			
399	4,9				Х	459	19,2			Х		519	3		Х		
400	2,1				х	460	20,8			х		520	8,2		х		
401	0,9				Х	461	22,2			Х		521	14,3		Х		
402	0	Х				462	23			X		522	19,3		Х		
403	0	Х				463	23				X	523	23,5		Х		
404	0	Х				464	22				X	524	25				<u> </u>
405	0	X				465	20,1				X	525	25				
406	0	X				466	17,7				X	526 527	25 25				
407	1,2	Х	Х			467 468	15 12,1		 		X	528	25				
400	3,2		X		 	469	9,1		 		X	529	25	 			
410	5,9		X			470	6,2				X	530	25				
411	8,8		X			471	3,6				X	531	23,2				Х
412	12		X			472	1,8				X	532	18,5				X
413	15,4		Х			473	0,8				X	533	13,8				Х
414	18,9		Х			474	0	X				534	9,1				Х
415	22,1		Х			475	0	Х				535	4,5				Х
416	24,7		Х			476	0	X				536	2,3				Х
417	25					477	0	Х				537	0	Х			
418	25					478	0	X				538	0	Х			
419	25					479	0	Х				539	0	Х	<u> </u>		<u> </u>
420	25					480	0	X				540	0				<u> </u>

Table B.5.14.-27: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (25 km/h) and a low engine displacement ($< 50 \text{ cm}^3$) or maximum net or continuous rated power ($\le 4 \text{ kW}$), cold or warm, 361 to 540 s

2.3.2.4.

time in s	roller speed in		phase i	ndicators	
ume m s	km/h	stop	acc	cruise	dec
541	0	X			
542	2,8		х		
543	8,1		х		
544	14,3		X		
545	19,2		Х		
546	23,5		Х		
547	25				
548	25				
549	25				
550	25				
551	25				
552	25				
553	25			Х	
554	25			Х	
555	25			Х	
556	25			X	
557	25 25			X	
558				X	
559 560	25 25			X	
561	25			X	
562	25			X X	
563	25				
564	25			X X	
565	25			×	
566	25			×	
567	25			X	
568	25			X	
569	25			X	
570	25			X	
571	25			Х	
572	25			х	
573	25				
574	25				
575	25				
576	25				
577	25				
578	25				
579	25				
580	25				
581	25				
582	21,8				X
583	17,7				Х
584	13,5				Х
585	9,4				X
586	5,6				X
587	2,1			-	X
588	0	X		-	
589	0	X		-	
590	0	X		-	
591 592	0	X			
592	0	X		-	
593	0	X			
594	0	X			
596	0	X X			
597	0	X			
598	0	X		 	
599	0	X			
600	0	X			
550		- ^			

Table B.5.14.-28: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (25 km/h) and a low engine displacement ($< 50 \text{ cm}^3$) or maximum net or continuous rated power ($\le 4 \text{ kW}$), cold or warm, 541 to 600 s

2.3.2.5.

	roller	,	phase in	ndicators		Ι	roller		phase in	ndicators		I	roller		phase in	dicators	
time in s	speed in	stop	acc	cruise	dec	time in s	speed in	stop	acc	cruise	dec	time in s	speed in	stop	acc	cruise	dec
	km/h		acc	Ciuise	uec		km/h	stop	acc	Ciuise			km/h	stop	acc		uec
0	0	Х				61	29,6				Х	121	31,2			Х	
1	0	X				62	26,9				X	122	33			X	
3	0	X				63 64	23 18,6				X X	123 124	34,4 35,2			X X	
4	0	X X				65	14,1				X	125	35,4			X	Х
5	0	X				66	9,3				X	126	35,2				X
6	0	X				67	4,8				X	127	34,7				X
7	0	Х				68	1,9				X	128	33,9				X
8	0	X				69	0	X				129	32,4				Х
9	0	Х				70	0	Х				130	29,8				X
10	0	Х				71	0	X				131	26,1				X
11	0	X				72	0	X				132	22,1				X
12	0	X				73	0	X				133	18,6				X
13	0	X				74	1,7		Х			134	16,8		Х		
14	0	Х				75	5,8		Х			135	17,7		Х		
15	0	X	 	-		76	11,8		X	 		136 137	21,1		Х		
16 17	0	X		-	<u> </u>	77 78	17,3 22		X			137	25,4 29,2		X		
18	0	X X				79	26,2		X X	 		139	31,6		X		
19	0	X	<u> </u>			80	29,4		X	<u> </u>		140	32,1		X		X
20	0	X				81	31,1		X			141	31,6				X
21	0	X				82	32,9		X			142	30,7				X
22	1		х			83	34,7		X			143	29,7				X
23	2,6		х			84	34,8		Х			144	28,1				X
24	4,8		Х			85	34,8		Х			145	25				X
25	7,2		X			86	34,9		X			146	20,3				X
26	9,6		Х			87	35,4		Х			147	15				X
27	12		Х			88	36,2		Х			148	9,7				X
28	14,3		Х			89	37,1		Х			149	5				X
29 30	16,6 18,9		X			90 91	38 38,7		Х			150 151	1,6 0	.,			X
31	21,2		X			92	38,9			X		152	0	X X			
32	23,5		X			93	38,9			X		153	0	X			
33	25,6		X			94	38,8			Х		154	0	X			
34	27,1		Х			95	38,5			Х		155	0	Х			
35	28		Х			96	38,1			Х		156	0	X			
36	28,7		Х			97	37,5			X		157	0	Х			
37	29,2		Х			98	37			X		158	0	X			
38	29,8		Х			99	36,7			X		159	0	X			
39	30,3			Х		100	36,5			Х		160	0	Х			
40	29,6		-	X		101	36,5		-	X		161	0	X			
41	28,7 27,9			X		102 103	36,6 36,8		-	X		162 163	0	X X			
43	27,4		<u> </u>	X		103	37		<u> </u>	X		164	0	X			
44	27,3			X		105	37,1			X		165	0	X			
45	27,3			X		106	37,3		1	X		166	0	Х			
46	27,4		İ	Х		107	37,4			Х	İ	167	0	X	İ		
47	27,5			X		108	37,5			X		168	0	Х			
48	27,6			Х		109	37,4			Х		169	0	X			
49	27,6			X		110	36,9				Х	170	0	X			
50	27,6			Х		111	36				Х	171	0	X			
51	27,8			X	<u> </u>	112	34,8				Х	172	0	X			
52	28,1		<u> </u>	X		113	31,9		<u> </u>		X	173	0	X			
53	28,5		-	X		114	29		-		X	174	0	X			
54 55	28,9 29,2		<u> </u>	X		115	26,9 24,7		<u> </u>	 	Х	175 176	0	X			
56	29,2		 	X	-	116 117	25,4		-	X		176	0	X	<u> </u>		
57	29,4		-	X		118	26,4		-	X		178	0	X X			
58	30			X		119	27,7			X		179	0	X			
59	30,5			X		120	29,4		i –	X		180	0	X			
60	30,6				Х					İ					İ		

Table B.5.14.-29: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (where applicable truncated at 45 km/h, respectively at 50 km/h) and a low engine displacement ($< 50~{\rm cm}^3$) or maximum net or continuous rated power ($\le 4~{\rm kW}$), cold or warm, 0 to 180 s

2.3.2.6.

	roller		phase ir	ndicators		I	roller		phase ir	ndicators		I	roller	<u> </u>	phase in	ndicators	
time in s	speed in	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec
181	km/h 0	· ·				241	43,9	-		v		301	30,6			v	
182	0	X				242	43,8			Х	Х	302	29			X	
183	0	X				243	43				X	303	27,8			X	
184	0	X				244	40,9				X	304	27,2			X	
185	0,4		Х			245	36,9				Х	305	26,9			Х	
186	1,8		Х			246	32,1				Х	306	26,5			Х	
187	5,4		X			247	26,6				Х	307	26,1			Х	
188	11,1		X			248	21,8				X	308	25,7			X	
189 190	16,7 21,3		X			249 250	17,2 13,7				X X	309 310	25,5 25,7			X X	
191	24,8		X			251	10,3				X	311	26,4			Х	
192	28,4		X			252	7				X	312	27,3			X	
193	31,8		Х			253	3,5				Х	313	28,1			Х	
194	34,6		Х			254	0	Х				314	27,9				Х
195	36,3		X			255	0	X				315	26				X
196	37,8		X			256	0	X				316	22,7				X
197	39,6		Х	ļ		257	0	X				317	19				X
198 199	41,3 43,3		X			258 259	0	X				318 319	16 14,6		.,		Х
200	45,5		Х			260	0	X X				320	15,2		X		
201	45					261	0	X				321	16,9		X		
202	45					262	0	Х				322	19,3		X		
203	45			Х		263	0	Х				323	22		Х		
204	45			Х		264	0	X				324	24,6		Х		
205	45			X		265	0	X				325	26,8		Х		
206	45			X		266	0	X				326	27,9		Х		
207	45			Х		267	0,5		X			327	28			Х	
208	45 45			X		268	2,9		X			328 329	27,7 27,1			X	
210	45 45			X X		269 270	8,2 13,2		X			330	26,8			X	
211	45			X		271	17,8		X			331	26,6			X	
212	45			Х		272	21,4		Х			332	26,8			Х	
213	45			X		273	24,1		X			333	27			X	
214	45			X		274	26,4		X			334	27,2			X	
215	45			Х		275	28,4		X			335	27,4			X	
216	45			Х		276	29,9		Х			336	27,5			Х	
217	45			X		277	30,5			X		337	27,7			X	
218 219	45 45			X X		278 279	30,5 30,3			X X		338 339	27,9 28,1			X	
220	45			X		280	30,3		 	X		340	28,3			X	
221	45			X		281	30,1			X		341	28,6			X	
222	45			X		282	30,1			X		342	29,1			Х	
223	45			Х		283	30,1			Х		343	29,6			X	
224	45			Х		284	30,2			X		344	30,1			X	
225	45			Х		285	30,2			X		345	30,6			Х	
226 227	45 45			X		286 287	30,2 30,2			X		346 347	30,8 30,8			X	
228	45 45			X X		288	30,2		 	X X		347	30,8		_	X	
229	45			Х		289	31		 	X		349	30,8			X	
230	45			X		290	31,9			X		350	30,8			X	
231	45			X		291	32,8			X		351	30,8			Х	
232	45			Х		292	33,7			X		352	30,8			Х	
233	45			Х		293	34,5			X		353	30,8			Х	
234	45			X		294	35,1			X		354	30,9			Х	
235	45		<u> </u>	X		295	35,5		<u> </u>	X		355	30,9			X	
236	44,4 43,5		-	X X		296 297	35,6 35,4		 	X X		356 357	30,9 30,8		-	X	
238	43,5			X	—	298	35,4			X		358	30,6			X	
239	43,3			X		299	34			X		359	29,6			Х	
240	43,7			X		300	32,4			X		360	28,4			X	
	177						9.5						.,,,				

Table B.5.14.-30: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (where applicable truncated at 45 km/h, respectively at 50 km/h) and a low engine displacement ($< 50~{\rm cm}^3$) or maximum net or continuous rated power ($\le 4~{\rm kW}$), cold or warm, 181 to 360 s

2.3.2.7.

	roller		phase in	ndicators			roller		phase ii	ndicators]	roller		phase ir	ndicators	
time in s		stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec	time in s	speed in km/h	stop	acc	cruise	dec
361	27,1			х		421	34		х			481	0	Х			
362	26			Х		422	35,4		Х			482	0	Х			
363	25,4			X		423	36,5		Х			483	0	X			
364	25,5			X		424	37,5		X			484	0	X	-		
365 366	26,3 27,3			X X		425 426	38,6 39,6		X X			485 486	0 1,4	Х	Х		
367	28,3			X	_	427	40,7		X			487	4,5		X		
368	29,2			X		428	41,4		X			488	8,8		X		
369	29,5			х		429	41,7			х		489	13,4		х		
370	29,4			Х		430	41,4			Х		490	17,3		Х		
371	28,9			Х		431	40,9			X		491	19,2		Х		
372	28,1			Х		432	40,5			Х		492	19,7		Х		
373 374	27,1 26,3			X		433 434	40,2 40,1			X		493 494	19,8 20,7		X		
375	25,7			X X		434	40,1			X X		494	23,7		X		
376	25,5			X		436	39,8			^	Х	496	27,9		X		
377	25,6			X		437	38,9				X	497	31,9		X		
378	25,9			х		438	37,4				Х	498	35,4		х		
379	26,3			Х		439	35,8				X	499	36,2				Х
380	26,9			Х		440	34,1				Х	500	34,2				Х
381 382	27,6 28,4			X		441 442	32,5 30,9				X	501 502	30,2 27,1				X
383	29,3			X X	_	442	29,4		_		X X	502	26,6		Х		Х
384	30,1			X		444	27,9				X	504	28,6		X		
385	30,4			X		445	26,5				X	505	32,6		X		
386	30,2			Х		446	25				Х	506	35,5		Х		
387	29,5			Х		447	23,4				X	507	36,6				Х
388	28,6			Х		448	21,8				X	508	34,6				Х
389	27,9			Х		449	20,3				X	509	30				Х
390 391	27,5 27,2			X X		450 451	19,3 18,7				X X	510 511	23,1 16,7				X
392	26,9			^	Х	452	18,3				X	512	10,7				X
393	26,4				X	453	17,8				X	513	4,7				Х
394	25,7				х	454	17,4				Х	514	1,2				Х
395	24,9				Х	455	16,8				X	515	0	X			
396	21,4				Х	456	16,3			X		516	0	X			
397	15,9				Х	457	16,5			Х		517	0	Х			
398 399	9,9 4,9				X	458 459	17,6 19,2			X		518 519	3	Х	v		
400	2,1				X	460	20,8			X		520	8,2		X		
401	0,9				X	461	22,2			X		521	14,3		X		
402	0	Х				462	23			х		522	19,3		Х		
403	0	Х				463	23				Х	523	23,5		Х		
404	0	Х				464	22				X	524	27,3		Х		
405	0	X				465 466	20,1		-		X	525	30,8		X		
406 407	0	X X	 		 	466 467	17,7 15		-	 	X X	526 527	33,7 35,2		X	\vdash	
408	1,2	۸	Х			468	12,1				X	528	35,2		^		Х
409	3,2		X			469	9,1				X	529	32,5				X
410	5,9		Х			470	6,2				X	530	27,9				Х
411	8,8		Х			471	3,6				Х	531	23,2				Х
412	12		х			472	1,8				X	532	18,5				X
413	15,4		X			473	0,8				Х	533	13,8				X
414 415	18,9 22,1		X		<u> </u>	474 475	0	X				534 535	9,1 4,5				X
416	24,7		X X		-	476	0	X X				536	2,3				X
417	26,8		X			477	0	X				537	0	Х		\vdash	^
418	28,7		X			478	0	X				538	0	X			
419	30,6		Х			479	0	Х				539	0	Х			
420	32,4		Х			480	0	Х				540	0	Х			

Table B.5.14.-31: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (where applicable truncated at 45 km/h, respectively at 50 km/h) and a low engine displacement (< 50 cm 3) or maximum net or continuous rated power (\le 4 kW), cold or warm, 361 to 540 s

2.3.2.8.

	roller		phase indicators						
time in s	speed in	stop	acc	cruise	dec				
541	km/h 0	x							
542	2,8	^	x						
543	8,1		×	1					
544	14,3		×						
545	19,2		×						
546	23,5								
547	27,2		×	1					
548	30,5								
549	33,1		×						
550	35,7		×						
551	38,3		×						
552	41		×	 					
553	43,6		_^	x					
554	43,7								
555	43,8		 	X					
			-	X					
556	43,9		-	X					
557	44			X					
558	44,1		-	X					
559	44,2		 	X					
560	44,3		-	X					
561	44,4			X					
562	44,5			X					
563	44,6			×					
564	44,9			X					
565	45			X					
566	45			×					
567	45			X					
568	45			X					
569	45			X					
570	45			X					
571	45			×					
572	45			X					
573	45								
574	45								
575	45								
576	42,3				X				
577	39,5				x				
578	36,6				X				
579	33,7				X				
580	30,1				X				
581	26		.		X				
582	21,8		-		X				
583	17,7				X				
584	13,5				X				
585	9,4				X				
586	5,6		₩		X				
587	2,1		-		X				
588	0	X							
589	0	X	.	-					
590	0	X	-						
591	0	X							
592	0	X							
593	0	X	.						
594	0	X							
595	0	X							
596	0	X							
597	0	X							
598	0	X							
599	0	X							
600	0	×							

Table B.5.14.-32: WMTC, part 1, class 1, applicable for vehicles with a maximum design vehicle speed (where applicable truncated at 45 km/h, respectively at 50 km/h) and a low engine displacement ($< 50 \text{ cm}^3$) or maximum net or continuous rated power ($\le 4 \text{ kW}$), cold or warm, 541 to 600 s

B.5.15. Annex: explanatory note on the gearshift procedure

1. Introduction

This explanatory note explains matters specified or described in this Regulation, including its Annexes or Appendices, and matters related thereto with regard to the gearshift procedure.

2. Approach

- 2.1. The development of the gearshift procedure was based on an analysis of the gearshift points in the in-use data. In order to establish generalised correlations between technical specifications of the vehicles and desired vehicle speeds to shift gears, the engine speeds were normalised to the utilisable band between rated engine speed and idling engine speed.
- 2.2. In a second step, the end speeds (vehicle speed as well as normalised engine speed) for upshifts and downshifts were determined and recorded in a separate table. The averages of these speeds for each gear and vehicle were calculated and correlated with the vehicles' technical specifications.
- 2.3. The results of these analyses and calculations can be summarised as follows:
 - (a) the gearshift behaviour is engine-speed-related rather than vehicle-speed-related;
 - (b) the best correlation between gearshift desired vehicle speeds and technical data was found for normalised engine speeds and the power-to-mass ratio (maximum continuous rated power/(reference mass));
 - (c) the residual variations cannot be explained by other technical data or by different drive train ratios. They are most probably due to differences in traffic conditions and individual driver behaviour;
 - (d) the best approximation between gearshift desired vehicle speeds and power-tomass ratio was found for exponential functions;
 - (e) the gearshift mathematical function for the first gear is significantly lower than for all other gears;
 - (f) the gearshift desired vehicle speeds for all other gears can be approximated by one common mathematical function;
 - (g) no differences were found between five-gear and six-gear transmissions;
 - (h) gearshift behaviour in Japan is significantly different from the equal-type gearshift behaviour in the European Union (EU) and in the United States of America (USA).
- 2.4. In order to find a balanced compromise between the three regions, a new approximation function for normalised upshift engine speeds versus power-to-mass ratio was calculated as a weighted average of the EU/USA curve (with 2/3 weighting) and the Japanese curve (with 1/3 weighting), resulting in the following equations for normalised upshift engine speeds:
 - Equation B.5.15.-1: Normalised upshift engine speed in 1st gear (gear 1)

$$n_{max_{acc}(1)} = (0.5753 \times e^{(-1.9 \times \frac{P_n}{m_k + 75})} - 0.1) \times (s - n_{idle}) + n_{idle}$$

Equation B.5.15.-2: Normalised upshift engine speed in gears > 1

$$n_{max_{acc}(i)} = (0.5753 \times e^{(-1.9 \times \frac{P_n}{m_k + 75})}) \times (s - n_{idle}) + n_{idle}$$

3. Calculation example

- 3.1 Figure B.5.15.-1 shows an example of gearshift use for a small vehicle:
 - (a) the lines in bold show the gear use for acceleration phases;
 - (b) the dotted lines show the downshift points for deceleration phases;
 - (c) in the cruising phases, the whole engine speed range between downshift engine speed and upshift engine speed may be used.

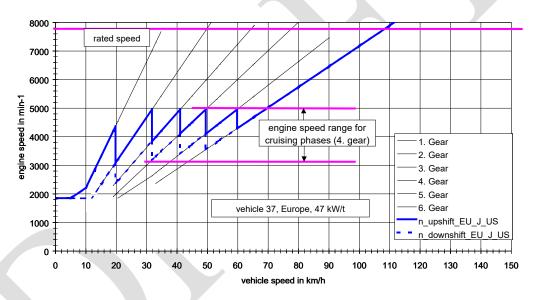


Figure B.5.15.-1: Example of a gearshift sketch for a small vehicle

3.2 Where vehicle speed increases gradually during cruise phases, upshift engine speeds $(v1\rightarrow 2, v2\rightarrow 3$ and $vi\rightarrow i+1)$ in km/h may be calculated using the following equations:

Equation B.5.15.-3:

$$v_{1\rightarrow 2} = \left[0.03 \times (s - n_{idle}) + n_{idle}\right] \times \frac{1}{ndv_2}$$

Equation B.5.15.-4:

$$v_{1 \rightarrow 2} = \left[\begin{array}{c} (0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{mref})}{mref}} - 0.1) \times (s - n_{idle}) + n_{idle} \end{array} \right] \times \frac{1}{n dv_1}$$

Equation B.5.15.-5:

$$v_{i \rightarrow i+1} = \left[(0.5753 \times e^{\frac{(-1.9 \times \frac{P_n}{mref})}{mref}}) \times (s - n_{idle}) + n_{idle} \right] \times \frac{1}{ndv_{i-1}}, i = 3 \text{ to ng}$$

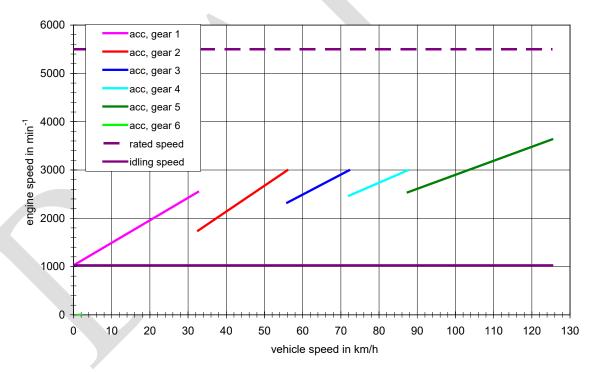


Figure B.5.15.-2: gear use during acceleration phases

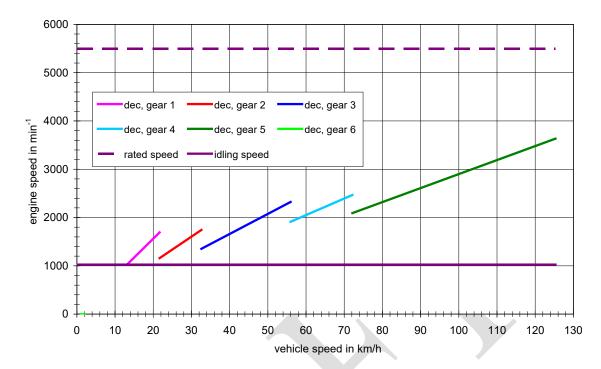


Figure B.5.15.-3: Example of a gearshift sketch — Gear use during deceleration and cruise phases

In order to allow the technical service more flexibility and to ensure driveability, the gearshift regression functions should be considered as lower limits. Higher engine speeds are permitted in any cycle phase.

4. Phase indicators

4.1 In order to avoid different interpretations in the application of the gearshift equations and thus to improve the comparability of the test, fixed-phase indicators are assigned to the vehicle speed pattern of the cycles. The specification of the phase indicators is based on the definition from the Japan Automobile Research Institute (JARI) of the four driving modes as shown in the following table:

4 modes	Definition
Idle mode	vehicle speed < 5 km/h and -0.5 km/h/s $(-0.139 \text{ m/s}^2) < \text{acceleration} < 0.5$ km/h/s (0.139 m/s^2)
Acceleration mode	acceleration $> 0.5 \text{ km/h/s} (0.139 \text{ m/s}^2)$
Deceleration mode	acceleration $< -0.5 \text{ km/h/s} (-0.139 \text{ m/s}^2)$
Cruise mode	vehicle speed \geq 5 km/h and -0.5 km/h/s (-0.139 m/s ²) < acceleration < 0.5 km/h/s (0.139 m/s ²)

Table B.5.15.-1: Definition of driving modes

4.2 The indicators were then modified in order to avoid frequent changes during relatively homogeneous cycle parts and thus improve driveability. Figure Ap9-2 shows an example from cycle part 1.

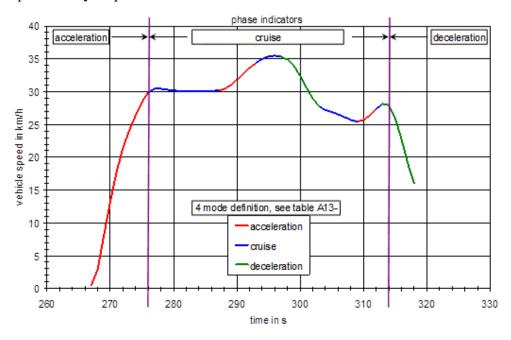


Figure B.5.15.4: Example for modified phase indicators

5. Calculation example

- 5.1. An example of input data necessary for the calculation of shift engine speeds is shown in Table B.5.15.-2. The upshift engine speeds for acceleration phases for first gear and higher gears are calculated using Equations B.5.15.-1 and B.5.15.-2. The denormalisation of engine speeds can be performed using the equation $n = n_n$ norm x (s n_{idle}) + n_{idle} .
- 5.2. The downshift engine speeds for deceleration phases can be calculated using Equations B.5.15.-3 and B.5.15.-4. The ndv values in Table B.5.15.-2 can be used as gear ratios. These values can also be used to calculate the corresponding vehicle speeds (vehicle shift speed in gear i = engine shift speed in gear i / ndvi). The results are shown in Tables B.5.15.-3 and B.5.15.-4.
- 5.3. Additional analyses and calculations were conducted to investigate whether these gearshift algorithms could be simplified and, in particular, whether engine shift speeds could be replaced by vehicle shift speeds. The analysis showed that vehicle speeds could not be brought in line with the gearshift behaviour of the in-use data.

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Item Input data

Engine capacity in cm ³	600
P _n in kW	72
m _k in kg	199
s in min ⁻¹	11800
nidle in min-1	1150
ndv ₁ */	133.66
ndv2	94.91
ndv3	76.16
ndv4	65.69
ndv5	58.85
ndv ₆	54.04
pmr <u>**</u> / in kW/t	262.8

^{*/}ndv means the ratio between engine speed in min⁻¹ and vehicle speed in km/h

Table B.5.15.-2: Input data for the calculation of engine and vehicle shift speeds

5.3.2.

	EU/USA/JAPAN DRIVING BEHAVIOUR			
	EU/USA/Japan driving behaviour	n_acc_max (1)		
n_norm */ in percent	24.9	34.9		
n in min-1	3804	4869		

Table B.5.15.-3: Shift engine speeds for acceleration phases for first gear and for higher gears (see Table B.5.15.-1)

5.3.3.

Gearshift	EU/USA/Japan driving behaviour
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^{**/}pmr means the power-to-mass ratio calculated by Pn / (mk) · 1000; Pn in kW, mk in kg

		v in km/h	n_norm (i) in percent	n in min ⁻¹	
Upshift	1→2	28.5	24.9	3804	
	2→3	51.3	34.9	4869	
	3→4	63.9	34.9	4869	
	4→5	74.1	34.9	4869	
	5→6	82.7	34.9	4869	
Downshift	2 → cl <u>*</u> /	15.5	3.0	1470	
	3→2	28.5	9.6	2167	
	4→3	51.3	20.8	3370	
	5→4	63.9	24.5	3762	
	6→5	74.1	26.8	4005	
*/'cl' means 'Clutch-Off' timing.					

Table B.5.14.-4: Engine and desired vehicle shift speeds based on Table B.5.15.-2



